## Guardrail Design



# MDOT/ACEC Design Basic Training <br> Guardrail Design <br> November 1, 2023 <br> 9:00 a.m. to 4:30 p.m. <br> Virtual Training, via Teams 

## AGENDA

Our presenter today is Carlos Torres. Carlos is the Roadside Safety Engineer Specialist and the Chairperson of the
Barrier Advisory Committee for MDOT. He has held that role since 2004.
9:00 a.m.-12:00 p.m. Guardrail Design
Topics to be covered in this training include:

- Provide an overview of guardrail design
- Clear zone concept
- Roadside topography and its effects on guardrail design
- Overview of different guardrail types and related features
- Guardrail types
- Approach terminals
- Departing terminals
- Anchorages
- Curved guardrail
- Long span details
- Other guardrail features
- Guardrail design terminology and applications
- Methodology for calculating minimum length of need
- Knowing which guardrail features to use for different applications
- Solve a guardrail design example problem
- Provide a brief overview of MDOT standards and guidelines related to guardrail

12:00 p.m.-1:00 p.m. - Lunch Break -
1:00 p.m.- 4:30 p.m. Guardrail Design - continuation of above topics
Total CEHs offered for A.M. and P.M. sessions: 6.50

Thank you for attending today's training. The following are helpful links:
Event Links: A.M. Session: Guardrail A.M. Session P.M. Session: Guardrail P.M. Session
Design Basic Training Wiki Page: DBT Wiki Page
Survey: Guardrail Survey

## Presenter

Carlos Torres, P.E.

- MDOT Roadside Safety Engineer (2004)
- Chairman - Barrier Advisory Committee (2004)
- Statewide specialist in all aspects of roadside design and safety


## Objectives

- Provide an overview of guardrail design
- Clear Zone Concept
- Roadside Topography and Its Effects on Guardrail Design
- Overview of Guardrail Types and Related Features
- Methodology for Calculating Minimum Length of Need
- MASH-Compliant Guardrail and Related Features


## Objectives

- Provide an overview of guardrail design
- Guidelines and Standards Related to Guardrail Design
- Michigan Road Design Manual - Chapter 7 https://mdotiboss.state.mi.us/stdplan/englishroadma nual.htm
- MDOT Standard Plans and Special Details https://mdotiboss.state.mi.us/stdplan/standardPlans Home.htm
- 2011 AASHTO Roadside Design Guide
- Available for purchase through AASHTO website
- MDOT employees can access electronically through ASTM/AASHTO Web Portal (in MDOT-CFS Sharepoint page)


## $4^{\text {th }}$ Edition, 2011 AASHTO Roadside Design Guide



## Other Reference Documents

- MDOT 2020 Standard Specifications for Construction https://michigan.gov/mdot/business/construction/standard-specifications-and-publications
- MDOT Previously Approved Special Provisions (PASPs)
https://mdotjboss.state.mi.us/SpecProv/specProvHome.htm
- MDOT Frequently Used Special Provisions (FUSPs)
- SOM employees only: Available through MDOT Supplemental Specs and Special Provisions (SS/SP) app using MILogin
»Must request access to use this app


## Objectives

- Solve example problems
> Type 2M Guardrail Approach Terminals
> Type MGS-8 Guardrail
> M-Series Guardrail Bridge Anchorages
> MDOT Guardrail Worksheet


## *** Disclaimers ***

- The contents of this class represent current Michigan DOT (MDOT) guardrail design practices and principles
- Many of the terms and some of the design principles/practices presented in this class are specific to MDOT and may not reflect the terms and design principles/practices utilized by other agencies
- The concepts presented in this class are intended to serve as general guidelines
- There are exceptions to the norms!
- Guardrail design can be subjective and usually requires detailed knowledge of the conditions and constraints at each proposed installation site
- Engineering judgment may need to be utilized
- What works at one location may not be suitable at a different location


## What is MASH?

AASHIO

- MASH stands for Manual for Assessing Safety Hardware
- AASHTO Publication
- MASH is the current standard for establishing the crash worthiness of roadside safety features


# Manual for Assessing Safety Hardware 

Second Edition


## History of Crash Testing Standards

- 1962: HRB 482
- 1971: NCHRP 115
- 1972: NCHRP 118
- 1974: NCHRP 153
- 1978: TRC 191
- 1981: NCHRP 230
- 1993: NCHRP 350
- 2009: MASH 2009 (MASH-09)
- 2016: MASH 2016 (MASH-16)


## Roadside Topography



## Clear Zone Concept

- An area available for use by an errant vehicle
- This area should be free of hazards
- If hazards exists within this area, appropriate action should be taken


## Clear Zone Concept

- In the early 1970s, most state agencies used 30 feet as the clear zone distance
- However, a 30 -foot clear zone is not adequate for certain applications
- In the late 1970s, AASHTO developed a clear zone table, taking into consideration:
- Design Speed
- Traffic Volume (ADT)
- Roadside Geometry


## MDOT Clear Zone Table

## Section 7.01.11.C - Michigan Road Design Manual

CLEAR ZONE DISTANCES
(IN FEET FROM EDGE OF DRIVING LANE)

| $\begin{aligned} & \text { DESIGN } \\ & \text { SPEED } \end{aligned}$ | $\begin{gathered} \text { DESIGN } \\ \text { ADT } \end{gathered}$ | FILL SLOPES |  |  | CUT SLOPES |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1:6 OR FLATTER | $\begin{aligned} & 1: 5 \\ & \text { TO } \\ & 1: 4 \end{aligned}$ | 1:3 | $1: 3$ | $\begin{aligned} & 1: 4 \\ & \text { TO } \\ & 1: 5 \end{aligned}$ | $\begin{gathered} \text { 1:6 } \\ \text { OR } \\ \text { FLATTER } \end{gathered}$ |
| 40 mph or Less | under 750 | 7-10 | 7-10 | ** | 7-10 | 7-10 | 7-10 |
|  | 750-1500 | 10-12 | 12-14 | ** | 10-12 | 12-14 | 12-14 |
|  | 1500-6000 | 12-14 | 14-16 | ** | 12-14 | 14-16 | 14-16 |
|  | over 6000 | 14-16 | 16-18 | ** | 14-16 | 16-18 | 16-18 |
| $\begin{gathered} 45-50 \\ \mathrm{mph} \end{gathered}$ | under 750 | 10-12 | 12-14 | ** | 8-10 | 8-10 | 10-12 |
|  | 750-1500 | 14-16 | 16-20 | ** | 10-12 | 12-14 | 14-16 |
|  | 1500-6000 | 16-18 | 20-26 | ** | 12-14 | 14-16 | 16-18 |
|  | over 6000 | 20-22 | 24-28 | ** | 14-16 | 18-20 | 20-22 |
| $\begin{gathered} 55 \\ \mathrm{mph} \end{gathered}$ | under 750 | 12-14 | 14-18 | ** | 8-10 | 10-12 | 10-12 |
|  | 750-1500 | 16-18 | 20-24 | ** | 10-12 | 14-16 | 16-18 |
|  | 1500-6000 | 20-22 | 24-30 | ** | 14-16 | 16-18 | 20-22 |
|  | over 6000 | 22-24 | 26-32* | ** | 16-18 | 20-22 | 22-24 |
| $\begin{gathered} 60 \\ \mathrm{mph} \end{gathered}$ | under 750 | 16-18 | 20-24 | ** | 10-12 | 12-14 | 14-16 |
|  | 750-1500 | 20-24 | 26-32* | ** | 12-14 | 16-18 | 20-22 |
|  | 1500-6000 | 26-30 | $32-40^{*}$ | ** | 14-18 | 18-22 | 24-26 |
|  | over 6000 | 30-32* | 36-44* | ** | 20-22 | 24-26 | 26-28 |
| $\begin{aligned} & \geq 65 \\ & \mathrm{mph} \end{aligned}$ | under 750 | 18-20 | 20-26 | ** | 10-12 | 14-16 | 14-16 |
|  | 750-1500 | 24-26 | 28-36* | ** | 12-16 | 18-20 | 20-22 |
|  | 1500-6000 | 28-32* | 34-42* | ** | 16-20 | 22-24 | 26-28 |
|  | over 6000 | 30-34* | 38-46* | ** | 22-24 | 26-30 | 28-30 |

Where a site specific investigation indicates a high probability of continuing crashes, or such occurrences are indicated by crash history, the designer may provide clear zone distances greater than 30 feet as indicated. Clear zones may be limited to 30 feet for practicality and to provide a consistent roadway template if previous experience with similar projects or designs indicates satisfactory performance.
** Since recovery is less likely on the unshielded, traversable 1:3 slopes, fixed objects should not be present in the vicinity of the toe of these slopes.

