

# MICHIGAN DEPARTMENT OF TRANSPORTATION

# An Evaluation of Concrete Median Barrier in Michigan

TSD 531-83

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## Disclaimer

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The contents of this report reflect the views of the authors who are responsible for the facts and the accuracy of the data presented. The contents do not necessarily reflect the official views or policies of the Michigan Department of Transportation.

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# ABSTRACT

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The accident experience before and after concrete median barrier (CMB) installations on Michigan roadways was examined in terms of accidents/mile, percentage of total accidents, severity ratio, single vehicle and multivehicle accidents, and fatal accidents. The effects of various roadway characteristics (i.e. alignment, shoulder slope, glare screen, curb/shoulder type, ADT, and lanes) on the number of injury and fatal CMB accidents were investigated. Finally, the effect of vehicle weight class on CMB accident severity was investigated.

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#### BACKGROUND

The safety benefits of guardrail and median barrier have been the subject of many studies. Generally, it has been found that fatal accidents remained the same or decreased slightly after barrier installation, and that injury and property damage accidents increased substantially. -1' The decrease in fatal accidents was due to the reduction of cross-median accidents which, according to a 1958 California study, -1' accounted for 19 percent of all fatalities on freeways in a three-year period. The increase in injury and property damage accidents was attributed to the median barrier being "...a fixed-object struck by out-of-control vehicles that might have recovered without incident if the barrier had not been installed."

Concrete median barrier (CMB) replaced the traditional steel beam guardrail on many sections of highway during the last few years. CMB is virtually maintenance-free compared to steel beam guardrail. Also, the shape of CMB is designed to cause less property damage than steel beam guardrail accidents and more safely redirect vehicles which leave the road. A 1979 Michigan study 4/ assessed whether snow accumulation along CMB installations was a problem. The author concluded, from analysis of winter accident data for 1971/72 through 1975/76 and a survey of district traffic and maintenance engineers, that accumulated snow along CMB did not present a hazard to motorists. Ten rollover and six cross-median accidents occurred in that five-winter study period. These 16 accidents were seven percent of total CMB accidents and no fatalities were involved. The study also noted that six of the ten rollover accidents involved "compact" cars.

Many experimental crash tests have been conducted with CMB to determine which barrier shape would permit drivers to regain control of their vehicles after striking the barrier and return to the roadway with a minimum of damage. A report published by the Federal Highway Administration in 1976  $\frac{5}{}$  recommended use of the New Jersey shape. It was based on standardized crash tests performed on the New Jersey and GM shapes using various vehicles ranging in size from a compact car to an intercity bus.

A British study conducted in 1977  $\frac{6}{}$  crashed a European subcompact car and a bus into various CMB shapes. The results also indicated the superiority of the New Jersey shape.

Accident experience before-and-after installation of CMB is not well documented. Early studies of the effectiveness of CMB in New Jersey  $\frac{7}{2}$  reported dramatic reductions in injury and fatal accidents after installation.  $\frac{9}{2}$  A study of various safety improvements on approximately five miles of I-75 in northern Kentucky found New Jersey-type CMB to be effective in reducing the overall accident rate.  $\frac{10}{12}$  Two preliminary accident studies  $\frac{11}{12}$  were done in Michigan; however, both studies were inconclusive.

## INTRODUCTION

The first standard plan for CMB in Michigan was approved by the Department of Transportation on May 30, 1974. CMB had been used, however, with various modifications as a special detail since late 1970.  $\frac{13}{2}$  Since then, the use of CMB has increased from 89 miles in 1976 to approximately 140 miles by 1979.

The majority of CMB along Michigan's freeway system was installed prior to 1976 and is the GM-type shape. Since May, 1976, only New Jersey-type has been installed on the state's freeways. This shape has a slightly steeper top face than the GM-type and was found to perform better in small car contacts.  $\underline{14/7}$ 

The median width of the study cross sections was unknown. Medians with CMB installed are less than 36-feet wide. Typically, CMB is used only where median width is less than 30 feet. For medians 30 to 60 feet wide, steel beam guardrail is normally used if a median barrier is required. Concrete glare screen is used on CMB where headlight glare may prove distracting.

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This study attempts to evaluate the relationship between CMB installation and accident severity (injury and fatal accidents) and between CMB accident severity and roadway alignment, shoulder characteristics, glare screen, average daily traffic, lanes, and vehicle size. Specifically, the study seeks to answer the following questions:

- 1. How does CMB accident severity compare with the "before" period accident severity on roadways where CMB has replaced guardrail or grass median?
- 2. Are there more secondary collisions (i.e. vehicles striking other vehicles after contacting the median barrier) when CMB replaces guardrail?
- 3. Does fatal accident experience change when CMB is installed in place of guardrail or grass medians?
- 4. Are there any roadway or traffic characteristics which have a particular influence on CMB accident severity?
- 5. Does vehicle weight influence CMB accident severity?

The answers to these and several other questions which arose in the course of the study are detailed in the Conclusions section on pages 12-14.

### PROCEDURE

CMB projects were located using the Construction Division's computer files. The locations from this file were verified using the two preliminary CMB studies  $\frac{11}{12}$  and the department's photolog.

The photolog was also used to gather the following information concerning the roadway and CMB:

- 1. Beginning and Ending Mileages.
- 2. Horizontal Alignment.
- 3. Shoulder Slope.
- 4. Glare Screen Presence and Type.
- 5. Curb Type/Shoulder Width.
- 6. Number of Lanes (one direction).
- 7. "Before" CMB Condition (Since the first photolog inventory was completed in 1974/75 the "before" condition was unavailable for CMB segments installed prior to 1975. These 43 segments totalled 48 miles.)
  - a. Grass
  - b. Guardrail (The guardrail type was unknown. An analysis of the relative performance of the various guardrail types was beyond the scope of this study.)

CMB installation dates were obtained from Construction Division records. It was not possible to determine the CMB shape (i.e. New Jersey or GM) from the photolog. Since prior work using crash tests has demonstrated the relative merits of the various CMB shapes, a further evaluation using accident data would contribute little new information.

Accident experience was obtained for the following three groups:

- 1. Group I (30 miles) had steel beam guardrail median barrier prior to CMB installation. The locations in this group had CMB installed in 1975 or later.
- 2. Group II (18 miles) had grass median with no barrier prior to CMB installation. The locations in this group had CMB installed in 1975 or later. About 50 percent of the mileage had an additional lane in each direction added on the median side of the roadway at the time CMB was installed. Hence the median was considerably narrowed.
- 3. Group III (94 miles) consisted of the locations in Groups I and II and additional segments with CMB installed as early as 1974 for which the "before" period median treatment was unavailable from the photolog. Reviewing the construction plans to obtain this information would not provide compatible milepoints for obtaining accident experience.

### ACCIDENT EXPERIENCE

The actual numbers of guardrail and CMB accidents were not of central concern in this analysis. The likelihood of a collision resulting in an injury or fatality was what this study attempted to assess. Accident occurrence is strongly influenced by median width, an analysis of which was beyond the scope of this study. In addition, the problem of unreported accidents adds uncertainty to accident numbers. (See reference 11 for an attempt to analyze the unreported accident problem and reference 1 for a median barrier collision probability model.) Severity ratios were used to reflect changes in the number of injury and fatal accidents before and after the CMB installations. It was still instructive, however, to examine the history of total accidents and total guardrail and CMB accidents at the study locations.

The somewhat unconventional term of "accidents per mile" was used to relate accidents to the number of miles of barrier. Traditional accident rates (per 100 MVM) would have been highly variable since the study locations were short segments of urban freeways with variable ADTs. In addition, the number of lanes was variable. The distribution of traffic across lanes may influence accident occurrence since many barrier accidents were caused by improper lane changes.

