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16. Abstract <p>In 2003, the Michigan Department of Transportation constructed an unbonded concrete overlay with experimental features on northbound I-75 in Ogemaw County. The experimental features are:</p> <ul style="list-style-type: none"> • 10 and 12 foot transverse joint spacing. Standard spacing is 14 to 16 feet for jointed plain concrete pavement depending on thickness. • No dowel bars at some of the transverse joints. • Transverse joints cut at 1/8" and left unsealed or 1/4" and sealed with hot-pour rubber. Standard transverse joints are 7/16" wide and sealed with preformed neoprene rubber. • Longitudinal joints cut at 1/8" and left unsealed compared to the standard of 1/4" and sealed with hot-pour rubber. • New, more open-graded HMA separator layer. <p>The southbound direction was rubblized and then paved with HMA under a separate contract from the unbonded concrete overlay.</p> <p>Both projects went very well with the unbonded overlay taking 69 days from start to completion of paving for 12 lane-miles plus shoulders. The rubblize and HMA surfacing took 51 days from start to completion of paving for 8 lane-miles plus shoulders.</p> <p>Both projects will be monitored with visual evaluations, falling weight deflectometer testing, and ride quality measurements, for 15 years. Interim performance reports will be written at years 5 and 10, or as needed.</p>			
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**MICHIGAN DEPARTMENT OF TRANSPORTATION
MDOT**

**UNBONDED CONCRETE OVERLAY DEMONSTRATION PROJECT
ON I-75 IN OGEMAW COUNTY - CONSTRUCTION REPORT**

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Andrew Bennett**

**Testing and Research Section
Construction and Technology Support Area
Work Plan No. 03 WP-147
Research Project G-0333
Research Report R-1465**

**Michigan Transportation Commission
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EXECUTIVE SUMMARY

In 2003, the Michigan Department of Transportation constructed an unbonded concrete overlay with experimental features on northbound I-75 in Ogemaw County. The experimental features are:

- 10 and 12 foot transverse joint spacing. Standard spacing is 14 to 16 feet for jointed plain concrete pavement depending on thickness.
- No dowel bars at some of the transverse joints.
- Transverse joints cut at 1/8" and left unsealed or 1/4" and sealed with hot-pour rubber. Standard transverse joints are 7/16" wide and sealed with preformed neoprene rubber.
- Longitudinal joints cut at 1/8" and left unsealed compared to the standard of 1/4" and sealed with hot-pour rubber.
- New, more open-graded HMA separator layer.

The southbound direction was rubblized and then paved with HMA under a separate contract from the unbonded concrete overlay.

Both projects went very well with the unbonded overlay taking 69 days from start to completion of paving for 12 lane-miles plus shoulders. The rubblize and HMA surfacing took 51 days from start to completion of paving for 8 lane-miles plus shoulders.

Both projects will be monitored with visual evaluations, falling weight deflectometer testing, and ride quality measurements, for 15 years. Interim performance reports will be written at years 5 and 10, or as needed.

INTRODUCTION

Unbonded concrete overlays of existing concrete pavements have been a successful rehabilitation alternative in Michigan since the early 1980's. In a continuing effort to use concrete as a rehabilitation alternative, the Michigan Department of Transportation (MDOT) teamed with the Michigan Concrete Paving Association (MCPA) to try a more economical unbonded concrete overlay design.

Michigan's unbonded overlays have averaged about eight inches thick, joints spaced 15 to 27 feet, and sealed with preformed neoprene. Both reinforced and non-reinforced designs have been built with the smaller joint spacing corresponding to the non-reinforced design. The asphalt bond breaker layer has been either one or two inches thick with one inch being the predominant design in more recent projects. The experimental design is a non-reinforced 6 inch concrete. It is intended for pavements with low truck traffic (< 5000 trucks a day). After discussions between MDOT and MCPA, the project was split into five sections as follows:

1. A ¼ mile section with 10 foot joint spacing and no load transfer at the transverse joints. Transverse and longitudinal joints will be cut 1/8 inch wide and not sealed.
2. A ¼ mile section with 10 foot joint spacing and no load transfer at the transverse joints. Transverse and longitudinal joints will be cut ¼ inch wide and will be filled with hot-pour rubber.
3. A 1½ mile section with 12 foot joint spacing and no load transfer at the transverse joints. Transverse and longitudinal joints will be cut at 1/8 inch wide and not sealed.
4. A 1½ mile section with 12 foot joint spacing and no load transfer at the transverse joints. Transverse and longitudinal joints again will be cut ¼ inch wide and will be filled with hot-pour rubber.
5. A ½ mile control section with 12 foot joint spacing and load transfer bars at the transverse joints. Transverse and longitudinal joints will be cut ¼ inch wide and will be filled with hot-pour rubber.

For all sections, the load transfer bars will be 1 inch diameter which is now the standard for concrete pavements from 6 inches to less than 8 inches. Previous projects used 1¼ inch diameter bars, which was standard for pavements under 11 inches. Tie bars will also be used at the longitudinal joints in all sections. A table of the stationing, as well as typical cross-sections, for each section can be found in the Appendix.

The overlay is a minimum of six inches thick but was allowed to vary in case grade correction is needed. The asphalt separator layer (bond breaker layer) was also modified from the typical. The separator layer mix is more open to allow more drain ability than has been typical on other unbonded concrete overlays. The cracks and joints in the existing concrete pavement were sealed with an overband crack fill prior to the placement of the interlayer. Full-depth repairs were also utilized to prep the pavement for the overlay.

A section of I-75 in Ogemaw County near West Branch was chosen as the site for the

experimental pavement. The limits are from Ski Park Rd. to the Ogemaw/Roscommon county line. A map showing the project location can be seen in Figure 1. The unbonded overlay was constructed on the northbound side only. The southbound side was rubblized and overlaid with 6 ½ inches of asphalt under a separate contract as a comparison to the unbonded overlay.

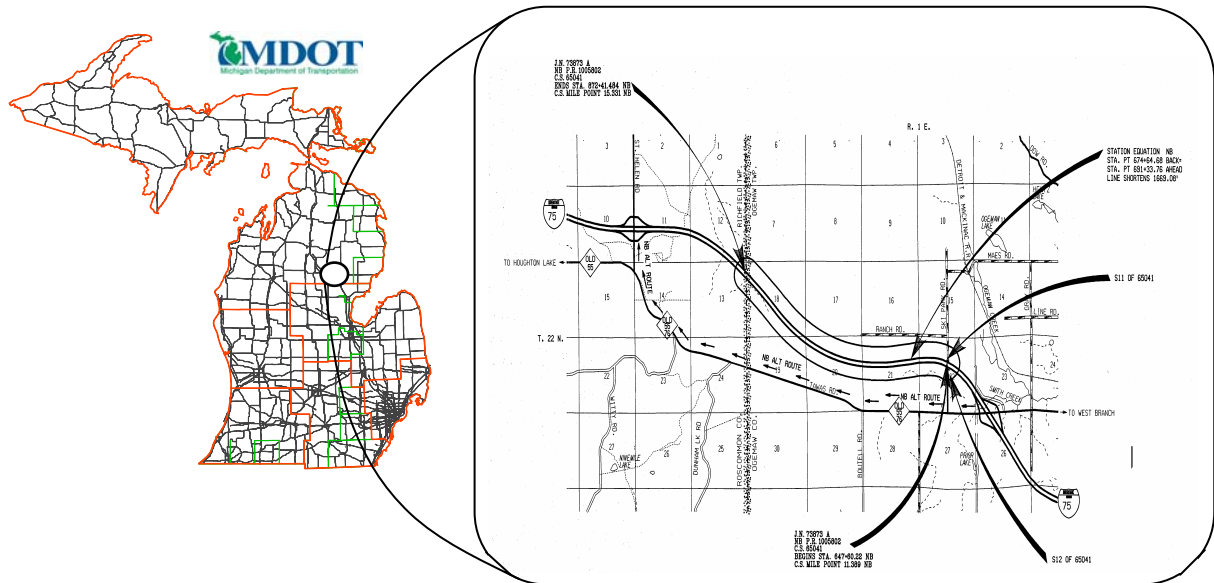


Figure 1. Project location.

BACKGROUND

The existing northbound pavement for this demonstration project is a three lane, 9” reinforced concrete with asphalt shoulders, built in 1973. The base is 4” of dense graded aggregate over 10” of sand subbase. Three different joint spacings of 71’-2”, 57’-3”, and 43’-4” were utilized as part of a joint spacing experiment. Plastic coated dowel bars for load transfer were also included as part of the experiment. A section of 71’-2” joint spacing with plain steel dowels, which were both the standards at the time, was also built for comparison to the experimental sections. The northern three-tenths of a mile is only two lanes.

2002 average daily traffic is 11,900 with 11.7% commercial traffic. One project was let in 1991 to fix deterioration at joints and cracks with full-depth repairs, crack sealing, and spall repair. Routine maintenance (pothole patching, etc.) done during the life of this pavement was not investigated. The southbound pavement has the same cross-section but is only two lanes.

CONSTRUCTION

Unbonded Concrete Overlay

Preparation work on the existing concrete pavement began on August 10 with full-depth repairs of deteriorated joints, cracks, and previous repairs. This work continued until August 21. Overband crack filling of the joints and cracks occurred behind the full-depth repair operation from August 14 to 22.

On August 27, work began on the inside (median) shoulder to widen it for traffic control purposes. The transition area from the Ski Park Road bridge approach slab to the unbonded overlay (235 feet) was removed starting on September 8. Paving of the inside shoulder began on September 9 with the separator layer paving of the inside shoulder and passing lane beginning on September 11. Concrete placement began on September 15 with both the 9" thick reinforced transition area and the unbonded overlay. Left shoulder and passing lane were completed on September 24 and traffic was shifted over on September 29.