## Only difference between MDOT and AASHTO CZ values

## MDOT

LEAR ZONE DISTANCES

| $\begin{aligned} & \text { DESIGN } \\ & \text { SPEED } \end{aligned}$ | $\begin{gathered} \text { DESIGN } \\ \text { ADT } \end{gathered}$ | FILL SLOPES |  |  | CUT SLOPES |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $1: 6$ OR FLATTER | $\begin{aligned} & 1: 5 \\ & \text { T0 } \\ & 1: 4 \end{aligned}$ | 1:3 | 1:3 | $\begin{aligned} & 1: 4 \\ & \text { TO } \\ & 7: 5 \end{aligned}$ | 1:6 OR <br> FLATTER |
| $\begin{gathered} 40 \mathrm{mph} \\ \text { or } \\ \text { Less } \end{gathered}$ | under 750 | 7-10 | 7-10 | ** | 7-10 | 7-10 | 7-10 |
|  | 750-1500 | 10-12 | 12-14 | ** | 10-12 | 12-14 | 12-14 |
|  | 1500-6000 | 12-14 | 14-16 | ** | 12-14 | 14-16 | 14-16 |
|  | over 6000 | 14-16 | 16-18 | ** | 14-16 | 16-18 | 16-18 |
| $\begin{aligned} & \text { 45-50 } \\ & \mathrm{mph} \end{aligned}$ | under 750 | 10-12 | 12-14 | ** | 8-10 | 8-10 | 10-12 |
|  | 750-1500 | 14-16 | 16-20 | ** | 10-12 | 12-14 | 14-16 |
|  | 1500-6000 | 16-18 | 20-26 | ** | 12-14 | 14-16 | 16-18 |
|  | over 6000 | 20-22 | 24-28 | ** | 14-16 | 18-20 | 20-22 |
| $\begin{gathered} 55 \\ \mathrm{mph} \end{gathered}$ | under 750 | 12-14 | 14-18 | ** | 8-10 | 10-12 | 10-12 |
|  | 750-1500 | 16-18 | 20-24 | ** | 10-12 | 14-16 | 16-18 |
|  | 1500-6000 | 20-22 | 24-30 | ** | 14-16 | 16-18 | 20-22 |
|  | over 6000 | 22-24 | 26-32* | ** | 16-18 | 20-22 | 22-24 |
| $\begin{gathered} 60 \\ \mathrm{mph} \end{gathered}$ | under 750 | 16-18 | 20-24 | ** | 10-12 | 12-14 | 14-16 |
|  | 750-1500 | 20-24 | 26-32* | ** | 12-14 | 16-18 | 20-22 |
|  | 1500-6000 | 26-30 | 32-40* | ** | 14-18 | 18-22 | 24-26 |
|  | over 6000 | 30-32* | 36-44* | ** | 20-22 | 24-26 | 26-28 |
| $\begin{aligned} & \geq 65 \\ & \mathrm{mph} \end{aligned}$ | under 750 | 18-20 | 20-26 | ** | 10-12 | 14-16 | 14-16 |
|  | 750-1500 | 24-26 | 28-36* | ** | 12-16 | 18-20 | 20-22 |
|  | 1500-6000 | 28-32* | 34-42* | ** | 16-20 | 22-24 | 26-28 |
|  | over 6000 | 30-34* | 38-46* | ** | 22-24 | 26-30 | 28-30 |

Where a site specific investigation indicates a high probability of continuing crashes, or such occurrences are indicated by crash history, the designer may provide clear zone distances greater than 30 feet as indicated. Clear zones may be limited to 30 feet for practicality and to provide a consistent roadway template if previous experience with similar projects or designs indicates satisfactory performance.

Since recovery is less likely on the unshielded, traversable 1:3 slopes, fixed objects should not be present in the vicinity of the toe of these slopes.

## AASHTO



Notes:
a) When a site-specific investigation indicates a high probability of continaing crashes or when such occurrences are indicated by crash history, the designer may provide clear-zone distances greater than the clear zone shown in Table 3-1. Clear zones may be limited to 30 ft for practicality and to provide a consistent roadway template if previous experience with similar projects or designs indicates satisfactory performance.
b) Because recovery is less likely on the unshielded, traversable 1 V :3H fill slopes, fixed objects should not be present in the vicinity of the toe of these slopes. Recovery of high-speed vehicles that encroach beyond the edge of the shoulder may be expected to occur beyond the toe of slope. Determination of the width of the recovery area at the toe of slope should consider right-of-way availability, environmental concerns, economic factors, safety needs, and crash histories. Also, the distance between the edge of the through traveled lane and the beginning of the 1 V : 3 H slope should influence the recovery area provided at the toe of slope. While the application may be limited by several factors, the foreslope parameters that may enter into determining a maximum desirable recovery area are illustrated in Figure 3-2. A 10 ft recovery area at the toe of slope should be provided for all traversable, non recoverable fill slopes.
) For roadways with low volumes it may not be practical to apply even the minimum values found in Table 3-1. Refer to Chapter 12 for additional considerations for low-volume roadways and Chapter 10 for additional guidance for urban applications.

When design speeds are greater than the values provided, the designer may provide clear-zone distances greater than those shown in Table 3-1,

## Horizontal Curves



## Horizontal Curves

## Horizontal Curve Adjustments

## CURVE CORRECTION FACTORS (Kcz)

| Radius <br> (ft) | DESIGN SPEED (mph) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{4 0}$ | $\mathbf{4 5}$ | $\mathbf{5 0}$ | $\mathbf{5 5}$ | $\mathbf{6 0}$ | $\mathbf{6 5}$ | $\mathbf{7 0}$ |  |
| 2950 | 1.1 | 1.1 | 1.1 | 1.2 | 1.2 | 1.2 | 1.2 |  |
| 2300 | 1.1 | 1.1 | 1.2 | 1.2 | 1.2 | 1.2 | 1.3 |  |
| 1970 | 1.1 | 1.2 | 1.2 | 1.2 | 1.3 | 1.3 | 1.4 |  |
| 1640 | 1.1 | 1.2 | 1.2 | 1.3 | 1.3 | 1.3 | 1.4 |  |
| 1475 | 1.2 | 1.2 | 1.3 | 1.3 | 1.4 | 1.4 | 1.5 |  |
| 1315 | 1.2 | 1.2 | 1.3 | 1.3 | 1.4 | 1.4 |  |  |
| 1150 | 1.2 | 1.2 | 1.3 | 1.4 | 1.5 | 1.5 |  |  |
| 985 | 1.2 | 1.3 | 1.4 | 1.5 | 1.5 | 1.5 |  |  |
| 820 | 1.3 | 1.3 | 1.4 | 1.5 |  |  |  |  |
| 660 | 1.3 | 1.4 | 1.5 |  |  |  |  |  |
| 495 | 1.4 | 1.5 |  |  |  |  |  |  |
| 330 | 1.5 |  |  |  |  |  |  |  |

$$
C Z_{\text {corr }}=C Z+\Delta C Z=K_{c z} \times C Z
$$

## Recoverable (1:4 or Flatter)



# Non-Recoverable (Steeper than 1:4, Up to 1:3) 

(Traversable)


## Critical (Steeper than 1:3)


(Non-Traversable, Non-Recoverable)

## Clear Runout Area



## Clear Runout Area



## Adjusted Clear Zone

## Adjusted Clear Zone



## Clear Zone for Auxiliary Lanes

## MDOT Method

Section 7.01.11 of the Michigan Road
Design Manual

- Obtain clear zone value from the clear zone table based on design speed and traffic volume (ADT) of adjacent through lanes
- Resulting clear zone distance:

1) Should be measured from the outer edge of the through lane, and;
2) Should not be less than 23 feet from the outer edge of the auxiliary lane.

## Clear Zone for Auxiliary Lane MDOT Method



## Clear Zone for Freeway Ramps

## MDOT Method

Preferred:
Clear Zone Based on Speed, Volume, and Horizontal Curvature of Ramp at Selected Point

- Engineering Judgment must be used

Acceptable Alternative:
May also use Clear Zone of 30 feet if:

- Traffic Volume and/or Speed at Selected Point are unknown or not well established, or
- Previous satisfactory experience with similar designs


## Transverse Slopes

- 1:10 or flatter desirable
- 1:6 or flatter for high-speed roadways, especially within clear zone
- May be considered a hazard under certain conditions
- steep transverse slopes


Grading Recommendations for Transverse Slopes Facing Oncoming Traffic at Bridge Approach Berms

Standard Plan R-105-Series


NOTE:
THE 1:6 SLDPE FACING FREEWAY TRAFF IC SHOULD BE USED ON ALL NEW CONSTRUCTION UNLESS THE DISTANCE FROM THE EDGE DF THE NEAREST FREEWAY THROUGH LANE TO THE
TOE OF THE $1: 2$ SLOPE UNDER THE BRIDGE EXCEEDS THE CLEAR ZONE.


## Is a $1: 2$ Longitudinal Backslope A Hazard If Located Within The Clear Zone?



NOTE:
THE $1: 6$ SLDPE FACING FREEWAY TRAFFIC SHOULD BE USED ON ALL NEW CONSTRUCTION UNLESS THE DISTANCE FROM THE EDGE DF THE NEAREST FREEWAY THROUGH LANE TD THE TOE OF THE 1:2 SLDPE UNDER THE BRIDGE EXCEEDS THE CLEAR ZONE.

A $1: 2$ backslope generally is not a hazard if:

- Relatively Smooth, and;
- Obstacle Free, and;
- Foreslope between roadway and toe of backslope is traversable (1:3 or flatter)




## Shielding Bodies of Water RDM - 7.01.31

- Permanent water > 2' in depth usually require shielding if within the CZ
- May be necessary to shield for bodies of water outside the CZ if there is potential for entry


## Bridge Columns and Foundations in 70' Medians

- At one time these were considered outside the CZ
- Shielding columns and foundation new construction/ reconstruction should be according to Standard Plan R-56 Series
- Standard Plan R-56 also covers medians $36^{\prime}$ - 70'
- Note, bridge piers may have additional shielding requirements
- Concrete barriers or struts may be required in certain cases
- Bridge Design Manual: 7.01.04.K (Vehicle Collision Force) and 12.08.08 (Protection of Existing Piers in the Clear Zone)