Although ADT on two roadway segments doubled between 1971 and 1981, the typical increase was much less, with some segments experiencing lower volumes. The overall change for all study segments from 1971 to 1981 was an increase of three percent.

<u>Total Accidents</u> - For Group I, total accidents increased from 22 accidents per mile in 1971 to a peak of 92 in 1976. The number declined to 50 accidents per mile in 1981. The Group II rate showed a similar trend with peaks in 1973 and 1977 of 21 and 18, respectively. The rate then declined to a low of 11 accidents per mile in 1981. The differences between Groups I and II may have been due to differences in median width since those medians without barriers were generally wider; however, about one-half of the Group II mileage had considerably narrower medians after CMB installation since additional lanes were built within the median. Many factors may influence the difference in rates between groups, and a detailed discussion of these factors was beyond the scope of this report.

An attempt was made to model total accident experience by a straight line. A regression analysis was performed with total accidents as the dependent variable and time the independent variable. The calculated line accounted for only 0.7 percent of the variance in total accidents. The conclusion was that the total accident experience at the study locations for the period 1971-1981 could not be modelled by a single increasing or decreasing straight line.

#### Guardrail and CMB Accidents

Left-side guardrail accidents in Group I (steel beam guardrail in the median initially) averaged 2.7 per mile per year in the period before CMB installation (1971-1975). CMB accidents in Group I averaged 4.5 per mile per year in the "after" period (1976-1981). A Group II (grass medians in the "before" period) accident type corresponding to barrier-related accidents was the head-on and sideswipe-opposite direction accident which averaged 0.6 per mile per year in the period before CMB installation (1971-1975). Total CMB accidents in Group II averaged 1.7 per mile per year in the "after" period (1976-1981).

The complete data are shown in Table A of the appendix. Several irregularities were apparent. A small number of left-side guardrail accidents occurred in the Group I "after" period. These were presumed to involve guardrail around bridge piers, etc., and/or coding errors. They numbered about 0.8 accidents per mile. Secondly, head-on and sideswipe-opposite direction accidents should have included all cross-median barrier accidents. A check of accident reports indicated they did not. They included miscellaneous accidents involving vehicles losing trailers, wheels, tires, etc. These numbered about 0.3 accidents per mile. Presumably, when median barriers are absent, such as in Group II, the cross-median accidents are included in this category.

Table A also shows the percentage of total accidents that were median barrier related for the study groups for each year. Four things were apparent:

- 1. The percentage of accidents involving the median or median barriers was low. Rear-end accidents, in comparison, accounted for an average of 61 percent of Group I accidents and 42 percent of Group II accidents.
- 2. For Group I the 1981 <u>CMB</u> accident percentage was similar to the 1971-72 guardrail accident percentage.
- 3. Group II, despite having fewer CMB accidents per mile than Group I, had a similar percentage of CMB accidents in 1981.
- 4. For Group II, the head-on and sideswipe-opposite direction accident percentage showed a sharp decline in 1976 as CMB was installed.

<u>Severity Ratio</u>: (The ratio of injury and fatal accidents to total accidents.) The Group I severity ratio for left-side guardrail accidents in the period before CMB installation was 0.37. The severity ratio for <u>CMB</u> accidents in the "after" period was 0.47.

For Group II, the severity ratio for head-on and sideswipe-opposite accidents in the period before CMB installation was 0.57<sup>°</sup>. The severity ratio for CMB accidents in the "after" period was 0.43.

None of these differences was significant at the 95 percent confidence level based on the log - likelihood test (see appendix).

\* The "after" period head-on and sideswipe-opposite severity ratio was also 0.57; however, this figure was based on a sample of seven accidents, whereas the "before" period severity ratio was based on 30 accidents. The severity ratio further confirmed that many of these were not the high severity accident expected from a head-on, or sideswipe-opposite direction collision.

The analysis of severity ratio was complicated by the problem of unreported accidents. A 1973 study  $\frac{15}{12}$  indicated that less than half of CMB collisions result in reported accidents. This would tend to distort the severity ratio of CMB accidents making it as much as twice as high. (For example, with 44 injury accidents out of 100 reported accidents the severity ratio is 0.44. However, if there were an additional 100 unreported noninjury accidents the true severity ratio would be 0.22). It was assumed that guardrail accidents were more likely to be reported since the vehicle was less likely to be drive-able.

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Because of the unreported accident problem, the number of injury and fatal accidents per mile per year was analyzed to provide information concerning the effects of CMB installation beyond an analysis of the severity ratio. With injury and fatal accidents, the problem of unreported accidents was greatly reduced since it was assumed that the nonreported accidents seldom involved injuries. Table 1 shows the changes in the number of injury and fatal accidents per mile per year between the "before" and "after" periods. (Three segments in Group I with only two years of before and after data were extrapolated to three years.) The changes in injury and fatal accidents on Michigan freeways (Interstate and U.S.) were used as controls to estimate the expected "after" values.

# TABLE 1

## Injury and Fatal Accidents/Mile/Year

Group I: Guardrail in "Before" Period

	Before	Afte	r
Left-side, Guardrail CMB	1.03	0bserved  2.09	Expected 1.02
Group II: Grass Median in "Before" Period			
Head-on & SS-OP CMB	0.31	0.09 0.77	0.30

Analysis of the injury and fatal accidents per mile per year implied similar conclusions to those from the analysis of severity ratios. For Group I, injury and fatal accidents occurred about twice as frequently with CMB than expected with guardrail. For Group II, it is important to note that the number of head-on and sideswipe-opposite injury and fatal accidents per mile, per year dropped to a quarter of the expected value when CMB was installed.

Single Vehicle/MultiVehicle Accidents - Secondary collisions (i.e., those involving a vehicle striking a barrier, then striking other vehicles) have been a concern where CMB has been installed. A comparison of the percentage of multivehicle accidents with guardrail and with CMB indicated CMB did not increase the percentage of secondary collisions. Analyzing Group III, it was found that multivehicle accidents were 10.6 percent of left-side guardrail accidents. Multivehicle injury and fatal accidents were 17.3 percent of left-side guardrail injury and fatal accidents. In comparison, multivehicle accidents were 8.8 percent of CMB accidents. Multivehicle injury and fatal

accidents were 9.5 percent of the CMB injury and fatal accidents. The differences in both barrier accidents and injury and fatal accidents were not significant at the 95 percent confidence level when the data for each segment were compared using the paired t-test.

Fatal Accidents - There were 16 fatal single-vehicle accidents and 12 fatal multivehicle accidents involving left-side guardrail at the 49 locations in Group III from 1971 through 1981. There were four CMB fatal accidents at the same locations after CMB installation, all of them single-vehicle accidents.

Table 2 shows the number of left-side guardrail fatal accidents, CMB fatal accidents, and the number of fatal head-on and sideswipe-opposite direction accidents for the Group III roadways from 1971 through 1981. Also shown are the number of barrier related and nonbarrier-related fatal accidents.

## TABLE 2

### Fatal Accidents

Year	Left-Side Guardrail	СМВ	Head-On SS-OP	Barrier Related	Nonbarrier Related	<u>Barrier/</u> Nonbarrier
1971	5	*	4	9	25	0.36
1972	3	-	11	14	23	0.61
1973	8	-	1	9	33	0.27
1974	7	æ	4	11	27	0.41
1975	2	0	2	4	18	0.22
1976	3	0	0	3	15	0.20
1977	0	0	1 ·	1	7	0.14
1978	0	0	2	2	15	0.13
1979	0	0	0	0	12	0
1980	0	1	1	2	9	0.22
1981	0	3	0	3	11	0.27
Total	28	4	26	58	195	0.30

The average barrier/nonbarrier accident ratio for 1971-1976 (i.e. the period before widespread CMB use) of 0.35 was used to predict an expected number of barrier-related fatal accidents (68), that would have occurred if CMB had not been installed. The actual number of barrier-related fatal accidents was 58. This gives a reduction of 10 fatal accidents or 15 percent. This difference was tested for statistical significance using the Kolmogorov-Smirnov test (see appendix) and was significant at the 95 percent confidence level.