Pavement removal for the transition area on the middle and traffic lanes began on September 29 with concrete placement beginning the next day. On October 2, separator layer paving began for the middle and traffic lanes and the outside shoulder and ends on October 7. The unbonded overlay paving began for the middle and traffic lanes on October 6 and is completed on October 9. The outside shoulder concrete was paved from October 15 to 17. Miscellaneous work occurred after that including pavement striping on October 23 and shoulder corrugation grinding on November 6.

In general, construction of the unbonded concrete overlay went smoothly. There were a few problems and changes however. A leaching trench was to be installed under both shoulders except on the high side of superelevated sections. However, the class II sand that was being removed from the inside shoulder was almost as permeable as the 2NS sand that was used for the trench backfill. Because of this, the leaching trench was eliminated under the outside shoulder.

Tie bars at longitudinal joints were placed by hand as seen in Figures 2 and 3. The tie bars placed on the edge of the paver were placed in the top third of the pavement for the first few days of paving until it was adjusted downward accordingly. In many cases, the bent portion of the bar was embedded in the concrete (Figure 4) and therefore could not be straightened prior to paving the adjacent lane.

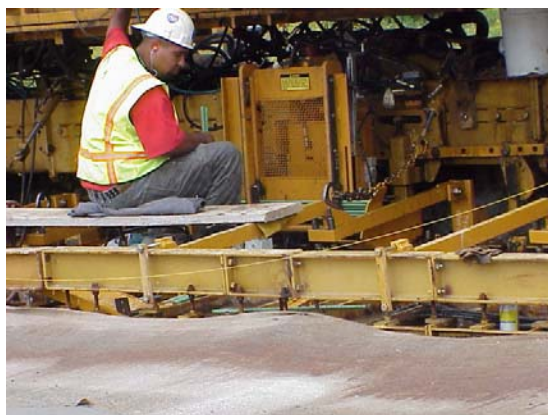


Figure 2. Set-up for placing lane tie bars during two lane paving.



Figure 3. Set-up for placing tie bars at edge of paver.



Figure 4. Tie bar embedded in the concrete. This bar can not be straightened and, therefore, is of no use.

When the passing lane and inside shoulder was paved, the separator layer was paved a foot wider than the concrete. This caused the paver track to run on the edge of the separator layer as shown in Figure 5. This broke up the edge as seen in Figures 6, 7 and 8, which caused slight headaches when paving the separator layer in the adjacent lane.



Figure 5. Paver track running on asphalt separator layer.



Figure 6. Asphalt separator layer broken from paver track.



Figure 7. Loose asphalt separator layer. Note embedded lane tie that can not be straightened for the adjacent lane



Figure 8. Missing asphalt separator layer.

Another problem with the extra one foot area was that fines from construction traffic and the concrete placement plugged the voids on the surface of the interlayer (see Figure 9). The idea of the coarse graded separator layer was drain ability of any water that reached it. Drain ability of that section of the separator layer could be a problem especially due to it's closeness to the longitudinal joint.



Figure 9. Voids in the separator layer are plugged with construction debris.

The sub-contractor paving the separator layer complained about working with it because of the coarseness of the stone, stickiness due to polymer, and it being only one inch thick. No changes were made to the layer and the sub-contractor just had to deal with the problems they cited.

Although not a problem per se, it should be noted that due to grade correction, depth of the overlay varied from about six inches to twelve inches as seen in Figures 10 and 11. The thicker sections were typically in super elevated areas. The majority of the pavement was in the seven inch range.



Figure 10. Concrete overlay close to the six inch proposed thickness.



Figure 11. Area where the concrete overlay was twelve inches thick. This was at the outside shoulder joint.

Rubblize and asphalt overlay

Work began on the southbound side with inside shoulder crushing in preparation for leaching trench placement on August 21. Paving of the inside shoulder after leaching trench began on August 23. Outside leaching trench was placed on August 26 and 27. Rubblization began on traffic lane on September 3. Base and leveling course paving began on September 5 and 6 respectively. The transition area at Ski Park Road bridge approach removal began on September 9 and concrete placement began the next day.

Rubblization of traffic lane was completed on September 17. Base and leveling course paving was completed on the traffic lane and outside shoulder on September 20.

On September 22, rubblization began on the passing lane. Transition area pavement removal began on September 23 and concrete placement started the next day. Rubblization was completed on the passing lane on September 26. Base course paving of the passing lane and inside shoulder occurred from September 30 to October 2. Leveling course was paved from October 6 to 9. Top course of asphalt was paved on the outside shoulder on October 9, and on the traffic lane on October 10. Passing lane and inside shoulder top course was paved October 11.

Miscellaneous work occurred until October 24 including rumble strip grinding and pavement marking on October 15. The authors did not follow the work on the southbound side so no problems or changes were known.

EVALUATION

For the unbonded concrete overlay on the northbound side, all distresses and full-depth repair locations were logged on paper - after the full-depth repairs were completed but prior to any paving. This was done to possibly match any problems or distresses that may occur in the overlay, with distresses in the underlying concrete. Visual evaluations of both northbound and southbound will occur every six months for the first two years and then once a year after that.

Distress Index (DI) data was requested from the MDOT's Pavement Management System (PMS) Operations Group. Pavements under MDOT's jurisdiction are surveyed every other year and the distresses are logged. The distresses are assigned point values based on their extent and severity. The points can then be aggregated over a specified distance which we call the DI for that section. Table 1 shows the 2001 and 2003 DI for northbound and southbound. Northbound has been broken down into the various test sections. When the DI reaches 50, the pavement is considered to have no life left and should be rehabilitated or reconstructed.

Table 1. Distress Index (DI) Values		
Roadway	2001 DI	2003 DI
Southbound	NA	87.2
Northbound Section 1	57.6	72.1
Northbound Section 2	53.4	67.8
Northbound Section 3	41.2	63.6
Northbound Section 4	44.1	81.0
Northbound Section 5	44.4	86.7

NA = Data not available for southbound in 2001

Ride quality was also measured just prior to and several months after construction. The initial measurements occurred after construction had begun so only one lane in each direction was available to test. The outside lane in the northbound direction and the

inside lane in the southbound direction were tested. Due to construction barrels on the southbound side, the left wheelpath laser was actually measuring the asphalt shoulder, so those numbers are not reported. All other numbers are an average of the left and right wheelpaths.

Roadway	Before Construction RQI	After Construction RQI
Southbound inside lane	70.3	24.0
Northbound Section 1 outside lane	74.9	36.9
Northbound Section 2 outside lane	76.4	33.8
Northbound Section 3 outside lane	67.9	20.8
Northbound Section 4 outside lane	69.5	23.5
Northbound Section 5 outside lane	77.5	33.5

All lanes were tested after construction. Ride quality measurements will continue yearly. Table 2 shows the results. For the after measurements, only the lanes measured before paving are reported. Michigan uses it's own ride quality scale. Ride quality of 30 or less is considered excellent, 31 to 53 is good, 54 to 69 is fair, and anything over 70 is poor. For both projects, any RQI measurement over 40 would have had to be corrected.

Falling Weight Deflectometer (FWD) testing was conducted in 2001 (at design inception) and again after construction was complete. Measurements were taken approximately every 500 feet in the traffic lane only, in both directions. Three drops equivalent to a 9000 pound load were done at each location. FWD testing will be done yearly. FWD results can be found in the appendix. Included in the appendix are:

- average maximum deflection at the load plate and 60 inches away
- average AASHTO corrected subgrade resilient modulus
- average modulus of elasticity of the concrete
- average modulus of subgrade reaction
- load transfer efficiencies at random joints and cracks

After paving, cores were taken in the unbonded concrete overlay project to verify concrete and separator layer thicknesses. Four inch and six inch diameter cores were taken in the middle and outside (right) lanes only due to traffic control restrictions. Thicknesses were measured to the nearest 1/16th of an inch at three equidistant points around the perimeter of each core, and then averaged. Table 3 shows the locations and thicknesses of each core.

MDOT core no.	Dia.	Station	Lane	Distance from outside shldr.	Concrete thickness	Sep. layer thickness
1037	6"	651+78	outside	5.0'	10.19"	1.25"
1038	6"	698+94	center	16.1'	7.75"	1.19"
1039	6"	729+94	outside	9.0'	6.69"	1.06"
1040	6"	758+85	center	15.2'	8.44"	1.13"
1041	6"	789+00	outside	5.0'	6.44"	0.94"
1042	6"	819+12	center	16.6'	7.06"	1.0"
1043	6"	849+02	outside	7.6'	7.0"	1.06"
1044	4"	834+05	center	15.8'	7.81"	1.25"
1045	4"	803+99	outside	4.3'	7.06"	0.81"
1046	4"	773+90	center	16.3'	8.56"	1.25"
1047	4"	743+94	outside	4.9'	6.56"	1.06"
1048	4"	714+03	center	13.9'	7.06"	1.13"
1049	4"	664+85	outside	5.8'	9.56"	1.19"

The average concrete thickness was 7.64" for the outside lane and 7.78" for the center lane. The average separator layer thickness was 1.05" for the outside lane and 1.16" for the center lane.

The six inch cores were cut at the asphalt/concrete interface to remove the separator layer for further testing. The separator layer was tested for permeability according to ASTM Provisional Standard PS 129-01. After cutting, it was noted that much of the separator layer void structure near the asphalt/concrete interface was plugged with cement paste. After getting permeability results on each sample, they were cut again to try to eliminate the areas where the voids were plugged. The amount cut off was between 5/16" and 9/16". A second round of testing was then conducted to see if permeabilities went up without the cement paste plugging the voids. Table 4 shows the results before and after cutting.

MDOT Core No.	Permeability before cutting (ft./day)	Permeability after cutting (ft./day)
1037	0.0	14.5
1038	0.8	31.2
1039	16.5	57.8
1040	3.2	45.8
1041	0.6	39.5
1042	3.3	30.0
1043	5.2	38.6

The mix design selected for the separator layer was an open one to allow for drainability of any water that infiltrated the overlay. The low permeability numbers before the plugged voids were cut off is a concern. However, we do not know the permeability

required to effectively drain a significant storm event so these numbers are provided for information only.