## Clear Zone Examples



## Clear Zone Example \#1



Design Speed: 60 mph

## CLEAR ZONE DISTANCES

## (IN FEET FROM EDGE OF DRIVING LANE)

| $\begin{aligned} & \text { DESIGN } \\ & \text { SPEED } \end{aligned}$ | $\begin{aligned} & \text { DESIGN } \\ & \text { ADT } \end{aligned}$ | FILL SLOPES |  |  | CUT SLOPES |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} \text { 1:6 } \\ \text { OR } \\ \text { FLATTER } \end{gathered}$ | $\begin{aligned} & \text { 1:5 } \\ & \text { TO } \\ & 1: 4 \end{aligned}$ | 1:3 | 1:3 | $\begin{aligned} & 1: 4 \\ & \text { TO } \\ & 1: 5 \end{aligned}$ | $\begin{array}{\|c} \text { 1:6 } \\ \text { OR } \\ \text { FLATTER } \end{array}$ |
| 40 mph or Less | under 750 | 7-10 | 7-10 | ** | 7-10 | 7-10 | 7-10 |
|  | 750-1500 | 10-12 | 12-14 | ** | 10-12 | 12-14 | 12-14 |
|  | 1500-6000 | 12-14 | 14-16 | ** | 12-14 | 14-16 | 14-16 |
|  | over 6000 | 14-16 | 16-18 | ** | 14-16 | 16-18 | 16-18 |
| $\begin{gathered} 45-50 \\ \mathrm{mph} \end{gathered}$ | under 750 | 10-12 | 12-14 | ** | 8-10 | 8-10 | 10-12 |
|  | 750-1500 | 14-16 | 16-20 | ** | 10-12 | 12-14 | 14-16 |
|  | 1500-6000 | 16-18 | 20-26 | ** | 12-14 | 14-16 | 16-18 |
|  | over 6000 | 20-22 | 24-28 | ** | 14-16 | 18-20 | 20-22 |
| $\begin{gathered} 55 \\ \mathrm{mph} \end{gathered}$ | under 750 | 12-14 | 14-18 | ** | 8-10 | 10-12 | 10-12 |
|  | 750-1500 | 16-18 | 20-24 | ** | 10-12 | 14-16 | 16-18 |
|  | 1500-6000 | 20-22 | 24-30 | ** | 14-16 | 16-18 | 20-22 |
|  | over 6000 | 22-24 | 26-32* | ** | 16-18 | 20-22 | 22-24 |
| $\begin{gathered} 60 \\ \mathrm{mph} \end{gathered}$ | under 750 | 16-18 | 20-24 | ** | 10-12 | 12-14 | 14-16 |
|  | 750-1500 | 20-24 | 26-32* | ** | 12-14 | 16-18 | 20-22 |
|  | 1500-6000 | 26-30 | 32-40* | ** | 14-18 | 18-22 | 24-26 |
|  | over 6000 | 30-32* | 36-44* | ** | 20-22 | 24-26 | 26-28 |
| $\begin{aligned} & \geq 65 \\ & \mathrm{mph} \end{aligned}$ | under 750 | 18-20 | 20-26 | ** | 10-12 | 14-16 | 14-16 |
|  | 750-1500 | 24-26 | 28-36* | ** | 12-16 | 18-20 | 20-22 |
|  | 1500-6000 | 28-32* | 34-42* | ** | 16-20 | 22-24 | 26-28 |
|  | over 6000 | 30-34* | 38-46* | ** | 22-24 | 26-30 | 28-30 |

Where a site specific investigation indicates a high probability of continuing crashes, or such occurrences are indicated by crash history, the designer may provide clear zone distances greater than 30 feet as indicated. Clear zones may be limited to 30 feet for practicality and to provide a consistent roadway template if previous experience with similar projects or designs indicates satisfactory performance.
** Since recovery is less likely on the unshielded, traversable $1: 3$ slopes, fixed objects should not be present in the vicinity of the toe of these slopes.

CLEAR ZONE DISTANCES
(IN FEET FROM EDGE OF DRIVING LANE)

| DESIGN SPEED | $\begin{gathered} \text { DESIGN } \\ \text { ADT } \end{gathered}$ | FILL SLPPES |  |  | CUT SLOPES |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & 1: 6 \\ & \text { OR } \end{aligned}$ <br> FLATTER | $\begin{aligned} & 1: 5 \\ & \text { T0 } \\ & 1: 4 \end{aligned}$ | 1:3 | 1:3 | $\begin{aligned} & 1: 4 \\ & \text { TO } \\ & 1: 5 \end{aligned}$ | $\begin{gathered} 1: 6 \\ \text { OR } \\ \text { FLATTER } \end{gathered}$ |
| $\begin{gathered} 40 \mathrm{mph} \\ \text { or } \\ \text { Less } \end{gathered}$ | under 750 | 7-10 | 7-10 | ** | 7-10 | 7-10 | 7-10 |
|  | 750-1500 | 10-12 | 12-14 | ** | 10-12 | 12-14 | 12-14 |
|  | 1500-6000 | 12-14 | 14-16 | ** | 12-14 | 14-16 | 14-16 |
|  | over 6000 | 14-16 | 16-18 | ** | 14-16 | 16-18 | 16-18 |
| $\begin{gathered} 45-50 \\ \mathrm{mph} \end{gathered}$ | under 750 | 10-12 | 12-14 | ** | 8-10 | 8-10 | 10-12 |
|  | 750-1500 | 14-16 | 16-20 | ** | 10-12 | 12-14 | 14-16 |
|  | 1500-6000 | 16-18 | 20-26 | ** | 12-14 | 14-16 | 16-18 |
|  | over 6000 | 20-22 | 24-28 | ** | 14-16 | 18-20 | 20-22 |
| $\begin{gathered} 55 \\ \mathrm{mph} \end{gathered}$ | under 750 | 12-14 | 14-18 | ** | 8-10 | 10-12 | 10-12 |
|  | 750-1500 | 16-18 | 20-24 | ** | 10-12 | 14-16 | 16-18 |
|  | 1500-6000 | 20-22 | 24-30 | ** | 14-16 | 16-18 | 20-22 |
|  | over 6000 | 22-24 | 26-32* | ** | 16-18 | 20-22 | 22-24 |
| $\begin{gathered} 60 \\ \mathrm{mph} \end{gathered}$ | under 750 | 16-18 | 20-24 | ** | 10-12 | 12-14 | 14-16 |
|  | 750-1500 | 20-24 | 26-32* | ** | 12-14 | 16-18 | 20-22 |
|  | 1500-6000 | 26-30 | 32-40* | ** | 14-18 | 18-22 | 24-26 |
|  | over 6000 | 30-32* | 36-44* | ** | 20-22 | 24-26 | 26-28 |
| $\begin{aligned} & \geq 65 \\ & \mathrm{mph} \end{aligned}$ | under 750 | 18-20 | 20-26 | ** | 10-12 | 14-16 | 14-16 |
|  | 750-1500 | 24-26 | 28-36* | ** | 12-16 | 18-20 | 20-22 |
|  | 1500-6000 | 28-32* | 34-42* | ** | 16-20 | 22-24 | 26-28 |
|  | over 6000 | 30-34* | 38-46* | ** | 22-24 | 26-30 | 28-30 |

Where a site specific investigation indicates a high probability of continuing crashes, or such occurrences are indicated by crash history, the designer may provide clear zone distances greater than 30 feet as indicated. Clear zones may be limited to 30 feet for practicality and to provide a consistent roadway template if previous experience with similar projects or designs indicates satisfactory performance.
** Since recovery is less likely on the unshielded, traversable $1: 3$ slopes, fixed objects should not be present in the vicinity of the toe of these slopes.

## Clear Zone Example \#1



Design Speed: 60 mph

## Clear Zone Example \#2



Design Speed: 60 mph

CLEAR ZONE DISTANCES
(IN F EET FROM EDGE OF DRIVING LANE)

| $\begin{aligned} & \text { DESIGN } \\ & \text { SPEED } \end{aligned}$ | $\begin{aligned} & \text { DESIGN } \\ & \text { ADT } \end{aligned}$ | FILL SLOPES |  |  | CUT SLOPES |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $1: 6$ OR FLATTER | $\begin{aligned} & \text { 1:5 } \\ & \text { TO } \\ & 1: 4 \end{aligned}$ | 1:3 | 1:3 | $\begin{aligned} & 1: 4 \\ & \text { TO } \\ & 1: 5 \end{aligned}$ | $\begin{gathered} \text { 1:6 } \\ \text { OR } \\ \text { FLATTER } \end{gathered}$ |
| $\begin{aligned} & 40 \mathrm{mph} \\ & \text { or } \\ & \text { Less } \end{aligned}$ | under 750 | 7-10 | 7-10 | ** | 7-10 | 7-10 | 7-10 |
|  | 750-1500 | 10-12 | 12-14 | ** | 10-12 | 12-14 | 12-14 |
|  | 1500-6000 | 12-14 | 14-16 | ** | 12-14 | 14-16 | 14-16 |
|  | over 6000 | 14-16 | 16-18 | ** | 14-16 | 16-18 | 16-18 |
| $\begin{gathered} \text { 45-50 } \\ \mathrm{mph} \end{gathered}$ | under 750 | 10-12 | 12-14 | ** | 8-10 | 8-10 | 10-12 |
|  | 750-1500 | 14-16 | 16-20 | ** | 10-12 | 12-14 | 14-16 |
|  | 1500-6000 | 16-18 | 20-26 | ** | 12-14 | 14-16 | 16-18 |
|  | over 6000 | 20-22 | 24-28 | ** | 14-16 | 18-20 | 20-22 |
| $\begin{gathered} 55 \\ \mathrm{mph} \end{gathered}$ | under 750 | 12-14 | 14-18 | ** | 8-10 | 10-12 | 10-12 |
|  | 750-1500 | 16-18 | 20-24 | ** | 10-12 | 14-16 | 16-18 |
|  | 1500-6000 | 20-22 | 24-30 | ** | 14-16 | 16-18 | 20-22 |
|  | over 6000 | 22-24 | 26-32* | ** | 16-18 | 20-22 | 22-24 |
| $60$ | under 750 | 16-18 | 20-24 | ** | 10-12 | 12-14 | 14-16 |
|  | 750-1500 | 20-24 | 26-32* | ** | 12-14 | 16-18 | 20-22 |
|  | 1500-6000 | 26-30 | 32-40* | ** | 14-18 | 18-22 | 24-26 |
|  | over 6000 | 30-32* | 36-44* | ** | 20-22 | 24-26 | 26-28 |
| $\begin{aligned} & \geq 65 \\ & \mathrm{mph} \end{aligned}$ | under 750 | 18-20 | 20-26 | ** | 10-12 | 14-16 | 14-16 |
|  | 750-1500 | 24-26 | 28-36* | ** | 12-16 | 18-20 | 20-22 |
|  | 1500-6000 | 28-32* | 34-42* | ** | 16-20 | 22-24 | 26-28 |
|  | over 6000 | 30-34* | 38-46* | ** | 22-24 | 26-30 | 28-30 |

Where a site specific investigation indicates a high probability of continuing crashes, or such occurrences are indicated by crash history, the designer may provide clear zone distances greater than 30 feet as indicated. Clear zones may be limited to 30 feet for practicality and to provide a consistent roadway template if previous experience with similar projects or designs indicates satisfactory performance.
** Since recovery is less likely on the unshielded, traversable 1:3 slopes, fixed objects should not be present in the vicinity of the toe of these slopes.