The use of nonbarrier fatal accidents to predict an expected number of barrierrelated fatal accidents was complicated by the fact that other programs were instituted on these freeways during the study period which may have substantially reduced total fatal accidents. Examples of these are the "Yellow Book" programs to reduce roadside obstacles and the relocation of light poles from the right side of the roadway to the median on top of the CMB.

The left-side accidents in Group I when guardrail was replaced by CMB increased by 40 percent. Injury accidents doubled, and fatal accidents decreased from 11 to zero between the three-year period before CMB installation and the three years after.

The head-on and sideswipe-opposite direction accidents in Group II showed reductions of 77 percent in total accidents, 71 percent in injury accidents, and from three to zero in fatal accidents between the periods of three years before CMB installation and three years after. In addition, there were no fatal CMB accidents of any type in Group II in the three-year "after" period.

The evidence pointed to a reduction of fatal barrier-related accidents when CMB was installed, although it is difficult to assess the true contribution of CMB.

<u>Roadway Characteristics Model</u> - A multiple regression analysis was performed to determine which roadway characteristics, if any, contributed to CMB injury and fatal accidents. Accident experience from 1976 through 1980 for CMB installed after 1974 was used as the data file for the regression analysis. Dummy variables were used to express the nominal scale data (i.e. "either/or" data) in a form suitable for regression analysis. The roadway characteristics incorporated in the analysis were: alignment, shoulder slope, absence of glare screen, curb type, ADT, and the number of roadway lanes. The overall equation (see the complete analysis in the appendix) accounted for a total of 21 percent of the variance in CMB injury and fatal accidents. This indicated that other factors (vehicle speed, driver and vehicle characteristics, etc.) had a greater influence upon injury and fatal CMB accidents than roadway characteristics.

This analysis indicated, however, each factor's relative contribution to injury and fatal CMB accidents. Table 3 shows the roadway characteristics and the percentage of the variance associated with each characteristic.

### TABLE 3

Variable	Total R-Square (%)	Incremental R-Square (%)
Average ADT	13.4	13.4
Shoulder 7-13 feet		
w/Valley Gutter	15.6	2.2
Absence of Glare Screen	16.8	1.2
Roadway Alignment - Curve	17.7	0.9
Shoulder $\geq$ 13 feet		
w/Rolled Curb	18.4	0.7
Positive Shoulder Slope	20.6	2.2
Shoulder 7-13 feet w/o Curb -		
w/Negative Shoulder Slope	20.6	0.0
Number of Lanes	20.6	Too small to be computed

ADT was the most important of the studied roadway characteristics associated with injury and fatal CMB accidents (i.e., the higher the ADT, the more injury and fatal CMB accidents which occurred). The remaining characteristics appeared to have little influence, and the number of lanes had none. Based solely on injury and fatal accidents, this analysis indicates that a barrier treatment consisting of a 7-13 foot shoulder without curb and with a negative shoulder slope was preferred.

<u>Cross-Median and Rollover Accidents</u> - A study conducted in Milwaukee, Wisconsin  $\frac{167}{107}$  categorized 170 accidents which occurred in a one-year period with GM shape CMB as follows:

- 14% returned to traffic lane.
- 4% returned to traffic lane and had a secondary collision.
- 5% struck the barrier and rolled over. (75% small vehicles)
- 7% mounted the barrier.

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- 3% crossed the barrier and entered opposing lanes.
- 67% struck the barrier and remained on the shoulder
  - adjacent to the barrier.

Only injury and fatal CMB accident reports for 1980 and 1981 were screened to determine the number of cross-median and rollover accidents. It was assumed that very few rollover or cross-median accidents occurred that would not result in an injury or a fatality. The results are shown in Table 4. Six and one half percent of injury and fatal CMB accidents were rollovers. The percentage that mounted the barrier but did not cross was 0.6 percent and those that crossed the barrier accounted for 1.3 percent. The rollover data in Table 4 also indicated that small cars (under 2,500 lbs.), although a smaller percentage than in the Wisconsin study, were still over-represented in rollovers when compared to 1981 Michigan registration percentages. The significance of the difference between expected (registrations) and observed results was tested using the Chi-Square test and the difference was statistically significant at the 95 percent confidence level. The major contributor to the Chi-Square value was the "under 2,500 lbs." class. (See appendix.)

The six cross-median accidents occurred at three segments which had concrete glare screen, two segments which had green post glare screen and one segment which had no glare screen. This evidence, combined with the results of the analysis of roadway characteristics presented previously, indicates that glare screen has little benefit in reducing cross-median accidents. However, a prior department study  $\frac{17}{11}$  has shown glare screen to be effective in assisting drivers in performing their visual task and to have a positive influence in reducing accidents related to driver attention to opposing traffic.

#### TABLE 4

Vehicle Size	<u>Cross-Median</u>	Mounted Barrier	Rollover (%)	1981 Registrations
Passenger Cars				
Under 2500 lbs.		1	9 (30.0)	16.1
2500-3500 lbs.	1		10 (33.3)	39.0
Over 3500 lbs.	3	1	7 (23.3)	35.5
Truck	1		4	
Truck Tractor (Semi)	) 1		(13.4)	9.4
Bus		1		
Total	6	3	30	

1980-1981 Injury and Fatal Accidents

# CMB Accidents and Vehicle Size

Data on the size of vehicles involved in CMB collisions were available from 1978 through 1981. Table 5 shows the number of CMB single-vehicle accidents and the severity ratio by passenger car size for the four-year period.

# TABLE 5

 $\mathbf{f}_{i,i}^{(1)}$ 

# CMB (Single-Vehicle) Accidents/Severity Ratio

Passenger Car Size	1978	1979	1980	1981	Total
Less than 2500 lbs.	30/0.43	32/0.47	38/0.66	63/0.52	163/0.53
2500 to 3500 lbs.	111/0.53	134/0.51	136/0.51	183/0.52	564/0.52
Greater than 3500 lbs.	265/0.54	368/0.50	449/0.53	223/0.57	1305/0.53

Table 6 shows the same data for CMB multivehicle accidents.

## TABLE 6

# CMB (Multivehicle) Accidents/Severity Ratio

Passenger Car Size	1978	1979	1980	1981	Total
Less Than 2500 lbs.	7/0.29	5/0.60	7/0.75	10/0.70	29/0.55
2500 to 3500 lbs.	11/0.73	14/0.57	17/0.53	25/0.56	67/0.58
Greater than 3500 lbs.	37/0.49	40/0.63	32/0.63	28/0.50	137/0.56

Table 7 shows the severity ratio by passenger car size for the four-year total of state trunkline accidents from 1978 through 1981 and study location total accidents in addition to the severity ratios for both CMB single-vehicle and multivehicle accidents.