SUMMARY

Construction for both the unbonded concrete overlay and the rubblize with asphalt overlay went very well. A few concerns were noted in the unbonded concrete overlay: misplaced or embedded lane tie bars, paver track running on the edge of the asphalt separator layer, and plugging of the asphalt separator layer with concrete.

The unbonded concrete overlay took 69 days to construct from start to completion of paving for roughly 12 lane-miles plus shoulders. The rubblize and asphalt overlay took 51 days from start to completion of paving for roughly 8 lane-miles plus shoulders.

Both projects will continue to be monitored visually, and will be tested on a regular basis with the Falling Weight Deflectometer and the Rapid Travel Profilometer (ride quality).

Appendix

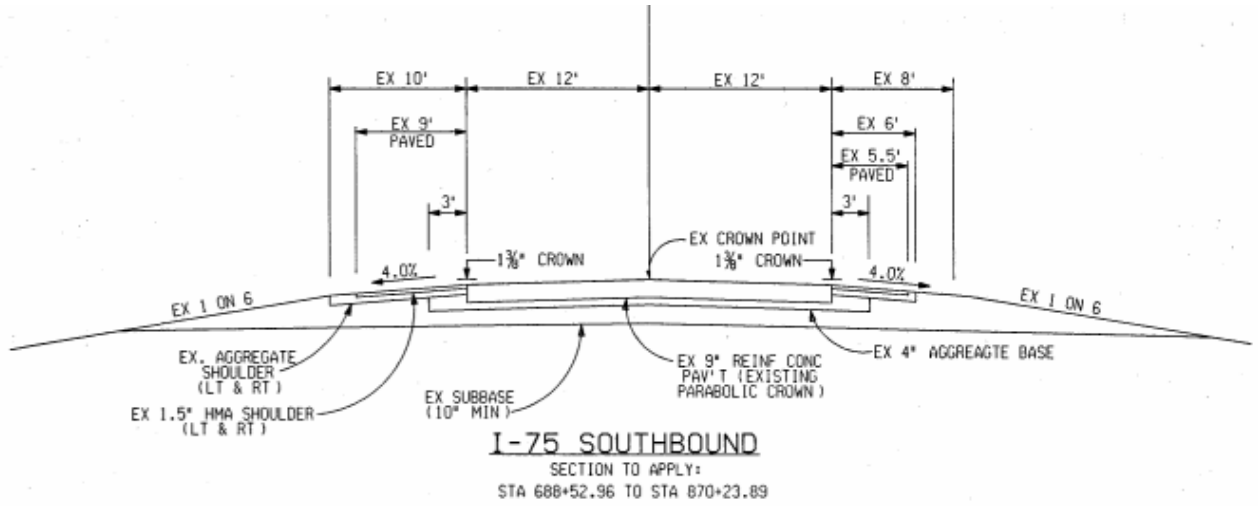
Test Section Stationing

UNBONDED CONCRETE OVERLAY JOINT TABLE			
FOR DETAILS OF ALL MODIFIED CONCRETE JOINTS SEE NEXT TYPICAL SHEET			
SECTION	TRANSVERSE JOINT TYPE	LONGITUDINAL BULKHEAD JOINT TYPE	LONGITUDINAL LANE TIE JOINT TYPE
STA 650+28.66 TO STA 664+00	MODIFIED (1) TRANSVERSE PLANE OF WEAKNESS JOINT AT 10' SPACING	MODIFIED (2) LONGITUDINAL BULKHEAD JOINT (UNSEALED JOINT WITHOUT SAWCUT)	MODIFIED (1) LONGITUDINAL LANE TIE JOINT (UNSEALED JOINT WITH 1/8" SAWCUT)
STA 664+00 TO STA 694+00 (SEE STA EDN)	MODIFIED (4) TRANSVERSE PLANE OF WEAKNESS JOINT AT 10' SPACING	MODIFIED (3) LONGITUDINAL BULKHEAD JOINT (SEALED JOINT WITH 1/4" SAWCUT)	MODIFIED (1) LONGITUDINAL LANE TIE JOINT (SEALED JOINT WITH 1/4" SAWCUT)
STA 694+00 TO STA 770+00	MODIFIED (1) TRANSVERSE PLANE OF WEAKNESS JOINT AT 12' SPACING	MODIFIED (2) LONGITUDINAL BULKHEAD JOINT (UNSEALED JOINT WITHOUT SAWCUT)	MODIFIED (1) LONGITUDINAL LANE TIE JOINT (UNSEALED JOINT WITH 1/8" SAWCUT)
STA 770+00 TO STA 845+00	MODIFIED (4) TRANSVERSE PLANE OF WEAKNESS JOINT AT 12' SPACING	MODIFIED (3) LONGITUDINAL BULKHEAD JOINT (SEALED JOINT WITH 1/4" SAWCUT)	MODIFIED (1) LONGITUDINAL LANE TIE JOINT (SEALED JOINT WITH 1/4" SAWCUT)
STA 845+00 TO STA 870+06.48	MODIFIED (1p) OR (13p) TRANSVERSE CONTRACTION JOINT AT 12' SPACING	MODIFIED (3) LONGITUDINAL BULKHEAD JOINT (SEALED JOINT WITH 1/4" SAWCUT)	MODIFIED (1) LONGITUDINAL LANE TIE JOINT (SEALED JOINT WITH 1/4" SAWCUT)