## Clear Zone Example \#2



Design Speed: 60 mph

## Clear Zone Example \#2



Design Speed: 60 mph

## Clear Zone Example \#2



Design Speed: 60 mph

## Clear Zone Example \#3



Design ADT: 1,400 vpd
Design Speed: 60 mph

| $\begin{aligned} & \text { DESIGN } \\ & \text { SPEED } \end{aligned}$ | $\begin{aligned} & \text { DESIGN } \\ & \text { ADT } \end{aligned}$ | FILL SLOPES |  |  | CUT S OPES |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & 1: 6 \\ & \text { OR } \end{aligned}$ <br> FLATTER | $\begin{aligned} & 1: 5 \\ & \text { TO } \\ & 1: 4 \end{aligned}$ | 1:3 | 1:3 | $\begin{aligned} & 1: 4 \\ & \text { TO } \\ & 1: 5 \end{aligned}$ | $\begin{gathered} \text { 1:6 } \\ \text { OR } \\ \text { FLATTER } \end{gathered}$ |
| $\begin{gathered} 40 \mathrm{mph} \\ \text { or } \\ \text { Less } \end{gathered}$ | under 750 | 7-10 | 7-10 | ** | 7-10 | 7-10 | 7-10 |
|  | 750-1500 | 10-12 | 12-14 | ** | 10-12 | 12-14 | 12-14 |
|  | 1500-6000 | 12-14 | 14-16 | ** | 12-14 | 14-16 | 14-16 |
|  | over 6000 | 14-16 | 16-18 | ** | 14-16 | 16-18 | 16-18 |
| $\begin{aligned} & \text { 45-50 } \\ & \mathrm{mph} \end{aligned}$ | under 750 | 10-12 | 12-14 | ** | 8-10 | 8-10 | 10-12 |
|  | 750-1500 | 14-16 | 16-20 | ** | 10-12 | 12-14 | 14-16 |
|  | 1500-6000 | 16-18 | 20-26 | ** | 12-14 | 14-16 | 16-18 |
|  | over 6000 | 20-22 | 24-28 | ** | 14-16 | 18-20 | 20-22 |
| $\begin{gathered} 55 \\ \mathrm{mph} \end{gathered}$ | under 750 | 12-14 | 14-18 | ** | 8-10 | 10-12 | 10-12 |
|  | 750-1500 | 16-18 | 20-24 | ** | 10-12 | 14-16 | 16-18 |
|  | 1500-6000 | 20-22 | 24-30 | ** | 14-16 | 16-18 | 20-22 |
|  | over 6000 | 22-24 | 26-32* | ** | 16-18 | 20-22 | 22-24 |
| mph | under 750 | 16-18 | 20-24 | ** | 10-12 | 12-14 | 14-16 |
|  | 750-1500 | 20-24 | 26-32* | ** | 12-14 | 16-18 | 20-22 |
|  | 1500-6000 | 26-30 | 32-40* | ** | 14-18 | 18-22 | 24-26 |
|  | over 6000 | 30-32* | 36-44* | ** | 20-22 | 24-26 | 26-28 |
| $\begin{aligned} & \geq 65 \\ & \mathrm{mph} \end{aligned}$ | under 750 | 18-20 | 20-26 | ** | 10-12 | 14-16 | 14-16 |
|  | 750-1500 | 24-26 | 28-36* | ** | 12-16 | 18-20 | 20-22 |
|  | 1500-6000 | 28-32* | 34-42* | ** | 16-20 | 22-24 | 26-28 |
|  | over 6000 | 30-34* | 38-46* | ** | 22-24 | 26-30 | 28-30 |

Where a site specific investigation indicates a high probability of continuing crashes, or such occurrences are indicated by crash history, the designer may provide clear zone distances greater than 30 feet as indicated. Clear zones may be limited to 30 feet for practicality and to provide a consistent roadway template if previous experience with similar projects or designs indicates satisfactory performance.
** Since recovery is less likely on the unshielded, traversable 1:3 slopes, fixed objects should not be present in the vicinity of the toe of these slopes.

## Clear Zone Example \#3



- 2011 AASHTO RDG Method (e.g., Example 3-F)
> Use larger of the two clear zones


## Clear Zone Example \#4

Where should the clear zone for EB traffic be measured from?


## Clear Zone Example \#4

Where should the clear zone for EB traffic be measured from?

Normal Practice
.-- - -

## Roadside Barriers



## Design Options in Order of Preference

> Remove Obstacle
> Relocate Obstacle
> Reduce Impact Severity
Shield Obstacle
> Delineate Obstacle


## Barrier Types

- Roadside Barriers
- Median

Barriers

- Bridge Railings



## Barrier Classifications

TYPE DEFLECTION

Flexible

Semi-Rigid

Rigid


Over 5 Feet

2-5 Feet

0-1 Foot

## Semi-Rigid Systems (Guardrail)

NCHRP 350 or Older Guardrail Systems

- Type A (Standard Plan R-60 Series)
- Type B (Standard Plan R-60 Series)
- Type BD (Standard Plan R-60 Series)
- Type C (old Standard Plan III-60 E)
- Type CD (old Standard Plan III-60 E)
- Type T (Standard Plan R-60 Series)
- Type TD (Standard Plan R-60 Series)


## MASH-Compliant Guardrail Systems

- Type MGS-8 (Standard Plan R-60 Series)
- Type MGS-8D (Standard Plan R-60 Series)


## Type A Guardrail

## Key Features

- No offset blocks
- 12 '-6" post spacing (typical)
- Typical top rail height is 28 inches
- Current use:
- Cul-de-sacs
- Parking lots
- Locations not exposed to
 through traffic


## Type B Guardrail

Key Features

- W-beam guardrail with 8" offset blocks
- Offset blocks are made of wood or plastic
- 6'-3" post spacing (typical)
- Typical top rail height is 28 inches
- IN MOST CASES, NOT PERMITTED FOR CONSTRUCTING NEW GUARDRAIL RUNS

- Current use:
- Repairing existing runs of Type B guardrail


## Type BD Guardrail

## Key Features

- Double-sided Type B guardrail
- W-beam guardrail and offset blocks on both sides
- Same post spacing and guardrail height as Type B
- IN MOST CASES, NOT PERMITTED FOR CONSTRUCTING NEW
 GUARDRAIL RUNS
- Current use:
- Repairing existing runs of Type BD guardrail


## Type C Guardrail

## Key Features

- Consists of two wbeams
- Upper beam has offset blocks
- Lower beam (rub rail) has no offset blocks
- 6'-3" post spacing (typical)
- Typical top rail height is 32 inches
- Current use:
- Repairing existing runs of


NOT PERMITTED FOR CONSTRUCTING NEW GUARDRAIL RUNS Type C guardrail

## Type CD Guardrail

## Key Features

- Double-sided Type C guardrail
- Same post spacing and guardrail height as Type C
- Current use:
- Repairing existing runs of Type CD guardrail


NOT PERMITTED FOR CONSTRUCTING NEW GUARDRAIL RUNS

## Type T Guardrail

## Key Features

- Thrie-beam guardrail with 8 " offset blocks
- 6'-3" post spacing (typical)
- Typical top rail height is 34 inches

- IN MOST CASES, NOT PERMITTED FOR CONSTRUCTING NEW GUARDRAIL RUNS
- Current use:
- Repairing existing runs of Type T guardrail


## Type TD Guardrail

## Key Features

- Double-sided Type T guardrail
- Same post spacing and guardrail height as Type T
- IN MOST CASES, NOT PERMITTED FOR CONSTRUCTING NEW GUARDRAIL RUNS

- Current use:
- Repairing existing runs of Type TD guardrail


## Type MGS-8 Guardrail

## Key Features

- W-beam guardrail with 8 " offset blocks
- Offset blocks are made of wood or plastic
- 6'-3" post spacing (typical)
- Typical top rail height is 31 inches
- Beam element splice located at midspan

- MASH, TL-3 Compliant
- Current use:
- Basic type for all roadways; free access roads, limited access roads, and freeways


## Type MGS-8

## 31" Tall W-Beam Guardrail with 8" Offset Blocks (MGS-8)



## Type MGS-8 Guardrail

## US-23 Flex Route Project, University Region



## Type MGS-8D Guardrail

## Key Features

- Double-sided Type MGS-8 guardrail
- Same post spacing and guardrail height as Type MGS-8
- Beam element splice located at midspan
- MASH, TL-3 Compliant
- Current use:
- Basic median guardrail
 type for all roadways; free access roads, limited access roads, and freeways