# TABLE 7

# Severity Ratios

Passenger Car Size	State Trunkline Accidents (1978-1980)	Study Location (S Accidents (1978-1981)	CMB ingle-Vehicle) Accidents (1978-1981)	CMB (Multivehicle) Accidents (1978-1981)
Less than 2500 lbs.	0.33	0.41	0.53	0.55
2500 to 3500 lbs.	0.32	0.41	0.52	0.58
Greater than 3500 lbs.	0.32	0.40	0.53	0.56

The severity ratios in Table 5 show very little variation with the exception of the less than 2,500 lb. class which rose to a peak in 1980, then fell in 1981. The data in Table 6 varied a bit more, due to the lower numbers of accidents, but the four-year totals were very close to those of the CMB singlevehicle. Table 7 shows that the severity ratio remained constant regardless of vehicle class for the three accident types.

#### SUMMARY

There were more CMB accidents per mile per year than left-side guardrail accidents. However, since total accidents increased during the study period, the 1981 percentage of CMB accidents was similar to the 1971 left-side guardrail accident percentage. Similarly, total accidents involving CMB were greater per mile per year than head-on and sideswipe-opposite direction accidents across grass medians. However, the head-on and sideswipe-opposite accidents decreased by 70 percent when CMB was installed in grass medians.

ADT on two roadway segments doubled; however, the typical change was much less, with some segments increasing and some decreasing. The overall change for all study segments between 1971 and 1981 was an increase of three percent.

Median barrier accidents were a relatively constant percentage of total freeway accidents, regardless of the type of barrier in place.

The severity ratio for CMB accidents was greater than that for left-side guardrail accidents where guardrail preceded CMB installation. The differences, however, were not statistically significant. The increase may have reflected only a greater number of unreported accidents in the "after" period. Head-on and sideswipe-opposite direction accidents across a grass median had a higher severity ratio than the "after" period CMB severity ratio. This difference was also not statistically significant.

The number of injury and fatal accidents per mile per year for CMB in the "after" period was approximately double the rate for guardrail in the "before" period. The number of injury and fatal accidents per mile per year for CMB in the "after" period was also higher than the number of head-on and sideswipe opposite direction injury and fatal accidents per mile per year in the "before" period at locations with grass median as the before condition. The number of head-on and sideswipe opposite injury and fatal accidents per mile per year fell 70 percent, however, when CMB was installed.

Multivehicle accidents are a smaller percentage of CMB accidents than of left-side guardrail accidents. Multivehicle injury and fatal accidents are also a smaller percentage of CMB injury and fatal accidents than of left-side guardrail injury and fatal accidents.

Fatal barrier-related accidents decreased by 10 (15 percent) compared to the number of barrier-related accidents expected, computed using the barrier/nonbarrier ratio for 1971-1976 (i.e. the period before widespread CMB use). This decrease was statistically significant at the 95 percent confidence level. Other safety programs which contributed to a decrease in nonbarrier related fatalities complicated this analysis. There were no fatal CMB accidents on the Group I and Group II roadways in the three years after CMB installation. Therefore, it appears that substantial reductions in barrier related fatal accidents occur after CMB installation.

While reductions in all types of accidents are desirable from a traffic engineering perspective, where a choice must be made, fatal accidents will receive primary attention even at the expense of increased property damage and/or injury accidents. The human and economic costs of fatal accidents far outweigh all other types. This must be taken into account when evaluating CMB installations.

Random factors, other than the roadway characteristics analysis, appeared to have the greatest influence on CMB injury and fatal accidents. Average Daily Traffic was the most important roadway characteristic influencing CMB injury and fatal accidents. As ADT increased, injury and fatal CMB accidents tended to increase. The preferred shoulder treatment indicated by this analysis was 7 to 13 feet wide without curb and with a negative shoulder slope. As more data on injury types become available, an analysis of this nature may be useful to identify factors which are associated with increasing severity of injuries.

Very few vehicles crossed the CMB, mounted the CMB, or rolled over as a result of striking CMB on Michigan freeways. The percentages of accidents in which vehicles crossed the barrier or mounted the barrier were both less than found in an earlier study. Although the results were based on a sample of 30 injury and fatal rollover accidents, small cars (under 2500 lbs.) appeared overrepresented in rollovers compared with vehicle registrations.

There was no evidence to suggest that vehicle size has any influence on the severity of CMB accidents.

### CONCLUSIONS

- A. Barrier-related Accidents
  - 1. Concrete median barriers experienced more reported accidents per mile than median guardrail. However, since total accidents in the study period generally increased, by 1981 the percentage of CMB accidents was about the same as noted for steel beam median accidents in 1971.
  - 2. Total accidents involving CMB were greater than the number of crossmedian crashes through grass medians. However, the particularly severe head-on and sideswipe-opposite direction crash decreased by 70 percent when CMB was installed in grass medians.
- B. Accident Severity
  - 1. Reported CMB accidents have a higher severity ratio (Injury + Fatal Accidents/Total Accidents) than left-side guardrail accidents. However, the problem of a possibly higher rate of unreported property damage accidents adds some uncertainty to this conclusion.
  - 2. The combined number of CMB injury and fatal accidents per mile per year was about twice that of left side guardrail accidents. (Note: Fatal accidents were relatively few compared to injury accidents, therefore, this number reflects primarily the change in injury accidents.)

- 3. CMB accidents have a lower severity ratio than head-on and sideswipeopposite direction accidents associated with grass medians.
- 4. The combined number of all types of CMB injury and fatal accidents per mile per year was about twice that of head-on and sideswipeopposite direction injury and fatal accidents per mile per year associated with grass medians. (See note under item B.2.)
- C. Secondary Collisions
  - 1. The installation of CMB did not appear to increase the percentage of secondary, multivehicle accidents (i.e., those where a vehicle strikes the barrier and then strikes another vehicle).
  - D. Fatal Accidents
    - 1. Although the number of CMB injury and fatal accidents per mile per year was greater than in the "before" conditions, both where no barrier (assuming head-on and sideswipe-opposite direction accidents reflect potential barrier accidents) or steel beam guardrail median barrier previously existed, the installation of CMB substantially reduced median-related fatal accidents.
  - E. Roadway Characteristics
    - 1. The roadway characteristics studied accounted for only 21 percent of the variance in CMB accident severity. This indicates that other factors (speed, driver and vehicle characteristics, etc.) had a greater influence upon CMB accident severity.
    - 2. ADT was the roadway characteristic most strongly associated with injury and fatal CMB accidents.
    - 3. A CMB treatment consisting of a 7 to 13-foot shoulder without curb and with a negative shoulder slope was the safest CMB cross section studied. However, the impact on safety of any cross-section studied was very small.
  - F. Rollover Performance
    - 1. Six and one-half percent of CMB injury and fatal accidents were rollovers. Less than one percent mounted the barrier, but did not cross and slightly more than one percent crossed the barrier.
    - 2. Small cars (under 2500 lbs.) appeared to be over-represented in the 30 injury and fatal rollover accidents.
  - G. Influence of Vehicle Weight
    - 1. Vehicle size had little effect on the severity ratio of CMB accidents.

### RECOMMENDATIONS

- 1. Since approximately 80 percent of the variance in CMB injury and fatal accidents was due to factors other than traffic or roadway characteristics, safety considerations probably do not warrant redesigning existing CMB. However, in deciding for or against new CMB, ADT should be the primary safety consideration in favor of CMB. The preferred shoulder treatment for new CMB installations should be 7 to 13-feet wide with no curb and a negative shoulder slope.
- 2. A larger sample size of rollover accidents needs to be investigated to confirm if small cars are over represented in CMB rollover accidents.
- 3. The effect of lateral placement of the median barrier on both accident frequency and severity should be investigated. As more data on injury types become available, the severity analysis can be refined.