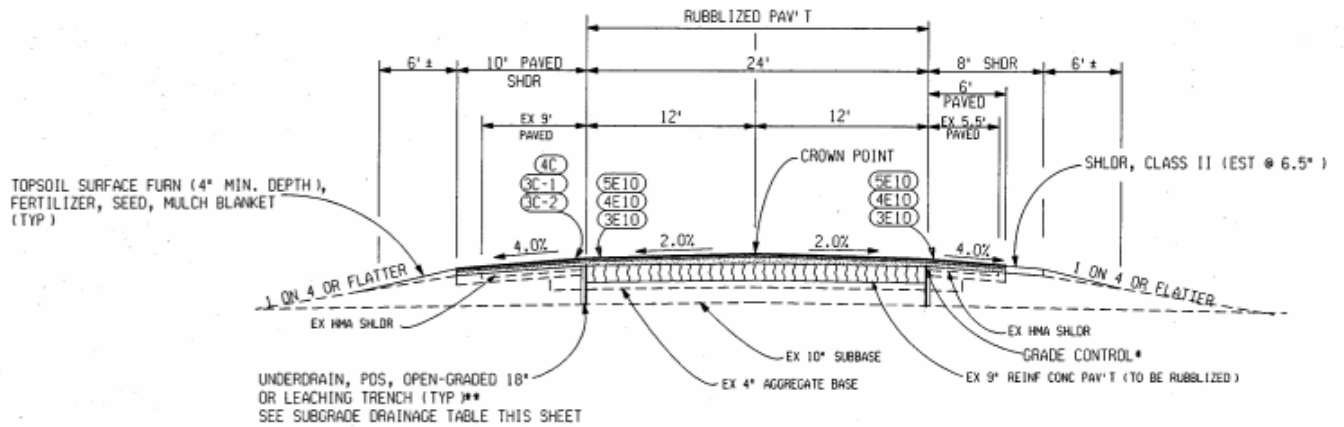
Typical Cross-Sections

Rubblize and Asphalt Overlay

Existing

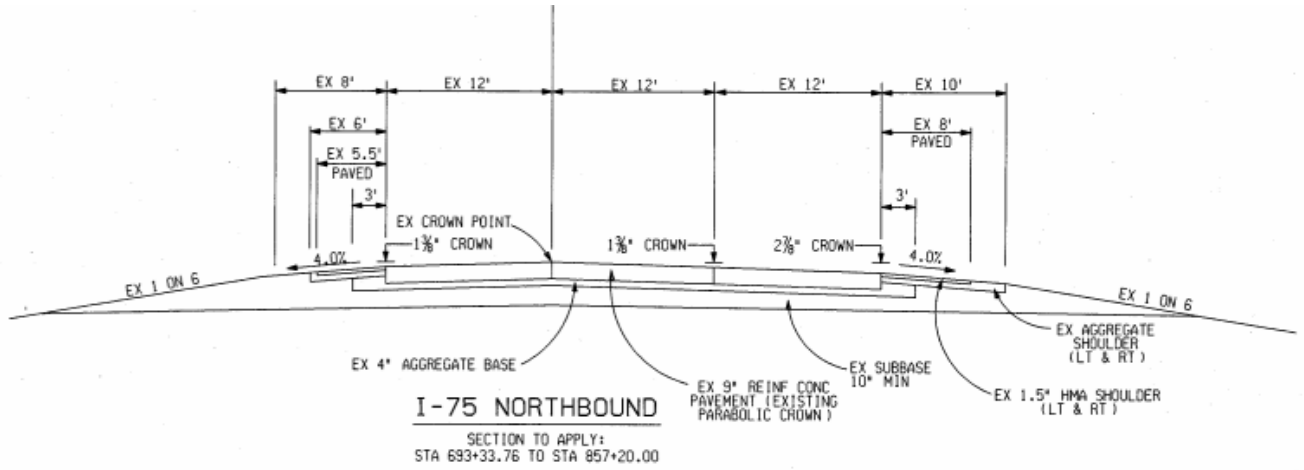


Proposed

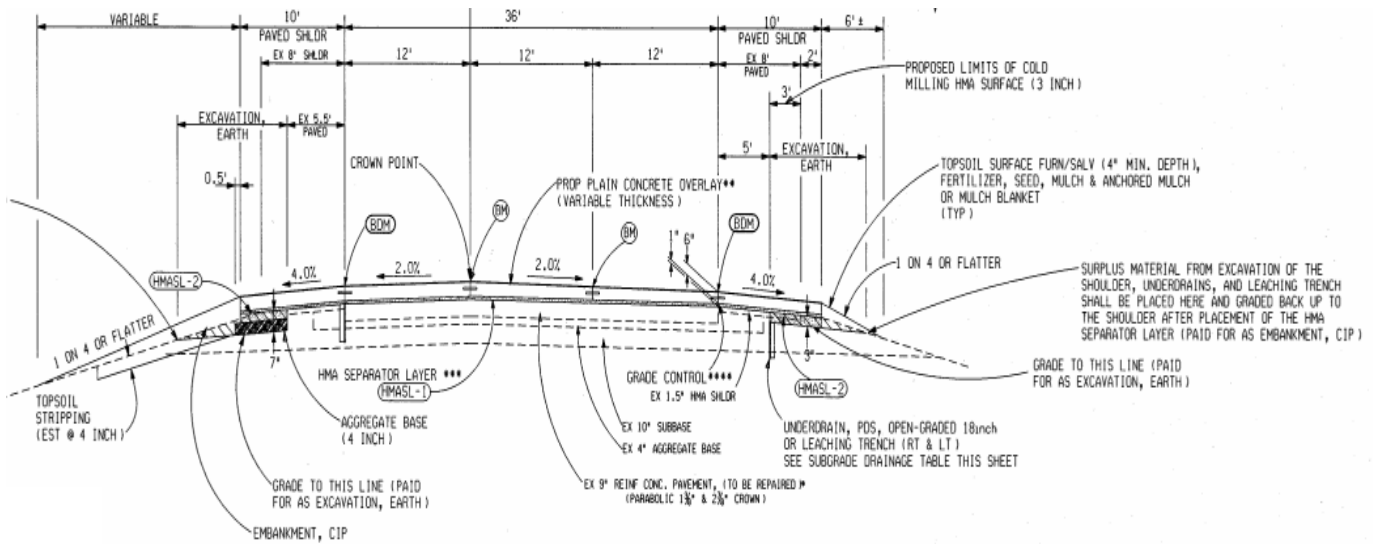


Unbonded Concrete Overlay

Existing

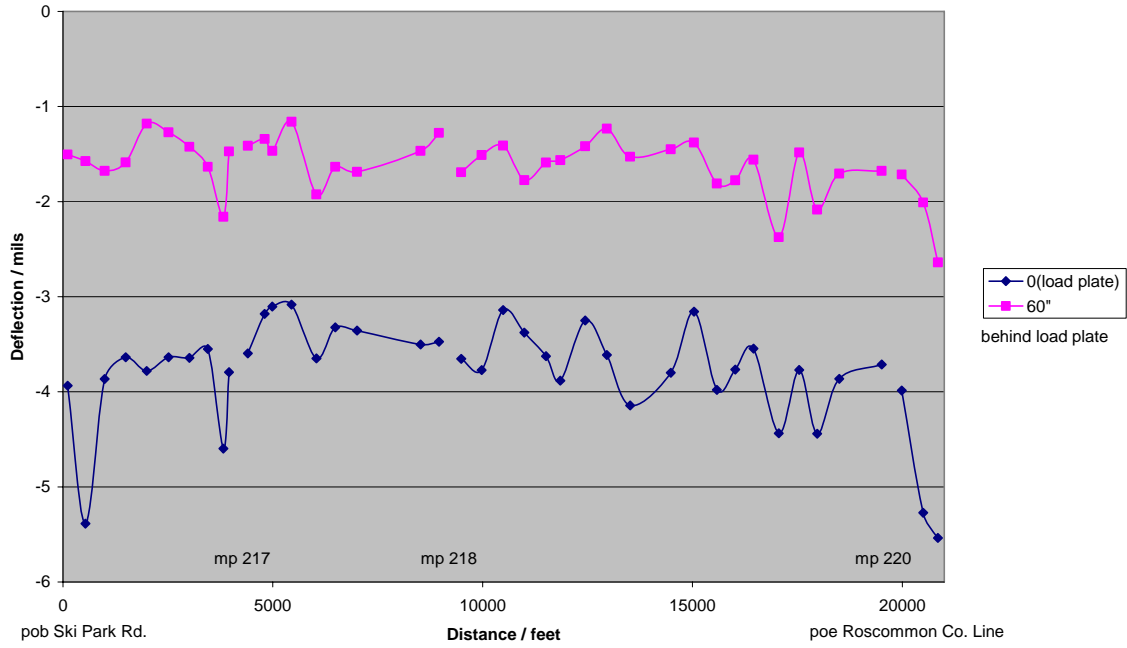


Proposed

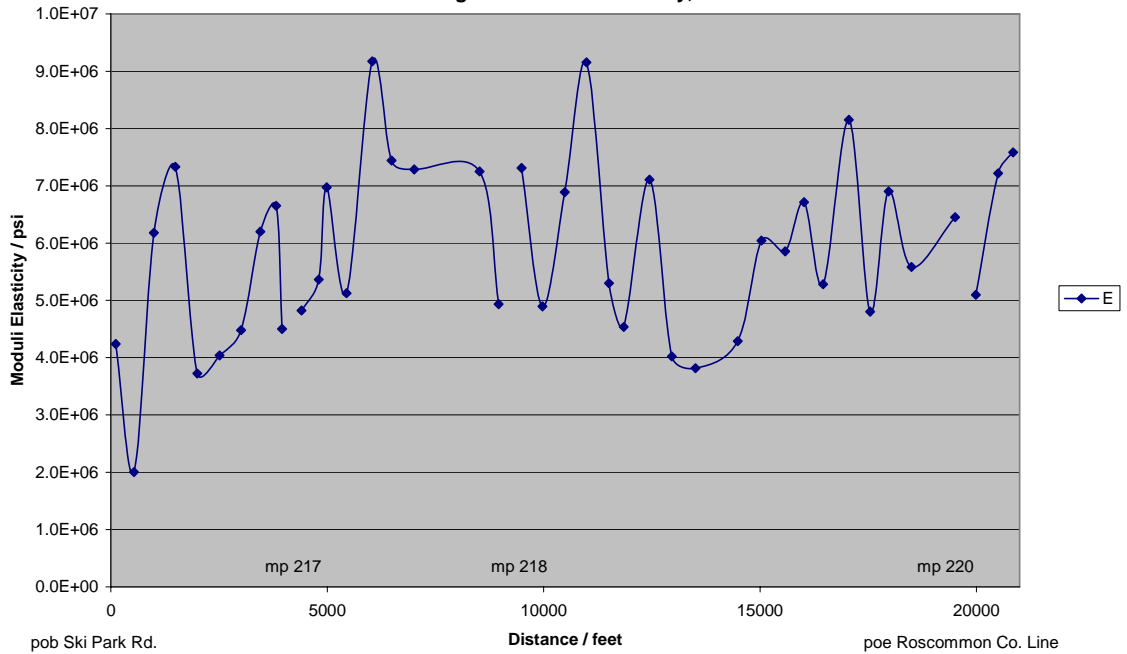


**FWD Results
Before Construction**

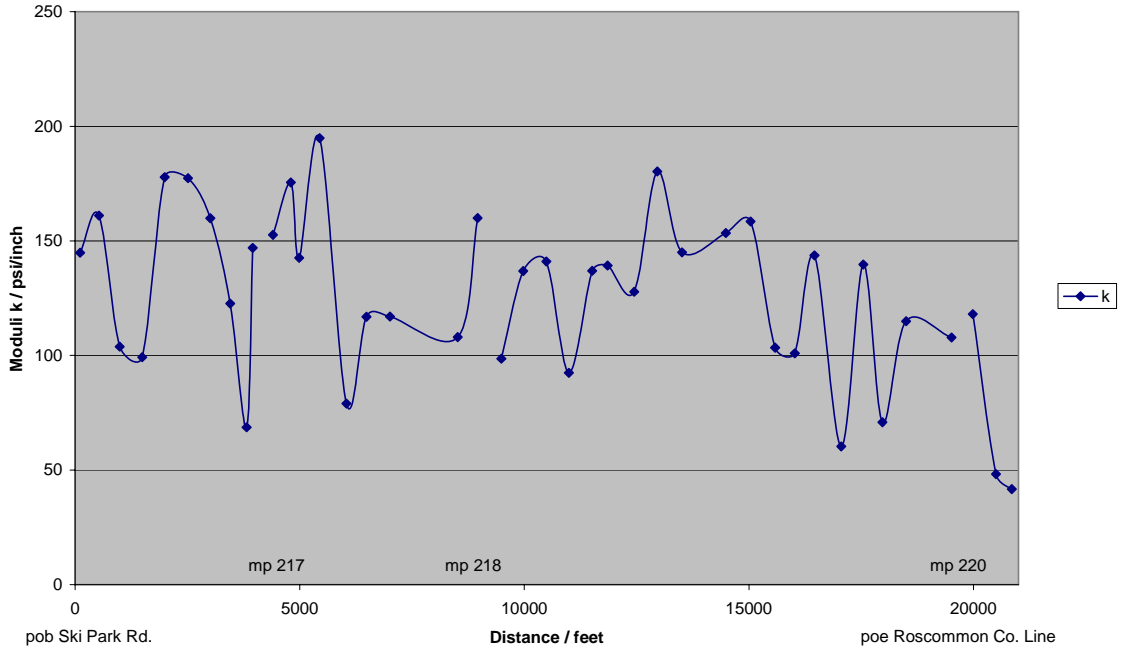
North Region CS 65042 JN 00947 I-75 NBOL
Average Maximum Deflection @ 9000 lbf @ 75 F