## Type MGS-8 Guardrail Details \& Guidelines

- MDOT Standard Plan (Special Detail) R-60-J
- Type MGS-8 \& MGS-8D Details
- Transition Details from Type MGS-8 to Other Guardrail Types
- Type MGS-8/8D to Type B/BD
- Type MGS-8/8D to Type T/TD
- Transition Details from Type MGS-8 to Guardrail Anchorages
- Transition Details from Type MGS-8 to Type 1B and Type 2B Guardrail Approach Terminals
- Chapter 7 - Road Design Manual
- Guidelines Pertaining to Type MGS-8 Guardrail
- Guardrail Worksheet Includes Type MGS-8 Guardrail Information


## Type B <br> Post Length Requirements



Specified in Standard Plan R-60-Series

## Type B Post Length Requirements



Specified in Standard Plan R-60-Series

## Type MGS-8 Post Length Requirements



Specified in Standard Plan R-60-Series

## Type MGS-8 Post Length Requirements



Specified in Standard Plan R-60-Series

# Guardrail Post Length Requirements Identified in Guardrail Pay Items 

Pay ItemPay Unit
Guardrail, Type __, __ inch Post ..... Foot
Guardrail, Temp, Type __, _inch Post ..... Foot
Guardrail, Curved, Type __, _ inch Post ..... Foot
Foot
Guardrail, Curved, Temp, Type _ , _ inch Post
> Defined in Frequently Used Special Provision (FUSP) 20SP-807H-01
> Designers must determine the required post length when setting up pay items

- A single guardrail run may have sections with different post lengths


## Barrier Location



Place Barrier
As Far From Traveled Way As Possible
Without Adversely Affecting Barrier Performance

## Barrier Location

Barrier to Hazard
Distance Is
Critical Element

## MDOT

## Guardrail Deflection Table

- Guardrail deflections are typical values
- Deflection may vary:
- Soil Type
- Thawed/Frozen Ground
- Length of installation
- Impact Characteristics
- Treat deflections from table as minimums
- If possible, consider adding factor of safety (e.g., $1^{\prime}$ ) to guardrail deflections listed in table

Guardrail Deflection

| Guardrail | Post Spacing | Minimum Design Offset * |
| :---: | :---: | :---: |
| Type T | $1^{\prime}-6{ }^{3 / 4}$ | 1'-2" |
| Type T | $3^{\prime}-11 / 2^{\prime \prime}$ | 1'-8" |
| Type T | $6^{\prime}-3{ }^{\prime \prime}$ | 2'-0" |
| Type B | $1^{\prime}-63 / 4^{\text {P }}$ | 1'-6" |
| Type B | $3^{\prime}-11 / 2^{\prime \prime}$ | 2'-0" |
| Type B | $6^{\prime}-3{ }^{\prime \prime}$ | 3'-0" |
| Type MGS-8 | $1^{\prime}-63 /{ }^{\text {" }}$ | 2'-5" |
| Type MGS-8 | $3^{\prime}-11 / 2^{\prime \prime}$ | 2'-11" |
| Type MGS-8 | $6^{\prime}-3{ }^{\prime \prime}$ | 3'-6" |
| Type MGS-8 Adjacent to Curb | $6^{\prime}-3{ }^{\prime \prime}$ | 4'-1" |
| Type MGS-8 Near Shoulder Hinge Point ** | $6^{\prime}-3{ }^{\prime \prime}$ | 4'-1" |

* An additional $12^{\prime \prime}$ or more is desirable where feasible
** Less than 2'-8" from the shoulder hinge point to the face of guardrail post


## Terrain Effects



- Curbs
- Slopes



# MDOT Guidelines Curb \& Guardrail 

- Section 7.01 .34 of the RDM discusses curb \& guardrail
- Use only Type D or valley gutter when design speed >50 mph
- Follow offset and max curb height recommendations when guardrail is placed away from curb


GUARDRAIL WHEN CURB IS ADJACENT TO EDGE OF PAVED SHOULDER OR TRAVELED LANE

CEESIGN SPEED 50 mph OR LESS)

** $2^{2}$ * when Curb is placed next to shoulder lane
GUARDRAIL WHEN CURB IS ADJACENT TO EDGE OF PAVED SHOULDER OR TRAVELED LANE (DESIGN SPEED GREATER THAN 50 mph)



GUARDRAIL WHEN CURB IS ADJACENT TO EDGE OF PAVED SHOULDER OR TRAVELED LANE (DESIGN SPEED 50 mph OR LESS)



GUARDRAIL - CURB OFFSET
WHEN GUARDRAIL IS PLACED AWAY FROM CURB

## Type D Curb \& Gutter MDOT Standard Plan R-30 Series



SEE NOTES WHEN PAVEMENT JOINT
IS SEaleo with Neoprene

| OETAIL | DIMENSION | LANE TIES | CONCRETE <br> CYD / LFI |
| :---: | :---: | :---: | :---: |
|  | T |  | AS SHOHN |
| D1 | $9^{\prime \prime}$ | OMITTED | 0.0788 |
| 02 | $10^{\prime \prime}$ | AS SHOHN | 0.0886 |
| 03 |  |  |  |

## Valley Gutter MDOT Standard Plan R-33 Series



LaNE TIE

## CONCRETE VALLEY GUTTER

## Looks OK?



## MDOT Standard Plan R-32-Series




CROSS SECTION WHEN APPROACH GUTTER IS USED


CROSS SECTION WHEN APPROACH GUTTER IS NOT USED

## Looks OK?



No !!
Use Detail 1A Bridge Approach Curb \& Gutter (Std. Plan R-32 Series) when there is no guardrail

## MDOT Standard Plan R-32-Series




CROSS SECTION WHEN DEPARTING GUTTER IS USED


CROSS SECTION WHEN DEPARTING GUTTER IS NOT USED

## 



## Guardrail on Slopes

- Optimum performance on $1: 10$ slopes or flatter
- May be installed on slopes as steep as 1:6 under certain (site-specific) conditions:
- Consult with the Geometric Design Unit (MDOT - Design Division)



## milu



## Type T Guardrail

TWIN Parallel guardrail Runs


## Standard Plan R-56-Series

## Type T Guardrail



## Standard Plan R-56-Series

## Type MGS-8 Guardrail

TWIN PARALLEL GUARDRAIL RUNS USING GUARDRAIL TYPE MGS-8


## Standard Plan R-56-Series

## Type MGS-8 Guardrail



Standard Plan R-56-Series

## MGS Long Span Details



Picture Source: MwRSF Research Report No. TRP-03-187-07


GUARDRAIL LONG SPAN, DETAIL MGS-1

## MDOT Standard Plan R-72-Series



## MDOT Standard Plan R-72-Series



GUARDRA]L, APPROACH TERM[NAL, TYPE 1B GUARDRAIL, APPROACH TERM[NAL, TYPE $2 B$ GUARDRAJL, DEPART ING TERMINAL, TYPE MGS GUARDRAJL, TYPE MGS-8


$37^{\prime}-6^{\prime \prime}$

GUARDRAIL, TYPE MGS-8 *
$37^{\prime}-6^{\prime \prime}$
$112^{\prime}-6^{\prime \prime}$ GUARDRAIL LDNG SPAN, DETAIL MGS-3
GUARDRAIL, TYPE MGS-8 *



$$
25^{\prime}-0^{\prime \prime}
$$

$28^{\prime \prime}$ GUARDRAIL, APPROACH TERMJNAL, TYPE 18
28 " GUARDRAIL. APPROACH TERMINAL, TYPE 2 B 28" GUARDRAIL, APPROACH TERMINAL, TYPE 2B 31" GUARDRAIL, DEPARTING TERMINAL, TYPE MGS $31^{\prime \prime}$ GUARDRAIL, TYPE MGS-8
$28^{\prime \prime}$ GUARDRAIL, APPROACH TERMJNAL, TYPE 2 B

31" GUARDRAIL, DEPARTING TERMINAL, TYPE MGS
$31^{\prime \prime}$ GUARDRAIL, TYPE MGS-8

## MDOT Standard Plan R-72-Series



## MDOT Standard Plan R-72-Series

# Placing Guardrail in Rock 7.01.33.C 



* WIDTH MAY BE INCREASED TO 15" TO ACCOMMODATE CONSTRUCTION TOLERANCES.
** $24^{\prime \prime}$ DIAMETER HOLE MAY BE USED.


WOOD POST PLAN VIEWS


STEEL POST PLAN VIEWS

FOR DVERLYING SOJL DEPTHS (A) RANGING FROM 0 TO $18^{n}$. THE DEPTH INTO ROCK (B) [S EQUAL TO $24^{\prime \prime}$.

FOR OVERLYJNG SOIL DEPTHS (A) RANGING FROM $18^{\prime \prime}$ TO FULL POST RANGING FROM 18 TI FULL POST EMBEDMENT DEPTH. THE REQUIRED DEPTH INTO ROCK (B) IS EQUAL TO FULL POST EMBEDMENT DEPTH MINUS (A).