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- 12/ "Concrete Median Barriers: Are They Effective" by Katie Sowell; Unpublished, Michigan Department of Transportation; December, 1980.
- $\frac{13}{}$  Personal Communication, Dwight A. Bell, Design Supervising Engineer.
- $\frac{14}{}$  Bronstad, Calcote, and Kimball; <u>op.</u> <u>cit.</u>; p 150.
- <u>15</u>/ <u>Ibid;</u> p. 14.
- <u>16</u>/ Ibid; p. 14.
- 17/ "Glare Screen Evaluation" by Gary R. Holben, C.E.T. and Thomas L. Malek, P.E.; TSD-263-75, Michigan Department of Transportation; February, 1975.

APPENDIX

# TABLE A

Guardrail/CMB Accident Rates (Percent of Total Accidents)

Year	<u>1971</u>	<u>1972</u>	<u>1973</u>	1974	1975	1976	1977	1978	<u>1979</u>	1980	1981
Group I: Guardrail in Before Period											
Left-Side, Guardrail Accidents/Mile Left-Side, CMB Accidents/Mile	2.7(12.3) 	3.2(11.3)	2.9(4.5) 	2.5(5.0) 	2.4(4.9) 0.9(1.9)	2.2(2.4) 2.8(3.1)	1.8(3.0) 4.5(7.4)	1.0(1.5) 4.1(6.1)	0.5(0.8) 4.7(7.7)	0.6(1.1) 5.1(9.8)	0.2(0.4) 5.8(11.5)
Group II: Grass Median in Before Perio	d										
Left-Side, CNB Accidents/Mile Head-On & SS-OP Accidents/Mile	- 0.7(3.8)	- 0.7(3.8)	0.7(3.4)	- 0.3(2.1)	1.0(6.4) 0.4(2.5)	2.1(13.8) 0.1(0.7)	2.0(11.3) 0.1(0.6)	2.0(13.5) 0.2(1.4)	1.2(8.6) 0.1(0.7)	1.6(13.6) 0.1(0.8)	1.1(10.5) 0.1(1.0

# SEVERITY RATIO GROUP I LOG-LIKELIHOOD TEST

	Before Left-Side	After	
	Guardrail (1)	CMB (2)	Total
Injury & Fatal Accidents (n)	94	190	284
Accidents (s)	230	349	579

 $\lambda_{1} = \frac{n_{1}}{s_{1}^{1}} = \frac{94}{230} = 0.41 \qquad \qquad \lambda_{2} = \frac{n_{2}}{s_{2}^{2}} = \frac{190}{349} = 0.54$  $\lambda_{0} = \frac{n_{1} + n_{2}}{s_{1}^{1} + s_{2}^{2}} = \frac{284}{579} = 0.49$  $T = 2 (n_{1} \log_{2} \lambda_{1} + n_{2} \log_{2} \lambda_{2} - (n_{1} + n_{2}) \log_{2} \lambda_{0})$ 

 $T = 2 (n_1 \log_{\lambda_1} + n_2 \log_{\lambda_2} - (n_1 + n_2) \log_{\lambda_1} \lambda_0)$ = 2 (94 log 0.41 + 190 log 0.541 - (284) log 0.49) = 2 (-83.81 - 117.08 + 202.59) = 2 (1.70) = 3.40

df = 1 0.10>P>0.05

# SEVERITY RATIO GROUP II LOG-LIKELIHOOD TEST

27

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	Before Head-on Sideswine	After		
	Opposite (1)	CMB (2)	Total	
Injury & Fatal Accidents (n)	17	41	58	
Accidents (s)	30	95	125	

$$\lambda_{1} = \frac{n_{1}}{s_{1}^{4}} = \frac{17}{30} = 0.57 \qquad \qquad \lambda_{2} = \frac{n_{2}}{s_{2}^{2}} = \frac{41}{95} = 0.43$$

$$\lambda_{0} = \frac{n_{1} + n_{2}}{s_{1}^{4} = s_{2}^{2}} = \frac{58}{125} = 0.46$$

$$\square = 2 (n_{1} \log_{e} \lambda_{1} + n_{2} \log_{e} \lambda_{2} - (n_{1} + n_{2}) \log_{e} \lambda_{0})$$

$$= 2 (17 \log_{e} 0.57 + 241 \log_{e} \lambda_{2} - (n_{1} + n_{2}) \log_{e} \lambda_{0})$$

$$= 2 (-9.56 = 34.60 + 45.04)$$

$$= 2 (0.88) = 1.76$$

$$df = 1 \qquad 0.20 \ge P \ge 0.10$$

# SEVERITY RATIOS GROUP II LOG-LIKELIHOOD TEST

	Before Head-on, Sideswipe Opposite (1)	After Head-on, Sideswipe Opposite (2)	Total
Injury & Fatal Accidents (n)	17	4	21
Accidents (s)	30	7	37
$\lambda_1 = \frac{n_1}{s_1^1} = \frac{17}{30}$	= 0.57	$\lambda_2 = \frac{n_2}{s_2^2} = \frac{4}{7} = 0.57$	
	$\lambda_0 = \frac{n_1 + n_2}{s_1 + s_2} =$	$\frac{21}{37} = 0.57$	

 $T = 2 (n_1 \log_{\lambda_1} \lambda_1 + n_2 \log_{\lambda_2} \lambda_2 - (n_1 + n_2) \log_{\lambda_1} \lambda_0)$ = 2 (17 log 0.57 + 4 log 0.57 - (21) log 0.57) = 2 (-9.56 - 2.25 + 11.80) = 2 (0) = 0

df = 1

p>0.20

1971-1981 MULTI-VEHICLE ACCIDENTS Paired-t Test

Before (L.S.G.R.)	After (C.M.B.)	d = A - B	ď <sup>2</sup>	
0	0	0	0	**
11	8	-3	9	Ho: B=A
1 7	0	= <u> </u>	1	d = A - B = 0
1	3	-4	16	N = 49
3	U	-j	9	$L_{12} = 26$
1	U	~1 ^	1	$\sum d = 1300$
0	0	0	0	d = Ld/N = 26/49 = 0.53
1	0	-1	U I	
<u> </u>	0	-1	0	$s = (5d)^2 - (5d)^2 / N$
Õ	· 0	0	0	$S = \frac{Lu - (2u)}{N-1}$
1	1	0	0	V N I
3	5	2	4	$= 1300 - (26)^2/49$
1	. 1	0	0	$\sqrt{\frac{1000}{49-1}}$
Ō	Ō	0	Ő	
6	5	-1	1	· ·
4	4	0	0	= 5.18
0	0	0	0	
0	2	2	4	
1	0	- 1	1	$t = \bar{d} - 0 = 0.53 - 0$
1	1	0	0	s/ Jn 5.18/ 49
1	0	-1	1	•
1	0	-1	1	= 0.72
2	2	0	0	
0	0	0	0	p> 0.10
6	1	-5	25	
3	1	-2	4	
0	. 0	0	0	
0	U	0	0	
3		=2	4	
4	/	د ۲0	900	
14 11	41 10	21	/29	
17	15	-2	49	
0	1	1		·
1	4	3	ģ	
õ	O	ő	ó	
14	33	19	361	
16	16	0.	0	
0	0	0	0	
1	0	-1	1	
3.	1	-2	4	
7	0	-7	49	
0	0	0	0	
2	2	0	0	
1	0	<u>-1</u>	1	
0	0	0	0	
0	1	1	1	
. 0	0	0	0	
		<u>}≞</u> 26	<b>≽</b> ₌1300	

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1971-1981 MULTI-VEHICLE INJURY AND FATAL ACCIDENTS Paired-t Test