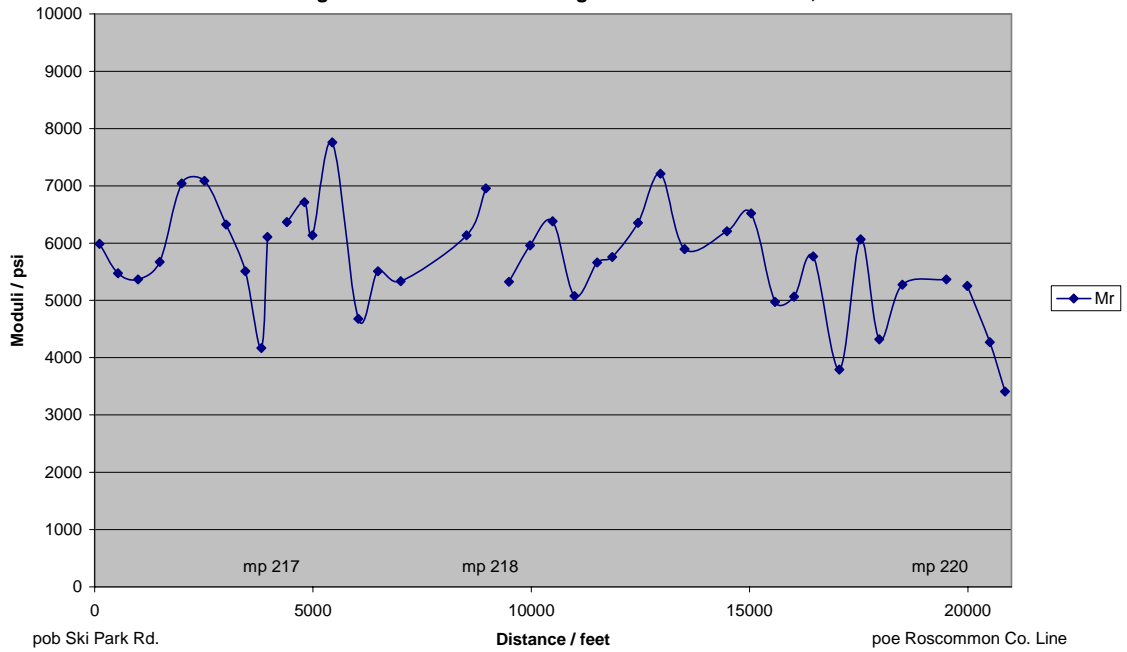
North Region CS 65041 JN 00947 I-75 NBOL
Average Modulus of Elasticity, E



North Region CS 65041 JN 00947 I-75 NBOL
Average Modulus of Subgrade Reaction Static k



North Region CS 65041 JN 00947 I-75 NBOL
Average AASHTO Corrected Subgrade Resilient Modulus, Mr

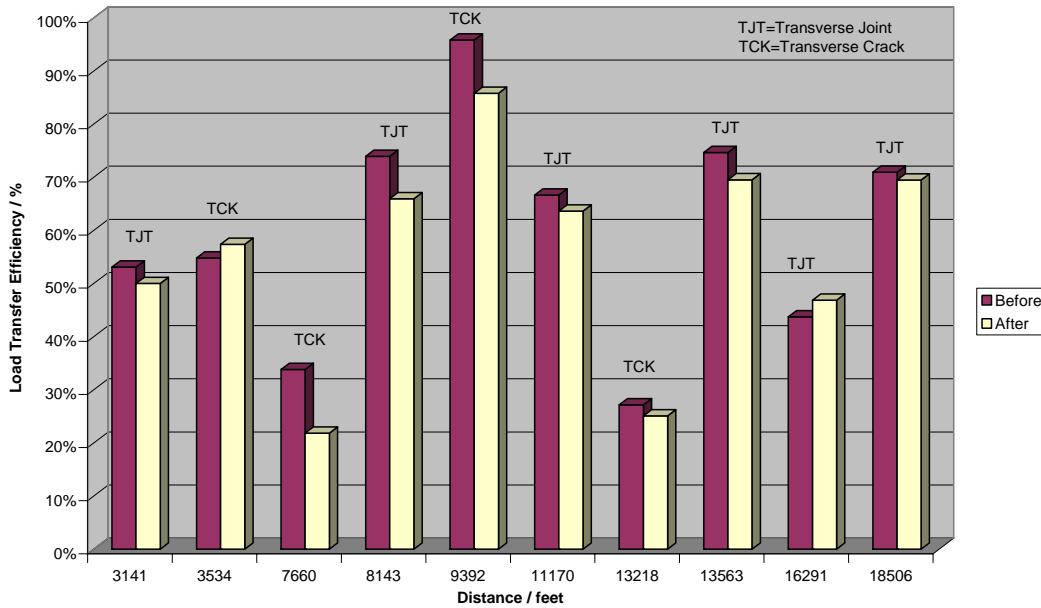


North Region CS 65041 JN 00947 I-75 NBOL
Transverse Joint/Crack Load Transfer Efficiency

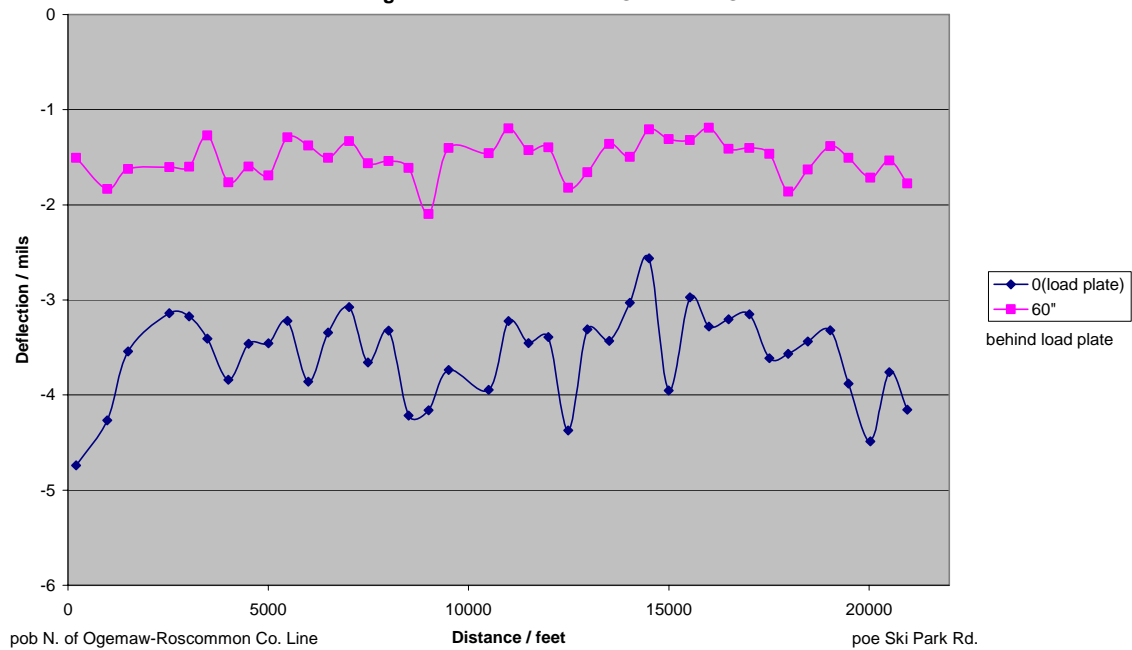
Distance ft	Load lbf	Load Plate D0 mils	12" Front D1 mils	12" Behind D4 mils	60" Behind D8 mils	Air øF	Pave øF	Test Type	Test Area	Pvmt Dstrs	Test Loc.	Transverse Joint/Crack Load Transfer Efficiency		
												Before	After	
0	pob Ski Park Road structure													
3141	9000	7.06	3.75	5.07	1.80	62	73	TJT	CUT	NA	BJT	53%	50%	
3142	9000	7.57	5.76	3.79	1.61	63	73	TJT	CUT	NA	AJT			
3534	9000	8.23	4.51	6.19	1.74	62	73	TCK	CUT	SPALL	BCK	55%		
3535	9000	8.55	6.40	4.90	1.67	62	72	TCK	CUT	FAULT	ACK		57%	
7660	9000	7.65	2.59	5.88	1.99	62	73	TCK	FILL	SPALL	BCK	34%		
7661	9000	13.12	10.16	2.87	1.32	63	73	TCK	FILL	FAULT	ACK		22%	
8143	9000	7.27	5.37	5.57	1.74	64	74	TJT	CUT	SPALL	BJT	74%		
8145	9000	7.44	5.94	4.90	1.73	64	75	TJT	CUT	SPALL	AJT		66%	
9392	9000	5.57	5.33	4.43	1.51	65	75	TCK	FILL	NA	BCK	96%		
9394	9000	6.07	4.80	5.21	1.67	65	75	TCK	FILL	FAULT	ACK		86%	
11170	9000	7.53	5.02	5.81	1.85	68	76	TJT	CUT	SPALL	BJT	67%		
11171	9000	8.53	6.42	5.43	1.80	68	77	TJT	CUT	SPALL	AJT		64%	
13218	9000	5.95	1.61	4.48	1.21	67	77	TCK	FILL	SPALL	BCK	27%		
13219	9000	8.20	6.11	2.06	0.82	67	77	TCK	FILL	FAULT	ACK		25%	
13563	9000	6.59	4.92	4.93	1.74	67	77	TJT	FILL	SPALL	BJT	75%		
13565	9000	6.89	5.24	4.79	1.69	66	76	TJT	FILL	SPALL	AJT		70%	
16291	9000	7.70	3.36	4.36	1.76	65	79	TJT	CUT	SPALL	BJT	44%		
16292	9000	6.98	4.92	3.27	1.54	65	79	TJT	CUT	SPALL	AJT		47%	
18506	9000	8.34	5.91	6.39	1.94	65	78	TJT	FILL	SPALL	BJT	71%		
18507	9000	8.46	6.56	5.88	1.95	64	78	TJT	FILL	SPALL	AJT		69%	
20899	poe Roscommon Co. Line													