## Guardrail Posts through Paved Surfaces 7.01.33.D



## Additional Blockouts on Guardrail Posts 7.01.33.E

Double Blockouts (up to 16" deep)

- Not permitted on terminals
- No limit to the number of posts in a guardrail run that can have double blockouts

Multiple Blockouts (up to 36" deep)

- Not permitted on terminals
- Limited to one or two posts in a guardrail run
- May use up to four blockouts on one post
** MUST TAKE SLOPE BEHIND POST INTO CONSIDERATION!!! **



## Guardrail Over Box/Slab Culverts MDOT Standard Plan R-73-Series

- 31" Tall Type MGS-8 Guardrail over Box/Slab Culvert
- 6'-3" Post Spacing Over Box/Slab Culvert
- Previous Version of R-73-Series Required a 3'-1½" Post Spacing


ELEVATION SHOWING GUARDRAIL, TYPE MGS-8



ELEVATION SHOWING GUARDRAIL, TYPE MGS-8

| MICHIGAN DEPARTMENT OF TRANSPORTATION bureau of development standard plan for |  |  |  |
| :---: | :---: | :---: | :---: |
| GUARDRAIL OVER |  |  |  |
| BOX OR SLAB CULVERTS |  |  |  |
|  | 8-1-2019 | $\mathrm{R}-73-\mathrm{F}$ | SHEET |



ELEVATION SHOWING GUARDRAIL, TYPE B

| MICHIGAN DEPARTMENT OF TRANSPORTATION buneau of development standard plan for |  |  |  |
| :---: | :---: | :---: | :---: |
| GUARDRAIL OVER |  |  |  |
| B0X | SL | CULVER |  |
|  | $\frac{8-1-2019}{\text { Prav Paile }}$ | R-73-F | $\begin{aligned} & \hline \text { SHEET } \\ & 1 \end{aligned}$ |



ELEVATION SHOWING GUARDRAIL, TYPE T


PREFERRED CONSTRUCTION METHOD


SECTION A - A
ALTERNATE CONSTRUCTION METHOD


BASE PLATE DETAIL

## Latest Version

## Earlier Versions



BASE PLATE DETAIL

Same post type (W6x8.5 or W6x9), but different base plate and welding requirements

## Barrier

## End Treatments



## Guardrail Terminals

- Gating
- Non-Gating



## Example of Gating Guardrail Terminals



## Beginning Length of Need Point (BLON)

Point where terminal is capable of redirecting a vehicle

## Gating Terminal



## Gating Terminals

Section 7.01.25.E of RDM

- The area behind and beyond the terminal should be traversable and free of fixed objects
- A 20' $\times 75^{\prime}$ (minimum) runout area beyond and parallel to the terminal should be provided



## MDOT MASH Compliant Guardrail Approach Terminals

Type 2M (Tangent) Approach Terminals

- Soft-Stop
- MSKT
- MAX-Tension
- Beginning Length of Need (BLON) varies

USED FOR MAJORITY OF NEW SINGLE-SIDED GUARDRAIL APPROACH TERMINAL INSTALLATIONS

## MASH Compliant Guardrail

 Terminals

## SoftStop (Trinity Industries)

## Soft-Stop

$50^{\prime}-g^{\prime \prime} /{ }^{\prime \prime}$


MDOT Standard Plan R-62-Series

## MASH Compliant Guardrail Terminals



Source: Road Systems

## MSKT (Road Systems, Inc.)

## SKT <br> NCHRP 350 Compliant

## MSKT

MASH Compliant


## MSKT

$59^{\prime}-4^{1} / 2^{\prime \prime}$


MDOT Standard Plan R-62-Series


## Max-Tension

$55^{\prime}-0^{\prime} / 2^{\prime \prime}$


## MDOT Standard Plan R-62-Series

## Max-Tension Crash Test Small Car (MASH, TL-3)



## Max-Tension Crash Test Pickup Truck (MASH, TL-3)



## MDOT NCHRP 350 Compliant Guardrail Approach Terminals

Type 1B or 1 T (Flared) Approach Terminals

- SRT
- FLEAT
- Beginning Length of Need (BLON) starts 12 '- 6 " from nose

USED VERY RARELY IN NEW GUARDRAIL INSTALLATIONS!
CONSULT WITH GEOMETRIC DESIGN UNIT BEFORE USING.

## SRT (Slotted Rail Terminal)



# FLEAT (Flared Energy Absorbing Terminal) 



## MDOT NCHRP 350 Compliant Guardrail Approach Terminals

Type 2B or 2T (Parallel) Approach Terminals

- ET
- SKT
- Beginning Length of Need (BLON) starts 12'-6" from nose

NOT USED FOR NEW GUARDRAIL INSTALLATIONS!

## ET (Extruder Terminal)




# SKT (Sequential Kinking Terminal) 


 atian


## MDOT NCHRP 350 Compliant Guardrail Approach Terminals

Type 3 (Double-Sided) Approach Terminals

- CAT (Standard Plan R-63 Series)
- FLEAT-MT (Standard Plan R-63 Series)
- All Type 3 Terminals are gating
- BLON varies - see MDOT Standard Plan R-63 Series
- STILL USED FOR NEW GUARDRAIL INSTALLATIONS, but MDOT will soon be switching to other terminals that are MASH compliant:
- MATT
- Max-Tension Median


## CAT

## (Crash Cushion Attenuation Terminal)



# FLEAT-MT (Median Terminal) 



## MATT

## 

- MASH, TL-3 compliant
- Currently not shown in Standard Plan R-63 Series, but this is expected to change in the near future


Source: Valtir

## MAX-Tension Median

- MASH, TL-3 compliant
- Currently not shown in Standard Plan R-63 Series, but this is expected to change in the near future


Source: Lindsay Transportation Solutions

# MDOT <br> Guardrail Approach Terminals 

Type 4 (Buried in Backslope)

- Non-proprietary
- Special Detail 24
- Non-Gating Terminal
> CAN BE USED FOR NEW GUARDRAIL INSTALLATIONS
> RECOMMENDED WHEN CONDITIONS ALLOW ITS USE


## Buried in Backslope



## Transition: MGS-8/8D to Type B or Guardrail Approach Terminals 1B/3B MDOT Standard Plan R-60-Series



ELEVATION SHOWING POST SPACING CONNECTING
GUARDRAIL, TYPE MGS-8 OR MGS-8D TO
GUARDRAIL, TYPE B, GUARDRAIL, TYPE BD, OR
GUARDRAIL APPROACH TERMINAL TYPE 1B, 2B, OR 3B


## Transition: MGS-8/8D to Type T/TD or Guardrail Bridge/Median Anchorages

MDOT Standard Plan R-60-Series guardrail, type T
GUARDRAIL, TYPE TD
GUARDRAIL ANCHORAGE, MEDIAN GUARDRAIL ANCHORAGE, BRIDGE DETAIL A1, T1, T4, OR T6


In This Case,
Height Transition is Measured and Paid as Type MGS-8 I 8D Guardrail

ELEVATION SHOWING POST SPACING CONNECTING GUARDRAIL, TYPE MGS-8 OR MGS-8D TO
GUARDRAIL, TYPE T, GUARDRAIL, TYPE TD, GUARDRAIL ANCHORAGE, MEDIAN,
GUARDRAIL ANCHORAGE, BRIDGE DETAIL A1, T1, T4 OR T6

# Transition: Type B to Guardrail Approach Terminal 2M <br> MDOT Standard Plan R-60-Series 



ELEVATION SHOWING TRANSITION DETAIL FOR CONNECTING GUARDRAIL, TYPE B TO
GUARDRAIL APPROACH TERMINAL TYPE 2M

NOTE: $34^{\prime}-4 \frac{1}{2} 2^{\prime \prime}$ Height Transition Included as Part of Guardrail Approach Terminal, Type 2M pay item, as defined in Guardrail Approach Terminal, Type 2M FUSP.

## Transition: Type T to Guardrail Approach Terminal 2M <br> MDOT Standard Plan R-60-Series



ELEVATION SHOWING TRANSITION DETAIL FOR CONNECTING GUARDRAIL, TYPE T TO
GUARDRAIL APPROACH TERMINAL TYPE 2M
NOTE: 28'-1½" Height Transition Included as Part of Guardrail Approach Terminal, Type 2M pay item, as defined in Guardrail Approach Terminal, Type 2M FUSP.

# Payment for Height Transitions When Connecting Guardrail Approach Terminal, Type 2M to Guardrail Types B or T MDOT FUSP 20SP-807F-01 

Payment for Guardrail Approach Terminal, Type 2M includes all materials, labor, and equipment within the length of each terminal, as defined in subsections d.1, d.2, and d. 3 of this special provision, and also includes payment for all materials, labor, and equipment required to construct a transition section, per Standard Plan R-60-Series, for connecting Guardrail Approach Terminal, Type 2M to guardrail Type B or Type T.

* Transition Included as Part of Guardrail Approach Terminal, Type 2M Pay Item


## Guardrail Terminal Action Plan

> Use Type 2M guardrail approach terminals for all new installations and upgrades on MDOT trunkline projects, unless deemed unfeasible due to site-specific conditions

- Use of NCHRP 350 compliant flared terminals will be permitted on a case-by-case basis
- Consult with the MDOT Geometric Design Unit, Design Division for assistance


# May be difficult to install Type 2 (tangent) approach terminal in this case 

- Consult with MDOT Geometric Design Unit, Design Division


## Possible Solution Type 2 (Tangent) Terminal Along Inside of Curve



## Guardrail Terminal Action Plan

- It will be necessary to obtain project-specific special details, and possibly develop a special provision, in order to use Type 1B or 1T guardrail approach terminals on a project.


## Guardrail Terminal Action Plan

- Use the Type 2M guardrail terminal frequently used special provision (FUSP) and Standard Plan R-62-Series when specifying Type 2M guardrail approach terminals
- Per the FUSP, manufacturers will be required to provide an electronic copy of detailed drawings, installation manuals, and maintenance manuals for each type of terminal being provided.


## Guardrail Terminal Action Plan

- Currently-approved, NCHRP 350 double sided Type 3 terminals (CAT and FLEAT-MT) will be specified until Standard Plan R-63 is updated
- CAT and FLEAT-MT will be retired and replaced by MATT and MAX-Tension Median in Standard Plan R-63
- The MATT and MAX-Tension Median will be classified as Type 3M guardrail approach terminals
- It is expected that an FUSP will be developed for Type 3M guardrail approach terminals


## Guardrail Terminal Action Plan

- Continue using Buried-in Backslope or Type 4 terminals (Special Detail 24 Series).