Before (L.S.G.R.)	After (C.M.B.)	d = A - B	d <sup>2</sup>	
(L.S.G.R.) 0 3 1 2 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0	(C.M.B.) 0 3 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0	d = A-B $0$ $0$ $-1$ $-1$ $0$ $0$ $-1$ $0$ $0$ $0$ $0$ $0$ $0$ $0$ $0$ $-4$ $0$ $0$ $0$ $-4$ $0$ $0$ $0$ $-4$ $0$ $0$ $0$ $-4$ $0$ $0$ $0$ $-4$ $0$ $0$ $0$ $-1$ $1$ $13$ $3$ $-3$ $0$ $0$ $-1$ $1$ $13$ $3$ $-3$ $0$ $0$ $-1$ $1$ $13$ $3$ $-3$ $0$ $0$ $-1$ $1$ $1$ $-1$ $0$ $0$ $-1$ $-1$ $-1$ $-1$ $-1$ $-1$ $-1$ $-1$	$     d^{2}     0     0     1     1     0     1     0     0     0     0     0     0     0     0     0     0     0     0     0     0     0     1     1     0     0     0     1     1     0     1     1     1     0     1     1     1     0     1     1     1     0     1     1     1     0     1     1     1     0     1     1     1     0     1     1     1     0     1     1     1     0     1     1     1     0     1     1     1     0     1     1     1     0     1     1     1     0     1     1     1     0     1     1     1     0     1     1     1     0     1     1     1     0     1     1     0     1     1     0     1     1     1     1     0     1$	Ho: B = A d = A-B = 0 N = 49 $\Sigma d = 1$ $\Sigma d^2 = 391$ $d = \Sigma d/N = 1/49 = 0.02$ $S = \sqrt{\Sigma d^2 - (\Sigma d)^2/N}$ $= \sqrt{391 - (1)^2/49}$ = 2.85 $t = \overline{d} - 0 = 0.02 - 0$ $S = \sqrt{\sqrt{N}} = 0.02 - 0$ $S = \sqrt{\sqrt{N}} = 0.10$
		21		

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Number of Street

# FATAL ACCIDENTS KOLMOGOROV-SMIRNOV TEST

Vere	Non-Barrier	Barrier R	elated			
iear		Expected (F)	Observed (f)	Cum. F	Cum. f	đ
1971	25	9	9	9	9	0
1972	23	8	14	17	23	6
1973	33	12	9	29	32	3
1974	27	9	11	38	43	5
1975	18	6	4	44	47	3
1976	15	5	3	49	50	1.
1977	7	2	1	51	51	0
1978	15	5	2	56	53	3
1979	12	4	0	60	53	7
1980	9	. 3	2	63	55	8
1981	11	4	3	67	58	9

Expected Barrier-Related Fatal Accidents = Non-Barrier Fatal Accidents X 0.35

$$D = \frac{\max.|d|}{n} = \frac{9}{11} = 0.82$$

P<0.001

# VEHICLE SIZE CHI-SQUARE TEST

	Percer	ntage	n	$(0-E)^2$
R	egistrations (E)	Rollovers (O)	$(0-E)^2$	E
Under 2500 lbs	16.1	30.0	193.2	12.0
2500-3500 lbs	39.0	33.3	32.5	0.8
Greater than 3500	lbs 35.5	23.3	148.8	4.2
Other	9.4	13.4	16.0	1.7
			X <sup>2</sup> =	= 18.7

df = 3

p>0.01

5-27-83 PMB:jsm(119A-263)-8 Safety Programs Unit

# STATISTICAL PACKAGE FOR THE SOCIAL SCIENCES

SPSS FOR B6700, VERSION H, RELEASE 7.2, LEVEL 72.001.045.006

DEFAULT SPACE	ALLOCATION	ALLOWS FOR 50	TRANSFORMATIONS
WORKSPACE	17500 WORDS	400	RECODE VALUES + LAG VARIABLES
TRANSPACE	2500 WORDS	600	IF/COMPUTE OPERATIONS

NUMBERED	YES
RUN NAME	CLYNN/CMB/PREDICTION/SPSS
VARIABLE LIST	ALIGN, SHOULDER, GLARE, YEARCMB, CURB, LANE, YEARACCI,
	CMBACC1.CMBFAT1.CMBINJ1.ADT1.
	YEARACC2,CMBACC2,CMBFAT2,CMBINU2,ADT2,
	YEARACC3,CMBACC3,CMBFAT3,CMBINU3,ADT3,
	YEARACC4, CMBACC4, CMBFAT4, CMBINU4, ADT4,
	YEARACC5, CMBACC5, CMBFAT5, CMBINJ5, ADT5
INPUT FORMAT	FIXED(16X,F1.0,F1.0,3X,F1.0,2X,F2.0,F1.0,F1.0,
	1X,F2.0,72X,3F4.0,36X,F6.0/3(29X,F2.0,72X,3F4.0,
	36X,F6.0/),29X,F2.0,72X,3F4.0,36X,F6.0)

1/09/82

ACCORDING TO YOUR INPUT FORMAT, VARIABLES ARE TO BE READ AS FOLLOWS

VARIABLE	FORMAT	RECORD	COLUMNS	
ALIGN	F 1. 0	1	17- 17	
SHOULDER	F 1. O	1	18- 18	
GLARE	F 1. O	1	22- 22	
YEARCMB	F 2. O	1	25- 26	
CURB	F 1. O	1	27- 27	
LANE	F 1. O	1	28- 28	
YEARACCI	F2.0	1	30 - 31	
CMBACC 1	F4.0	1	104- 107	
CMBFAT 1	F4.0	4	108-111	
CMBINJ1	F 4. O	1	112- 115	
ADT 1	F6.0	ţ	152- 157	
YEARACC2	F 2. O	2	30- 31	
CMBACC2	F4.0	2	104- 107	
CMBFAT2	F 4. O	2	108- 111	
CMBINJ2	F4.0	2	112- 115	
ADT2	F 6. O	2	152- 157	
YEARACC3	F 2. O	3	30- 31	
CMBACC3	F4.0	3	104- 107	
CMBFAT3	F4.0	3	108- 111	
CMBINJ3	F4.0	3	112- 115	
ADT 3	F 6. O	З	152- 157	
YEARACC4	F 2. O	4	30- 31	
CMBACC4	F4.0	4	104- 107	
CMBFAT4	F4.0	4	108-111	

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ACCORDING TO YOUR INPUT FORMAT, VARIABLES ARE TO BE READ AS FOLLOWS

VARIABLE	FORMAT	RECORD	COLUMNS
CMBINJ4	F4.0	Ą	112- 115
ADT4	F 6. O	4	152- 157
YEARACC5	F 2. 0	5	30- 31
CMBACC5	F4.0	5	104- 107
CMBFAT5	F4.0	5	108- 111
CMBINJ5	F4.0	5	112- 115
ADT5	F 6. O	5	152- 157

THE INPUT FORMAT PROVIDES FOR 31 VARIABLES. 31 WILL BE READ IT PROVIDES FOR 5 RECORDS ('CARDS') PER CASE. A MAXIMUM OF 157 'COLUMNS' ARE USED ON A RECORD.