	<u>Before</u>	<u>After</u>
TJT		
Average	64%	61%
Stdev.	0.13	0.10
Max	75%	70%
Min	44%	47%
C. of V.	0.20	0.16
TCK		
Average	53%	48%
Stdev.	0.31	0.30
Max	96%	86%
Min	27%	22%
C. of V.	0.59	0.63

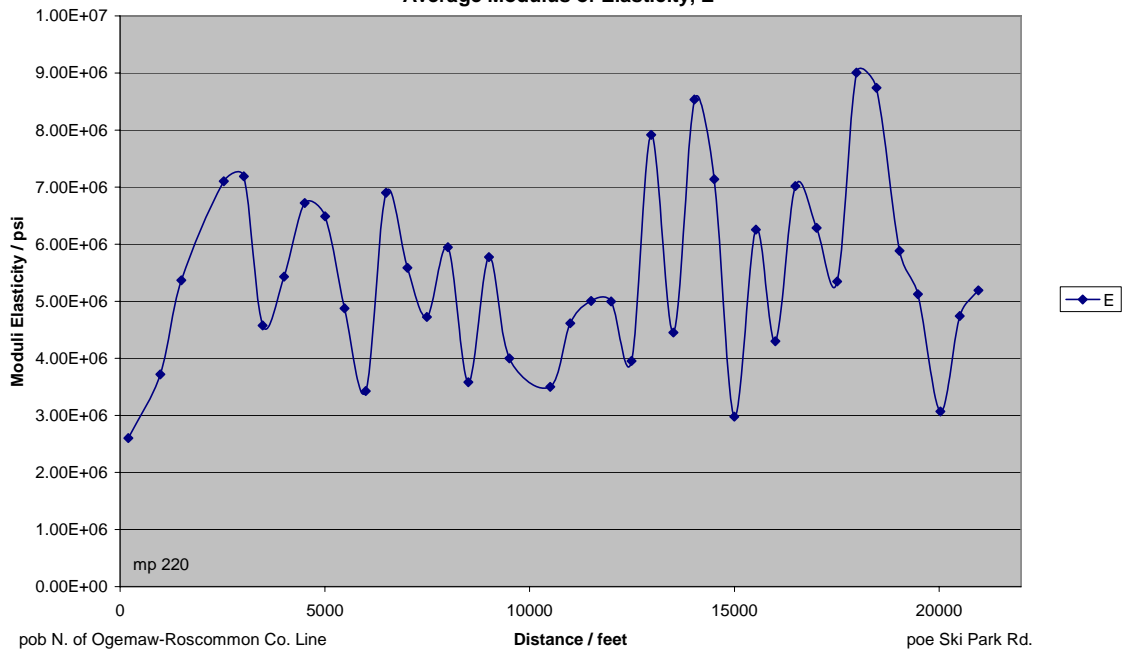
North Region CS 65041 JN 00947 I-75 NBOL
Random Transverse Joint/Crack Load Transfer Efficiencies, % @ 75 F



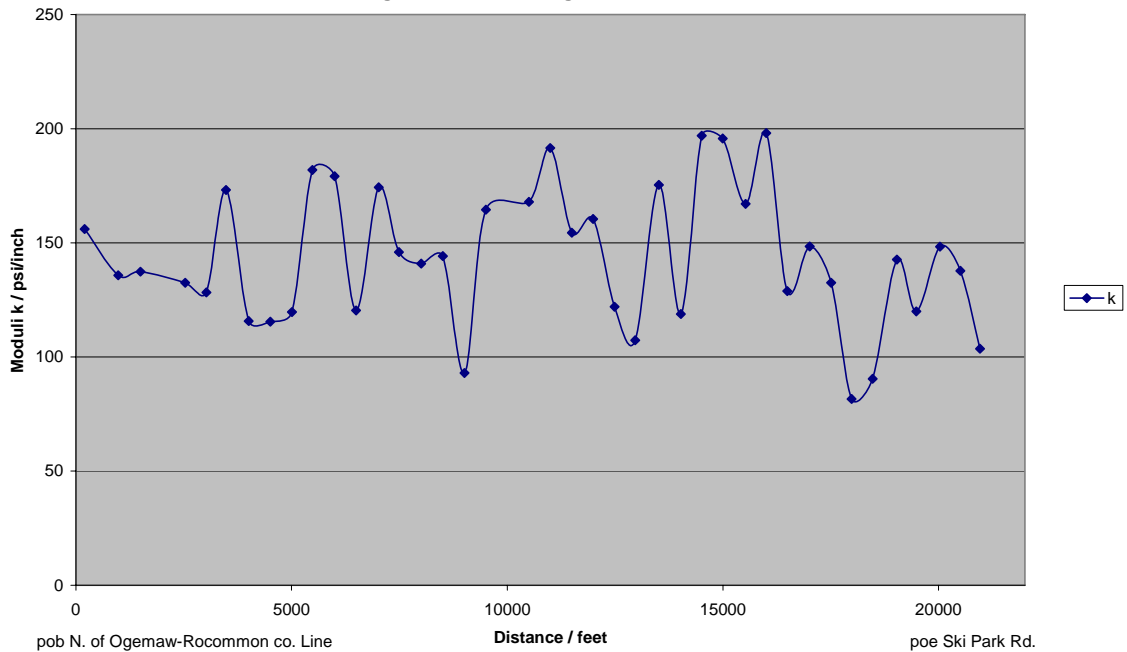
North Region CS 65041 JN 00947 I-75 SBOL
Average Maximum Deflection @ 9000 lbf @ 60 F



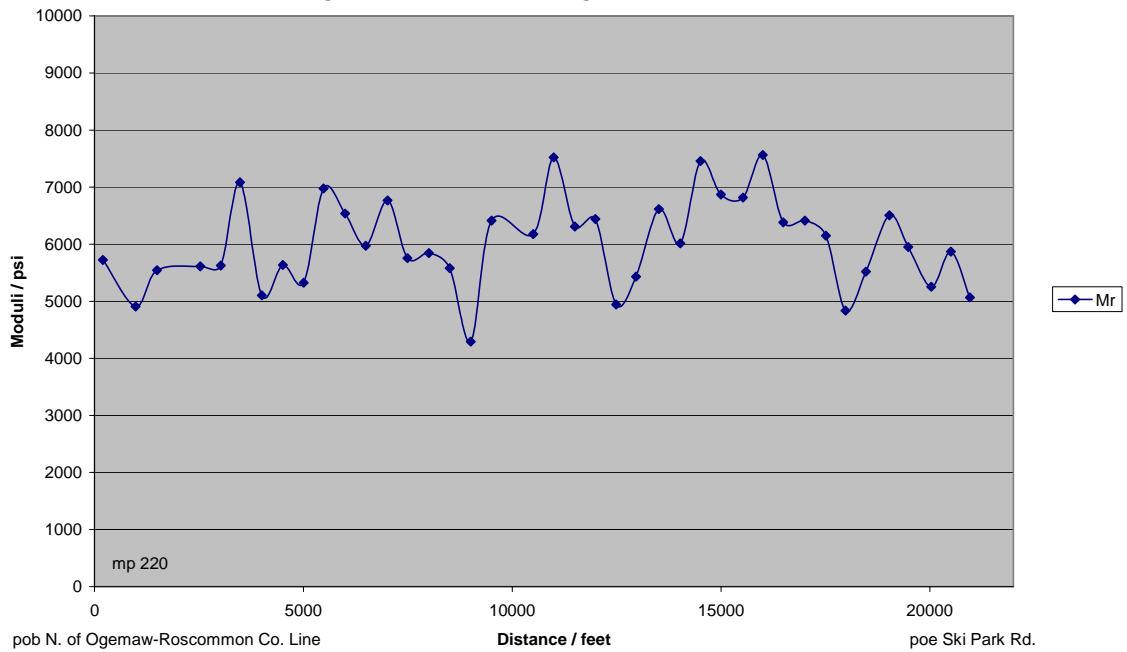
North Region CS 65041 JN 00947 I-75 SBOL
Average Modulus of Elasticity, E



North Region CS 65041 JN 00947 I-75 SBOL
Average Modulus of Subgrade Reaction Static k



North Region CS 65041 JN 00947 I-75 SBOL
Average AASHTO Corrected Subgrade Resilient Modulus, Mr