## Departing Terminals

- Detailed in MDOT Standard Plan R-66 Series

Important Note:

- Departing terminals may not be placed within approaching traffic's clear zone
- Not designed to withstand a head-on impact
- Comparable to blunt end


## Departing Terminals

- Type B Departing Terminals are used for terminating Type B guardrail (i.e., WBeam Guardrail)
- Type T Departing Terminals are used for terminating Type T guardrail (i.e., ThrieBeam Guardrail)
- Terminal is not flared
- It has a semi-circular end shoe
- Last post does not have an offset block
- No ground strut



## Departing Terminals

- Type MGS Departing Terminals are used for terminating Type MGS-8 guardrail
- Terminal is not flared
- It has a semi-circular end shoe
- Last post does not have an offset block
- No ground strut



## Curved Guardrail



## Curved Guardrail

Key Features:

- Used primarily when there is guardrail at intersections (e.g., driveways, freeway ramps, side streets, etc.).
- Guardrail can be terminated at the end of the curve with either an approach terminal or departing terminal.
- Guardrail may continue to run parallel to intersecting roadway beyond curved portion.
- MDOT Special Detail 21


## Use Type B-CRT guardrail along curved section when using Special Detail 21



## Curved Type B-CRT Guardrail Pay Items

Pay Item

Pay Unit
Guardrail, Curved, Type B-CRT.....................................................................................................................................................
Guardrail, Curved, Temp, Type B-CRT...........
> Defined in Frequently Used Special Provision (FUSP) 20SP-807H-01
> Clearly identifies when Special Detail 21 is applicable

- Curved Type B guardrail pay item was used previously


## Use CRT Posts Along Curved Portion of Special Detail 21



CONTROLLED RELEASING TERMINAL POST (CRT )

## Curved Guardrail

## NOTE:

FOR DRIVEWAYS, IF R.O.W. ALLOWS, USE DEPARTING END TERMINAL. (SEE STANDARD PLAN R-66-SERIES) IF R.O.W. IS LIMITED SUCH THAT A TYPICAL DEPARTING END TERMINAL CANNOT BE FIT IN, DRILL 8 HOLES IN THE CURVED BEAM GUARDRAIL TO ACCOMODATE AN ANCHOR PLATE AND INSTALL A CABLE ANCHOR SIMILAR TO THAT OF THE DEPARTING END TERMINAL ON STANDARD PLAN R-66-SERIES. THIS WILL BE PAID FOR AS GUARDRAIL, DEPARTING TERMINAL.

- Always use an approach terminal or departing terminal, as appropriate, to terminate curved guardrail
- Never use a terminal end shoe by itself
- Common mistake


## Purpose of Cable Assembly



## Curved Guardrail

## NOTE:

- Not all curved guardrail installations are constructed per Special Detail 21.

- In the example above, curved Type MGS-8 guardrail was correctly specified.
-Not constructed according to Special Detail 21.


## Grading

$1: 10$ slope or flatter at least 2'-0" feet behind guardrail posts and tapering toward road in advance of terminal


Note, this applies to ALL guardrail approach terminals

Designers must ensure grading quantities are included!

## AASHTO Roadside Design Guide Terminal Grading Recommendations <br>  <br> PREFERRED GRADING

NOT TO SCALE


ALTERNATIVE GRADING
Source: MSKT Installation Manual

## Guardrail Approach Terminal, Type 2M Grading Requirements

MDOT Standard Plan R-62 Series


## Guardrail Approach Terminal, Type 2M Grading Requirements

MDOT Standard Plan R-62 Series


Soft-Stop

## Guardrail Approach Terminal, Type 2M Grading Requirements

MDOT Standard Plan R-62 Series


Max-Tension

## Preferred Grading In Vicinity of <br> Flared Guardrail and Terminal


= 1:10 or flatter

# Brading Puantities and Pay ltems 

> Ensure earthwork and slope restoration pay items and quantities are included for all necessary grading associated with guardrail installations
> Standard guardrail pay items only include shoulder/berm grading to provide drainage

- This is very minor and does not cover significant slope regrading and other required slope work


## Lack of Grading



## Poor/Improper Grading



Hinge Point Too Close to Approach Terminal Posts
(Should be at least 2'-0" Behind Posts)

## Curb in Vicinity of Guardrail Approach Terminal

- Try to avoid placing curbs adjacent to guardrail terminals if possible. But if a curb is necessary:
- Use Type D curb or valley gutter adjacent to terminal
- Transition from high profile curb to Type D or valley gutter in advance of approach terminal
- Transition should occur at or in advance of grading transition


## Low-Profile Curb

## Placement Recommendation



L_Low-Profile Curb / No Curb Recommended



## Guardrail

## Anchorages and Transitions



## Anchorages \& Transitions

- Adequate Connection
- Block Outs as Specified
- Adequate Length
- Gradually Increase Stiffness



## Guardrail Strength Transition



- Typical transition from guardrail to concrete
- Must have gradual change in stiffiness
- Avoid sudden and extreme changes in stiffness



## M-Series Guardrail Anchorages MDOT Standard Plan R-67-Series

- There are nine different M-Series anchorages
- Determined by designer and defined in guardrail anchorage pay item
- Function of guardrail type attached to anchorage and concrete barrier type
- However, T-Series anchorages will be used for anchoring to existing concrete safety-shape railings



# MDOT Approved Guardrail Transitions 

- Guardrail Anchorage Bridge Detail M-1
- Guardrail Anchorage Bridge Detail M-2
- Guardrail Anchorage Bridge Detail M-3


MASH-Compliant Anchorages
Detailed in MDOT Standard Plan R-67 Series

# MDOT Approved Guardrail Transitions 

- Guardrail Anchorage Bridge Detail M-4
- Guardrail Anchorage Bridge Detail M-5
- Guardrail Anchorage Bridge Detail M-6


MASH-Compliant Anchorages
Detailed in MDOT Standard Plan R-67 Series

# MDOT Approved Guardrail Transitions 

- Guardrail Anchorage Bridge Detail M-7
- Guardrail Anchorage Bridge Detail M-8
- Guardrail Anchorage Bridge Detail M-9


MASH-Compliant Anchorages
Detailed in MDOT Standard Plan R-67 Series

# MDOT Approved Guardrail Transitions 

- Guardrail Anchorage Bridge Detail T-1
- Guardrail Anchorage Bridge Detail T-2
- Guardrail Anchorage Bridge Detail T-3


Detailed in MDOT Standard Plan R-67-SD
NOTES: Only Used for Connecting to Existing Safety-Shape Barriers
> T-series anchorages are NCHRP 350 Compliant

# MDOT Approved Guardrail Transitions 

- Guardrail Anchorage Bridge Detail T-4
- Guardrail Anchorage Bridge Detail T-5
- Guardrail Anchorage Bridge Detail T-6


Detailed in MDOT Standard Plan R-67-SD
NOTES: Only Used for Connecting to Existing Safety-Shape Barriers
$>$ T-series anchorages are NCHRP 350 Compliant

## Detail M-1 (Sheet 1; R-67-G)



## Detail M-2 (Sheet 2; R-67-G)

## 36.5 feet

GUARDRAIL


## Detail M-3 (Sheet 3; R-67-G)

### 42.75 feet



## Detail M-4 (Sheet 4; R-67-G)

GUARDRAIL TYPE MGS-8
$45^{\prime}-7^{3 / 4}{ }^{\prime \prime}$
GUARDRAIL ANCHORAGE, BRIDGE, DETAIL M4
39.625 feet


## Detail M-5 (Sheet 5; R-67-G)

GUARDRAIL TYPE T
$45^{\prime}-7^{3 / 4}{ }^{\prime \prime}$

### 39.625 feet



## Detail M-6 (Sheet 6; R-67-G)

## $51^{\prime}-10^{3} /_{4}^{\prime \prime}$

GUARORAIL ANCHORAGE, BRIDGE, DETALL M6


## Detail M-7 (Sheet 7; R-67-G)

$51^{\prime}-10^{3} /_{4}^{\prime \prime}$

$51^{\prime}-10^{3} 6^{*}$

POST 1 THROUCH $9-W 6 \times 9$ OR W6 $\times 8.5$ POST ( $6^{\prime}-0^{\circ}$ LONG) WITH $12^{\prime \prime}$ OFFSET BLOCK
POST 10 THROUGH $13-W 6 \times 15$ POST $\left(7^{\prime}-0^{*}\right.$ LONG) WITH $12^{*}$ OFFSET BLOCX

## Deduction Value = 39.625 feet



## Detail M-8 (Sheet 8; R-67-G)

$51^{\prime}-10^{3 / 4} 4^{\prime \prime}$
GUARDRA[L ANCHORAGE, BRIDGE, DETA]L NB


## Deduction Value = 39.625 feet



## Detail M-9 (Sheet 9; R-67-G)

$58^{\prime}-1^{3} / 4^{\prime \prime}$


Deduction Value = 45.875 feet


## Detail T-1 (Sheet 1; R-67-SD)



## Detail T-2 (Sheet 1; R-67-SD)



THRIE BEAM TERMINAL CONNECTOR
THRIE BEAM EXPANSION SECTION

BRIDCE BARRIER RAILING

## Detail T-4 (Sheet 2; R-67-SD)

GUARDRAIL ANCHORAGE. BRIDGE, DETAIL T-A ( SEE NOTES. SHEET 7 OF 7 I


## Detail T-3 (Sheet 2; R-67-SD)



SPECIAL END SHOE

## Detail T-1 (Sheet 3; R-67-SD)



THRIE BEAM TERMINAL CONNECTOR

BRIDGE BARRIER RAILING. TYPE 4

## Detail T-5 (Sheet 3; R-67-SD)

GUARDRAIL ANCHORAGE. BRIDCE. DETAIL T-5 (SEE NOTES. SHEET 7 OF 7)

$$
43^{\prime}-9^{\prime \prime}
$$



TERMINAL CONNECTOR THRIE BEAM EXPANSION SECTION
RIER RAILING, TYPE 4

## Detail T-6 (Sheet 4; R-67-SD)

GUARDRAIL ANCHORAGE, BRIDGE, DETAIL T-6 (SEE NOTES, SHEET 7 OF 7)

$$
37^{\prime}-6^{\prime \prime}
$$

SEE APPRRACH POST SPACING REQUIREMENTS CHART

$$
1^{\prime}-6^{\prime \prime}
$$

$$
1^{\prime}-6^{3 / 4}
$$

$$
\overrightarrow{M I N} .
$$

## Detail T-5 (Sheet 4; R-67-SD)

GUARDRAIL ANCHORAGE. BRIDGE, DETAIL T-5 (SEE NOTES. SHEET 7 OF 7 )

$$
43^{\prime}-9^{\prime \prime}
$$

SEE APPROACH POST SPACING REOUIREMENTS CHART
6'-3" TYPICAL POST SPACING


FIRST POST

## M-Series Guardrail Anchorages MDOT Standard Plan R-67-Series

- May Be Installed With or Without Curb \& Gutter
- However, curb height cannot exceed 4" !!
- Refer to Curb \& Gutter Details from Standard Plan R-32 Series
- Bridge Approach Curb \& Gutter, Details 5 through 7