INPUT MEDIUM	DISK
N OF CASES	UNKNOWN
MISSING VALUES	ALIGN,GLARE TO CMBACC5(0)
IF	(ALIGN EQ 2) $D1 = 1$
IF	(SHOULDER EQ 1) $D2 = 1$
IF	(GLARE EQ 3) $D4 = 1$
IF	(CURB EQ 2) D8 = 1
IF	(CURB EQ 3) D9 = 1
IF	(CURB EQ 5) D10 = 1
COMPUTE	SEVERITY=CMBFAT1+CMBINJ1+CMBFAT2+CMBINJ2+
	CMBFAT3+CMBINJ3+CMBFAT4+CMBINJ4+CMBFAT5+
	CMBINJ5
COUNT	N=ADT1,ADT2,ADT3,ADT4,ADT5(1 THRU HIGHEST)
COMPUTE	ADTTOTAL=ADT1+ADT2+ADT3+ADT4+ADT5
COMPUTE	AVEADT=ADTTOTAL/N
ASSIGN MISSING	AVEADT(O)
COMPUTE	CMBTOT=CMBACC1+CMBACC2+CMBACC3+CMBACC4+CMBACC5
COMPUTE	CMBTOTAL=SQRT (CMBTOT+.375)
REGRESSION	VARIABLES=D1, D2, D4, D8 TO D10, LANE, AVEADT, SEVERITY/
	REGRESSION = SEVERITY WITH D1, D2, D4, D8 TO D10, LANE,
	AVEADT(1)/
STATISTICS	1

STATISTICS

279 WORDS WORKSPACE, NOT INCLUDING RESIDUALS \*\*\*\*\* \*\* REGRESSION PROBLEM REQUIRES

READ INPUT DATA

AFTER READING

.

99 CASES FROM SUBFILE NONAME , END OF FILE WAS ENCOUNTERED ON LOGICAL UNIT # 8

#### CLYNN/CMB/PREDICTION/SPSS

(d)

26

11/09/82 /

8

فريد ويتأسبه

PAGE 3

FILE NONAME (CREATION DATE = 11/09/82)

### CORRELATION COEFFICIENTS

### A VALUE OF 99,00000 IS PRINTED IF A COEFFICIENT CANNOT BE COMPUTED.

	D1 .	D2	D4	08	D9	D 10	LANE	AVEADT	SEVERITY
D1	1.00000	0.08086	-0.25298	0.00000	-0.08287	0.03780	0.09949	0.10571	-0.02741
D2	0.08086	1.00000	-0.33542	0.34094	-0.66540	0.30562	0.51563	0.61111	0.22865
D4	-0.25298	-0.33542	1.00000	-0.14444	0.11007	-0.04183	-0.16962	-0.13662	-0.13327
D8	0.00000	0.34094	-0.14444	1.00000	-0.24460	-0.19920	-0.04104	-0.14465	-0.19714
D9	-0.08287	-0.66540	0.11007	-0.24460	1.00000	-0.21926	-0.55782	-0.64107	-0.14567
D10	0.03780	0.30562	-0.04183	-0.19920	-0.21926	1.00000	0.70959	0.01681	-0.04079
LANE	0.09949	0.51563	-0.16962	-0.04104	-0.55782	0.70959	1.00000	0.40720	0.08078
AVEADT	0.10571	0.61111	-0.13662	-0.14465	-0.64107	0.01681	0.40720	1.00000	0.36661
SEVERITY	-0.02741	0.22865	-0.13327	-0.19714	-0.14567	-0.04079	0.08078	0.36661	1.00000

CLYNN/CMB/PRED	DICTION/SPSS					11/09/82	PAGE	4	
	CREATION D	$\Delta TF = 11/0$	9/82)						
			-,,						
* * * * * * *	****	*****	**** # WUL1	IPLE RE	GRESSION	*****	* * * * *	* * VARIABL REGRESSIO	.ELIST 1 DNLIST 1
DEPENDENT VARI	ABLE. SEV	ERITY							
VARIABLE(S) EN	TERED ON STEP	NUMBER 1	AVEADT						
MULTIPLE R	0.36661		ANALYS	IS OF VARIANCE	DF SUM	OF SQUARES	MEAN S	OUARE	F
R SQUARE	0.13440	)	REGRES	SION	1.	832.61446	832.	61446	15.06139
STANDARD ERROR	14RE 0.12548 7.43515	i	KESIDO	AL	97.	5362.29464	55.	28139	
	VARIABLES	IN THE EO	UATION			VARIABLES	NOT IN THE	EQUATION	
VARTARI F	в	RFTA	STO FROOR B	F	VARTABLE	RFTA IN	ραρτίαι	TOI FRANCE	F
TANIADEE	U	0L/H			TANLADEE	DELY IN	1 401 1445	TOLENATOL	I
AVEADT .	9677218E-04	0.36661	0.00002	15.061	D1	-0.06691	-0.07152	0.98882	0.494
(CONSTANT) -2	.897508				02	0.00737	0.00627	0.62655	0.004
					D4	-0.08477	-0.09025	0.98133	0.788
					U8 D0	-0.14719	-0.15654	0.97908	2.412
					D9	-0.04607	0.12513	0.58903	1.527
					LANE	-0.08212	-0.08062	0.83419	0.628
* * * *. * *	* * * * * * \$	. * * * * *	* * * * * * * *	* * * * * * * *	* * * * * *	* * * * * *	* * * * *	* * * * * * *	* * * * *
VARIABLE(S) EN	ITERED ON STEP	NUMBER 2	D8						
	0 39448	I	AMAI Y	IS OF VADIANCE		OF SOLLARES	MEAN S		F
R SQUARE	0.15561		REGRES	SION	2.	964.01496	482.0	00748	8.84604
ADJUSTED R SQU	IARE 0. 13802		RESIDU	IAL	96.	5230.89413	54.	48848	
STANDARD ERROR	7.38163	1				i.			
	VARIABLES	IN THE EQ	UATION		<b></b>	VARIABLES	NOT IN THE	EQUATION	
VARIABLE	в	BETA	STD ERROR B	۶	VARIABLE	BETA IN	PARTIAL	TOLERANCE	F
AVEADT .	9115225E-04	0.34532	0.00003	13:274	D1	-0.06465	-0.06996	0.98859	0.467
D8 -3	1.018762	-0.14719	1.94394	2.412	D2	0.15471	0.11146	0.43828	1.195
(CONSTANT) -1	.888244		-		D4	-0.11255	-0.11962	0.95379	1.379
					D9	0.08397	0.06283	0.47281	0.377
					DIO	-0.07907	-0.08431	0.96017	0.680
			-		LANE	-0.07900	~0.07851	0.83386	0.583

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CLYNN/CMB/P	REDICTION/SPSS					11/09/82	PAGE 5	5	
ILE NONA	ME (CREATION	DATE = 11/09,	(82)						
	* * * * * * * *	* * * * * *	* * * * MUL	TIPLE REG	RESSION	* * * * * *	* * * * * *	* * VARIABI	ELIST
COCNOENT V		VEDITY						REGRESSIC	DN LIST
	ARIADLE., JE	VCRIII							
ARIABLE(S)	ENTERED ON SIE	P NUMBER 3.	. 04						
ULTIPLE R	O.4095	1	ANALY	SIS OF VARIANCE	OF SUM	OF SQUARES	MEAN SC	WARE	F
SQUARE	0.1677	0	REGRE	SSION	3.	1038.86745	346.2	18915	6.3803
TANDARD ER	ROR 7.3671	0	KE 210	UAL	39.	3138.04164	34.3	(1412	,
	VARIABLE	S IN THE EQUA	TION		*****	VARIABLE	S NOT IN THE	EQUATION	•
ARIABLE	ß	BETA	STD ERROR B	F	VARIABLE	BETA IN	PARTIAL	TOLERANCE	F
VEADT	.8637237E-04	0.32721	0.00003	11.655	Dt	-0.09726	-0.10283	0.93020	1.0
8	-3.405921	-0.16607	1.96792	2.995	D2	0.11762	0.08198	0.40134	0.6
4 20110 T 1117 )	-2.077578	-0.11255	1.76909	1.379	D9	0.07605	0.05725	0.47159	0.3
CUNSTANT	-0.9220172				LANE	-0.09546	-0.09481	0.82095	0.8
* * * * *	* * * * * * *	* * * * * * * *	* * * * * * * *	* * * * * * * * *	* * * * * * *	* * * * * *	* * * * * * *	* * * * * * * *	* * * * *
ARIABLE(S)	ENTERED ON STE	P NUMBER 4.,	D1						
WLTIPLE R	0.4201	2	ANALY	SIS OF VARIANCE	DF SUM	OF SQUARES	MEAN SC	WARE	F
SQUARE	0.1765	0	REGRE	SSION	4.	1093.38279	273.3	14570	5.036
DJUSIED R	SQUARE 0.1414 BOD 7 3660	5	RESID	UAL	94	5101.52630	54.2	(1156	
		-			2 8				
***	VARIABLE	S IN THE EQUA	TION			VARIABLE	S NOT IN THE	EQUATION	
ARIABLE	B	BETA	STD ERROR B	F	VARIABLE	BETA IN	PARTIAL	TOLERANCE	F
VEADT	.8812257E-04	0.33384	0.00003	12.076	D2	0.10956	0.07665	0.40303	0.5
8	-3.457540	-0.16858	1.96855	3.085	D9	0.07234	0.05472	0.47123	0.2
14	-2.521761	-0.13662	1.82372	1.912	DIO	-0.08597	-0.09253	0.95417	0.80
CONSTANT)	8871514E-01	0.03120	1.04402	1.004	5 146 B.A.E.	-0.03210	-0.03137	0.02000	0.1