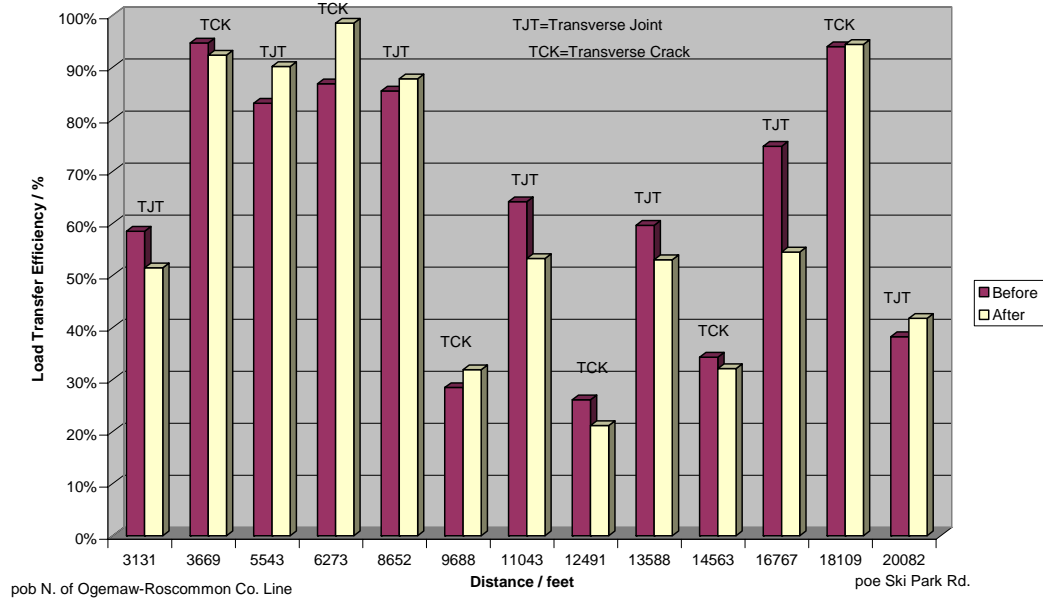


**North Region CS 65041 JN 00947 I-75 SBOL
Transverse Joint/Crack Load Transfer Efficiency**

Distance ft	Load lbf	Load Plate D0 mils	12" Front D1 mils	12" Behind D4 mils	60" Behind D8 mils	Air øF	Pave øF	Test Type	Test Area	Pvmt Dstrs	Test Loc.	Transverse Joint/Crack Load Transfer Efficiency		
0	pob N. of Ogemaw-Roscommon Co.Line													
3131	9000	16.32	9.55	11.95	3.91	43	51	TJT	CUT	NA	BJT	59%		
3132	9000	18.32	14.17	9.43	3.53	44	52	TJT	CUT	NA	AJT		51%	
3669	9000	7.17	6.79	5.63	1.73	44	51	TCK	CUT	FAULT	BCK	95%		
3670	9000	7.17	5.73	6.62	1.99	44	52	TCK	CUT	MID	ACK		92%	
5543	9000	10.48	8.71	8.31	2.47	49	54	TJT	CUT	NA	BJT	83%		
5544	9000	9.68	7.68	8.72	2.80	48	55	TJT	CUT	NA	AJT		90%	
6273	9000	9.73	8.45	7.58	2.09	50	56	TCK	FILL	SPALL	BCK	87%		
6274	9000	8.54	6.86	8.41	2.55	50	55	TCK	FILL	MID	ACK		98%	
8652	9000	11.86	10.13	9.38	2.87	51	56	TJT	CUT	SPALL	BJT	85%		
8653	9000	11.38	9.04	9.99	3.22	51	58	TJT	CUT	SPALL	AJT		88%	
9688	9000	7.80	2.22	5.88	1.93	50	58	TCK	CUT	SPALL	BCK	28%		
9689	9000	8.03	5.91	2.56	1.23	51	59	TCK	CUT	SPALL	ACK		32%	
11043	9000	9.41	6.04	7.09	2.06	51	60	TJT	CUT	NA	BJT	64%		
11044	9000	10.17	7.84	5.41	1.83	52	59	TJT	CUT	NA	AJT		53%	
12491	9000	7.61	1.99	6.03	2.08	52	60	TCK	CUT	SPALL	BCK	26%		
12492	9000	9.80	7.47	2.07	1.14	52	60	TCK	CUT	MID	ACK		21%	
13588	9000	6.96	4.15	5.21	1.54	52	65	TJT	FILL	SPALL	BJT	60%		
13589	9000	7.24	5.04	3.84	1.39	53	64	TJT	FILL	SPALL	AJT		53%	
14563	9000	7.15	2.45	5.35	1.62	54	63	TCK	CUT	SPALL	BCK	34%		
14564	9000	7.34	5.54	2.36	1.12	54	61	TCK	CUT	SPALL	ACK		32%	
16767	9000	6.67	4.99	5.07	1.53	54	64	TJT	FILL	NA	BJT	75%		
16768	9000	7.47	5.83	4.07	1.37	54	64	TJT	FILL	NA	AJT		55%	
18109	9000	4.73	4.45	4.04	1.80	56	68	TCK	CUT	SPALL	BCK	94%		
18110	9000	4.56	3.96	4.31	1.84	55	67	TCK	CUT	SPALL	ACK		94%	
20082	9000	10.40	3.98	5.50	1.80	56	67	TJT	CUT	SPALL	BJT	38%		
20084	9000	8.20	6.11	3.42	1.43	55	65	TJT	CUT	SPALL	AJT		42%	
21140	poe Ski Park Rd.													

	<u>Before</u>	<u>After</u>
TJT		
Average	66%	62%
Stdev.	0.16	0.19
Max	85%	90%
Min	38%	42%
C. of V.	0.25	0.31
TCK		
Average	61%	62%
Stdev.	0.34	0.37
Max	95%	98%
Min	26%	21%
C. of V.	0.56	0.60

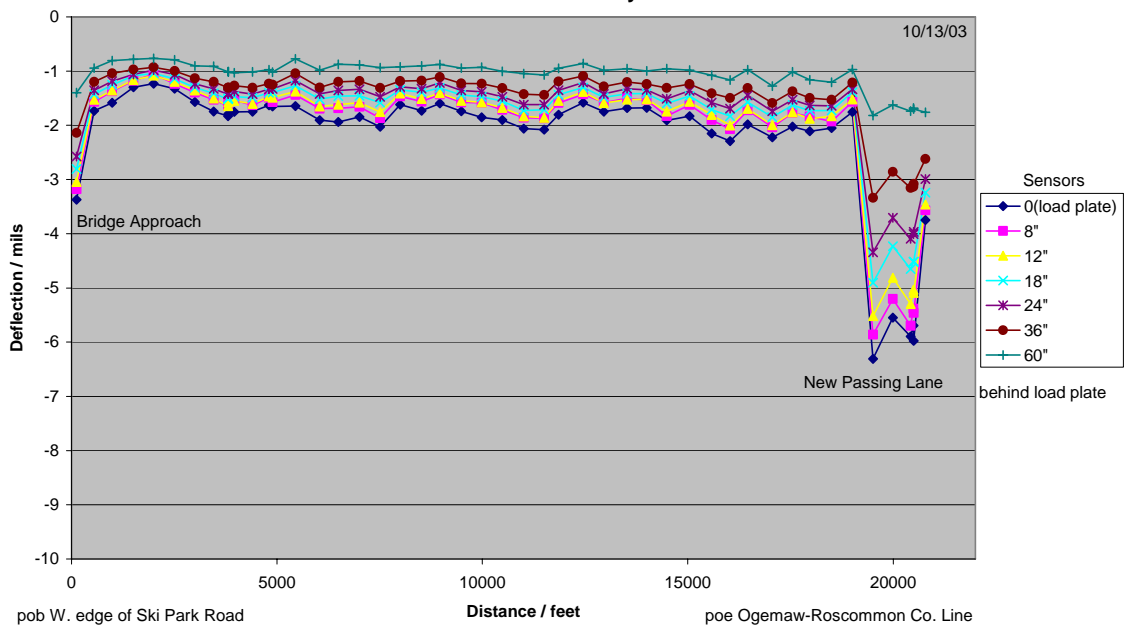
**North Region CS 65041 JN 00947 I-75 SBOL
Random Transverse Joint/Crack Load Transfer Efficiencies, % @ 59 F**



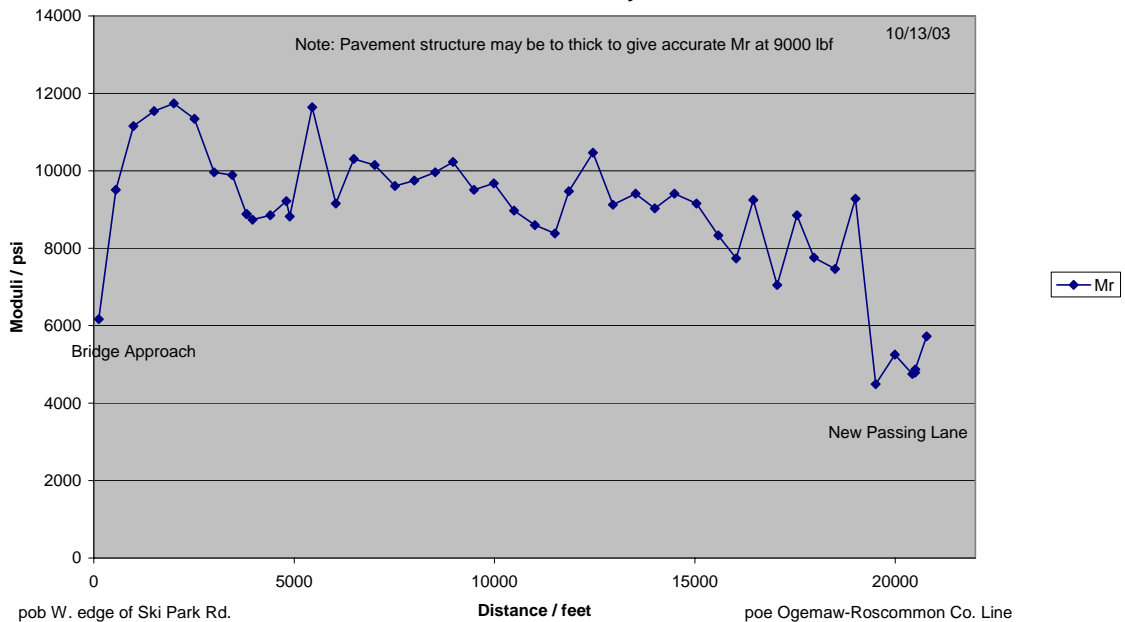
**FWD Results
After Construction**

11506	9000	2.08	1.86	1.75	1.87	1.86	1.71	1.62	1.44	1.07	78	78	NBPL	MD	CUT	NEW	14:11	6109		
11855	9000	1.80	1.58	1.52	1.59	1.55	1.44	1.35	1.19	0.95	79	79	NBPL	MD	CUT	NEW	14:13	5556		
11859	9000	2.23	1.93	1.89	1.93	1.88	1.70	1.58	1.42	1.01	79	81	NBPL	TJT	CUT	BJT	14:15		87%	
11860	9000	2.16	1.85	1.83	2.06	1.93	1.75	1.63	1.42	1.03	79	81	NBPL	TJT	CUT	AJT	14:16		89%	
12454	9000	1.58	1.37	1.32	1.43	1.38	1.30	1.21	1.09	0.86	77	78	NBPL	MD	FILL	NEW	14:19	5556		
12557	9000	1.75	1.54	1.47	1.58	1.59	1.49	1.42	1.28	0.99	78	80	NBPL	MD	FILL	NEW	14:21	6650		
13522	9000	1.68	1.51	1.45	1.50	1.53	1.42	1.32	1.20	0.96	77	78	NBPL	MD	FILL	NEW	14:24	5684		
14001	9000	1.68	1.49	1.44	1.54	1.52	1.41	1.35	1.24	1.00	76	78	NBPL	MD	FILL	NEW	14:26	5510		
14490	9000	1.91	1.62	1.62	1.83	1.75	1.60	1.51	1.31	0.96	75	81	NBPL	MD	FILL	NEW	14:29	7438		
14496	9000	1.85	1.58	1.58	1.71	1.71	1.59	1.49	1.30	0.97	75	80	NBPL	TJT	FILL	BJT	14:30		86%	
14497	9000	1.77	1.50	1.49	1.59	1.60	1.54	1.45	1.28	0.96	77	80	NBPL	TJT	FILL	AJT	14:32		90%	
15042	9000	1.83	1.54	1.51	1.62	1.57	1.46	1.36	1.24	0.98	78	81	NBPL	MD	GRADE	NEW	14:35	6338		
15583	9000	2.15	1.92	1.82	1.90	1.81	1.71	1.58	1.41	1.08	77	78	NBPL	MD	CUT	NEW	14:37	6801		
16027	9000	2.29	2.11	1.99	2.07	2.00	1.83	1.69	1.50	1.16	78	79	NBPL	MD	CUT	NEW	14:39	6683		
16458	9000	1.98	1.70	1.64	1.72	1.70	1.57	1.45	1.31	0.97	78	83	NBPL	MD	CUT	NEW	14:41	5960		
17056	9000	2.22	1.93	1.88	2.04	2.00	1.85	1.74	1.59	1.28	77	83	NBPL	MD	CUT	NEW	14:43	6040		
17551	9000	2.02	1.81	1.71	1.77	1.76	1.63	1.53	1.37	1.02	78	81	NBPL	MD	GRADE	NEW	14:45	6221		
17970	9000	2.11	1.80	1.73	1.84	1.88	1.73	1.63	1.50	1.16	79	80	NBPL	MD	FILL	NEW	14:47	6601		
18499	9000	2.05	1.85	1.75	1.93	1.83	1.73	1.64	1.53	1.21	79	79	NBPL	MD	GRADE	NEW	14:51	5684		
19005	9000	1.76	1.48	1.47	1.57	1.52	1.39	1.34	1.21	0.97	79	83	NBPL	MD	CUT	NEW	15:01	5315		
19500	pob new passing lane?																			
19511	9000	6.31	5.46	5.34	5.86	5.52	4.90	4.34	3.34	1.82	78	81	NBPL	MD	CUT	NEW	15:05	9534		
19992	9000	5.55	4.80	4.64	5.20	4.81	4.23	3.71	2.86	1.62	79	82	NBPL	MD	CUT	NEW	15:11	8106		
20426	9000	5.90	5.00	5.04	5.70	5.30	4.65	4.09	3.16	1.74	78	78	NBPL	MD	FILL	NEW	15:17	9221		
20496	9000	5.69	4.97	4.86	5.38	5.04	4.52	4.01	3.13	1.68	76	78	NBPL	MD	FILL	NEW	15:14	8671		
20501	9000	5.98	5.20	5.08	5.46	5.09	4.51	3.97	3.08	1.70	77	78	NBPL	MD	FILL	NEW	15:15	8696		
20783	9000	3.75	3.41	3.38	3.57	3.46	3.24	2.99	2.62	1.76	77	83	NBPL	MD	FILL	NEW	15:22	10791		
20873	poe concrete overlay																			
Average	9000	2.28	NA	NA	2.08	2.01	1.84	1.71	1.48	1.07	78	78							6852	
Stdev.		1.28	NA	NA	1.23	1.13	0.98	0.85	0.61	0.27	1	3							1302	
Max.		6.31	NA	NA	5.86	5.52	4.90	4.34	3.34	1.82	81	83							10791	
Min.		1.23	NA	NA	1.06	1.08	1.04	0.98	0.93	0.77	73	69							3353	
C. of V.		56%	NA	NA	59%	56%	53%	50%	41%	25%	2%	4%							19%	
Additional Tests																				
	pob NBCL adj. to new passing lane																			
19511	9000	2.16	1.88	1.81	1.96	1.86	1.72	1.62	1.44	1.12	79	83	NBCL	MD	CUT	NEW	15:38	8060		
19986	9000	2.08	1.71	1.76	1.92	1.84	1.67	1.58	1.43	1.07	79	83	NBCL	MD	CUT	NEW	15:41	8411		
20501	9000	2.22	1.91	1.88	2.02	1.91	1.80	1.68	1.53	1.16	77	80	NBCL	MD	CUT	NEW	15:44	7736		
20783	9000	2.92	2.65	2.62	2.80	2.72	2.49	2.31	2.01	1.40	77	84	NBCL	MD	FILL	NEW	15:48	6429		
	poe NBCL adj. to new passing lane																			
	pob new passing lane by station																			
85753	9000	5.69	5.07	4.94	5.54	5.15	4.55	3.98	2.99	1.62	77	81	NBPL	MD	CUT	NEW	16:13	5017		
86008	9000	5.54	4.88	4.75	5.27	4.92	4.40	3.92	3.08	1.77	78	80	NBPL	MD	CUT	NEW	16:15	4875		
86259	9000	5.39	4.75	4.63	5.05	4.78	4.24	3.76	2.92	1.63	78	76	NBPL	MD	CUT	NEW	16:18	5143		
86264	9000	5.85	5.10	5.02	5.39	5.04	4.43	3.89	3.01	1.68	79	78	NBPL	TJT	CUT	BJT	16:21	4978		
86265	9000	5.83	5.01	5.00	5.60	5.22	4.58	4.01	3.10	1.71	77	77	NBPL	TJT	CUT	AJT	16:23	4844		
86513	9000	5.94	5.18	5.00	5.54	5.18	4.60	4.07	3.13	1.78	76	80	NBPL	MD	GRADE	NEW	16:25	4792		
86753	9000	5.33	4.62	4.54	5.04	4.65	4.18	3.71	2.88	1.61	77	82	NBPL	MD	GRADE	NEW	16:27	5208		
87000	9000	5.95	5.10	4.96	5.53	5.22	4.59	4.04	3.10	1.65	77	82	NBPL	MD	GRADE	NEW	16:30	4834		
87210	9000	4.17	3.78	3.70	3.94	3.84	3.51	3.24	2.70	1.73	78	83	NBPL	MD	FILL	NEW	16:33	5202		
	poe new passing lane by station																			

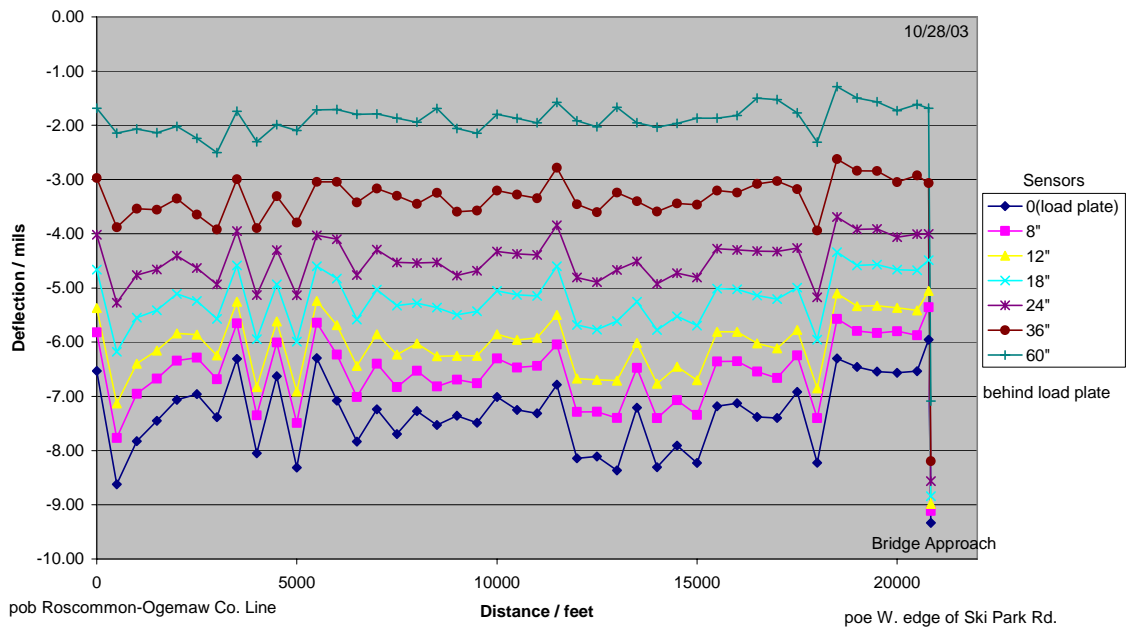
North Region CS 65041 I-75 NB Passing Lane
Average Maximum Deflection @ 9000 lbf @ 78 F
Concrete Overlay



North Region CS 65041 I-75 NB Passing Lane
Average AASHTO Corrected Subgrade Resilient Modulus, Mr
Concrete Overlay



North Region CS 65041 I-75 SBOL
Average Maximum Deflection @ 9000 lbf @ 47 F
Flexible Pavement



North Region CS 65041 I-75 SBOL
Average AASHTO Corrected Subgrade Resilient Modulus, Mr
Flexible Pavement