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CLYNN/CMB/I	PREDICTION/SPSS					11/09/82	PAGE 6	5	
FILE NON	AME (CREATION D	ATE = 11/0	9/82)		•				
* * * * *	* * * * * * * *	* * * *	* * * * MULI	TIPLE REG	RESSIO	N * * * * * *	* * * * * *	* * VARIAB REGRESSI	LE LIST 1 ON LIST 1
DEPENDENT	VARIABLE SEV	ERITY						1 L L OT L OT L	
VARIABLE(S	) ENTERED ON STEP	NUMBER 5	D10						
MULTIPLE R R SQUARE	0.42843 0.18355	1	ANALYS	SIS OF VARIANCE	DF SUN	4 OF SQUARES 1137.06517	MEAN SO 227.4	2UARE 11303	F 4,18151
ADJUSTED R STANDARD EI	SQUARE 0.13965 RROR 7.37465	•	RESIDU	JAL	93.	5057.84392	54.3	38542	
	VARĮABLES	IN THE EQI	UATION			VARIABLES	NOT IN THE	EQUATION	
VARIABLE	8	BETA	STD ERROR B	F	VARIABLE	BETA IN	PARTIAL	TOLERANCE	F
AVEADT	.8753144E-04	0.33160	0.00003	11.881	D2	0.29118	0.16448	0.26052	2.558
D8	-3.833339	-0.18690	2.01473	3.620	D9	0.02603	0.01799	0.38997	0.030
D4	-2.633517	-0.14267	1.82989	2.071	LANE	-0.05035	-0.03105	0.31057	0.089
D1 D10	~1.517279	-0.09531	1.54693	0.962					
(CONSTANT)	-1.896384	-0.08597	2.11622	0.803					
* * * * * * VARIABLE(S	* * * * * * * * * * ) ENTERED ON STEP	* * * * * *	* * * * * * * * *	* * * * * * *	* * * * * * *	* * * * * * * *	* * * * *	* * * * *	* * * * *
							•		
MULTIPLE R	0.45347	•	ANALYS	SIS OF VARIANCE	DF SUM	M OF SQUARES	MEAN SU	JUARE	F
R SQUARE	0.20564		REGRES	SION	6.	1273.89671	212.3	31612	3,96932
ADJUSTED R STANDARD EI	SQUARE 0.15383 RROR 7.31364		RESIDU	JAL	92.	4921.01238	53.4	18926	
	VARIABLES	IN THE EQ	UATION			VARIABLES	NOT IN THE	EQUATION	
VARIABLE	`В	BETA	STD ERROR B	F	VARIABLE	BETA IN	PARTIAL	TOLERANCE	F
AVEADT	.3704847E-04	0.14035	0.00004	0.842	09	0.04514	0.03153	0.38753	0.091
D8	-6.749243	-0.32908	2.70481	6.226	LANE	-0.02214	-0.01376	0.30703	0.017
D4	-1.715931	-0.09296	1.90327	0.813					
D1	~1.302336	-0.08181	1.54001	0.715					
010	-4.3/9223 A 850505	-U. 19849 0 20440	2.61036	2.814					
(CONSTANT)	1.4840626	0.29118	3.03214	«.J20					
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CLYNN/CMB/P	REDICTION/SPSS					11/09/82	PAGE 7		
FILE NONA	ME (CREATION	DATE = 11/09	/82)			· .			
* * * * * *	* * * * * * *	* * * * *	* * * * M U		REGRESSI	0 N * * * * * *	* * * * * *	* VARIA	BLE LIST 1
DEPENDENT V	ARIABLE. SE	EVERITY						REGRESS	ION LIST 1
VARIABLE(S)	ENTERED ON ST	EP NUMBER 7.	. 09						
MULTIPLE R R SQUARE ADJUSTED R STANDARD ER	0.4543 0.2064 SQUARE 0.1453 ROR 7.3500	34 13 38 06	AN/ REC RES	ALYSIS OF VARIAN GRESSION SIDUAL	NCE DF 7. 91.	SUM OF SQUARES 1278.78791 4916.12118	MEAN SQL 182.68 54.02	JARE 3399 233 1	F 3.38158
****	VARIABLE	ES IN THE EQU	ATION		****	VARIABLES	NOT IN THE	EQUATION	
VARIABLE	B	BETA	STD ERROR 8	٦	VARIAB	LE BETA IN	PARTIAL	TOLERANCE	F
AVEADT D8 D4 D1 D10 D2 D9 (CONSTANT)	.4466604E-04 -6.410435 -1.651209 -1.289764 -4.125852 4.923380 0.8734086 0.8608534	0.16921 -0.31256 -0.08945 -0.08102 -0.18701 0.29555 0.04514	0.00005 2.94226 1.92481 1.54824 2.75519 3.05743 2.90269	0.872 4.747 0.736 0.694 2.242 2.593 0.091	LANE	-0.00906	-0.00542	0.28447	0.003

F-LEVEL OR TOLERANCE-LEVEL INSUFFICIENT FOR FURTHER COMPUTATION

STATISTICS WHICH CANNOT BE COMPUTED ARE PRINTED AS ALL NINES.

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CLYNN/CMB/PREDICTION/SPSS				11/09/82	PAGE 8	
FILE NONAMÉ (CREATION DATE = 11/09/82)						۲
* * * * * * * * * * * * * * * * * * *	MULTIPLE	REGR	ESSION	* * * * *	* * * * * * * * · RE	VARIABLE LIST I GRESSION LIST 1
	SUM	IMARY TABLE				
VARTABLE	MULTIPLE R	R SQUARE	RSQ CHANGE	SIMPLE R	B	BETA
AVEADT D8 D4 D1 D10 D2 D9 (CDNSTANT)	0.36661 0.39448 0.40951 0.42012 0.42843 0.45347 0.45434	0.13440 0.15561 0.16770 0.17650 0.18355 0.20564 0.20643	0.13440 0.02121 0.01208 0.00880 0.00705 0.02209 0.00079	0.36661 -0.19714 -0.13327 -0.02741 -0.04079 0.22865 -0.14567	.4466604E-04 -6.410435 -1.651209 -1.289764 -4.125852 4.923380 0.8734086 0.8608534	0.16921 -0.31256 -0.08945 -0.08102 -0.18701 0.29555 0.04514

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