## T-Series Guardrail Anchorages MDOT Standard Plan R-67-SD

- Curb \& Gutter Required with Safety-Shape Barrier
- Curb height is 12 " !!
- Refer to Curb \& Gutter Details from Standard Plan R-32-SD
- Bridge Approach Curb \& Gutter, Details 1 through 3



# MDOT Approved Guardrail Transitions 

Standard Plan B-22 and B-23 Series

- Guardrail Anchorage, Bridge, Detail A-3
- Guardrail Anchorage, Bridge, Detail A-4
- Guardrail Anchorage, Bridge, Detail A-5



# MDOT Approved Guardrail Transitions 

## Standard Plan B-22 and B-23 Series



- May be constructed with or without curb
- $4^{\prime \prime}$ max curb height !!


# MDOT Approved Guardrail Transitions 

- Guardrail

Anchorage, Median

- Used to connect double-sided guardrail to concrete barrier


Detailed in MDOT Standard Plan R-71 Series NCHRP 350 Compliant



Figure 2.6.1-Roadside barrier elements
2.6.1

## Guardrail Terminal Selection

One-Way Traffic


## Guardrail Terminal Selection

Two-Way Traffic


## Guardrail Terminal Selection

Two-Way Traffic


## Runout Length

Edge of Pavement

Hazard


## Runout Length

Traffic Volume (ADT) veh/day

|  | Traffic Volume (ADT) veh/day |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Over 10,000 | Over <br> $5,000-10,000$ | $\mathbf{1 0 0 0 - 5 0 0 0}$ | Under 1000 |
| Design Speed <br> $(\mathrm{mph})$ | Runout Length <br> $\mathrm{L}_{\mathrm{R}}(\mathrm{ft})$ | Runout Length <br> $\mathrm{L}_{\mathrm{R}}(\mathrm{ft})$ | Runout Length <br> $\mathrm{L}_{\mathrm{R}}(\mathrm{ft})$ | Runout Length <br> $\mathrm{L}_{\mathrm{R}}(\mathrm{ft})$ |
| 80 | 470 | 430 | 380 | 330 |
| 70 | 360 | 330 | 290 | 250 |
| 60 | 300 | 250 | 210 | 200 |
| 50 | 230 | 190 | 160 | 150 |
| 40 | 160 | 130 | 110 | 100 |
| 30 | 110 | 90 | 80 | 70 |

- RDM - Section 7.01.19
- Runout length is a function of design speed and traffic volume - Interpolation is recommended for intermediate design speeds
- Example: DS = $75 \mathrm{mph} \& ~ A D T=12,000: \mathrm{L}_{\mathrm{r}}=415^{\prime}$


## Minimum

Length of Barrier Needed


AASHTO Method: $\Phi$ typically varies between $25^{\circ}$ and $90^{\circ}$

## Length of Barrier Needed



MDOT's Current Method: $\boldsymbol{\Phi}=90^{\circ}$

## Design Factors

## Clear Zone Line



Note: Edge of Pavement (a.k.a. Edge of Metal)

CLEAR ZONE DISTANCES
(IN FEET FROM EDGE OF DRIVING LANE)

| DESIGN SPEED | $\begin{aligned} & \text { DESIGN } \\ & \text { ADT } \end{aligned}$ | FILL SLOPES |  |  | CUT SLOPES |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} \text { 1:6 } \\ \text { OR } \\ \text { FLATTER } \end{gathered}$ | $\begin{aligned} & 1: 5 \\ & \text { TO } \\ & 1: 4 \end{aligned}$ | 1:3 | 1:3 | $\begin{aligned} & 1: 4 \\ & \text { TO } \\ & 1: 5 \end{aligned}$ | $\begin{gathered} 1: 6 \\ \text { OR } \\ \text { FLATTER } \end{gathered}$ |
| $\begin{array}{\|c\|} 40 \mathrm{mph} \\ \text { or } \\ \text { Less } \end{array}$ | under 750 | 7-10 | 7-10 | ** | 7-10 | 7-10 | 7-10 |
|  | 750-1500 | 10-12 | 12-14 | ** | 10-12 | 12-14 | 12-14 |
|  | 1500-6000 | 12-14 | 14-16 | ** | 12-14 | 14-16 | 14-16 |
|  | over 6000 | 14-16 | 16-18 | ** | 14-16 | 16-18 | 16-18 |
| $\begin{gathered} 45-50 \\ \mathrm{mph} \end{gathered}$ | under 750 | 10-12 | 12-14 | ** | 8-10 | 8-10 | 10-12 |
|  | 750-1500 | 14-16 | 16-20 | ** | 10-12 | 12-14 | 14-16 |
|  | 1500-6000 | 16-18 | 20-26 | ** | 12-14 | 14-16 | 16-18 |
|  | over 6000 | 20-22 | 24-28 | ** | 14-16 | 18-20 | 20-22 |
| $\begin{gathered} 55 \\ \mathrm{mph} \end{gathered}$ | under 750 | 12-14 | 14-18 | ** | 8-10 | 10-12 | 10-12 |
|  | 750-1500 | 16-18 | 20-24 | ** | 10-12 | 14-16 | 16-18 |
|  | 1500-6000 | 20-22 | 24-30 | ** | 14-16 | 16-18 | 20-22 |
|  | over 6000 | 22-24 | 26-32* | ** | 16-18 | 20-22 | 22-24 |
| $\begin{gathered} 60 \\ \mathrm{mph} \end{gathered}$ | under 750 | 16-18 | 20-24 | ** | 10-12 | 12-14 | 14-16 |
|  | 750-1500 | 20-24 | 26-32* | ** | 12-14 | 16-18 | 20-22 |
|  | 1500-6000 | 26-30 | 32-40* | ** | 14-18 | 18-22 | 24-26 |
|  | over 6000 | 30-32* | 36-44* | ** | 20-22 | 24-26 | 26-28 |
| $\begin{aligned} & \geq 65 \\ & \mathrm{mph} \end{aligned}$ | under 750 | 18-20 | 20-26 | ** | 10-12 | 14-16 | 14-16 |
|  | 750-1500 | 24-26 | 28-36* | ** | 12-16 | 18-20 | 20-22 |
|  | 1500-6000 | 28-32* | 34-42* | ** | 16-20 | 22-24 | 26-28 |
|  | over 6000 | 30-34* | 38-46* | ** | 22-24 | 26-30 | 28-30 |

Where a site specific investigation indicates a high probability of continuing crashes, or such occurrences are indicated by crash history, the designer may provide clear zone distances greater than 30 feet as indicated. Clear zones may be limited to 30 feet for practicality and to provide a consistent roadway template if previous experience with similar projects or designs indicates satisfactory performance.
$*$ Since recovery is less likely on the unshielded, traversable $1: 3$ slopes, fixed objects should not be present in the vicinity of the toe of these slopes.

## Design Factors

## Clear Zone Line



## Design Factors

## Clear Zone Line



## Design Factors

## Clear Zone Line



## Design Factors

## Clear Zone Line



## MDOT Shy Distance Table

| Design Speed (mph) | Shy Line Offset (Ls ) (ft) |
| :---: | :---: |
| 80 | 12 |
| 75 | 10 |
| 70 | 9 |
| 60 | 8 |
| 55 | 7 |
| 50 | 6.5 |
| 45 | 6 |
| 40 | 5 |
| 30 | 4 |

RDM - Section 7.01.18

## Design Factors

## Clear Zone Line



## Runout Length Table

|  | Traffic Volume (ADT) veh/day |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Over 10,000 | Over <br> $5,000-10,000$ | $1000-5000$ | Under 1000 |
| Design Speed <br> $(\mathrm{mph})$ | Runout Length <br> $\mathrm{L}_{R}(\mathrm{ft})$ | Runout Length <br> $\mathrm{L}_{R}(\mathrm{ft})$ | Runout Length <br> $\mathrm{L}_{R}(\mathrm{ft})$ | Runout Length <br> $L_{R}(\mathrm{ft})$ |
| 80 | 470 | 430 | 380 | 330 |
| 70 | 360 | 330 | 290 | 250 |
| 60 | 300 | 250 | 210 | 200 |
| 50 | 230 | 190 | 160 | 150 |
| 40 | 160 | 130 | 110 | 100 |
| 30 | 110 | 90 | 80 | 70 |

RDM - Section 7.01.19

## Design Factors

## Clear Zone Line



MDOT Guardrail Worksheet specifies $\mathrm{L}_{1}$ must be 25 ' min., but there are exceptions:

- Guardrail bridge anchorages
- Guardrail installations with a large offset between the hazard and the guardrail


## Bridge Approach Rail



* Use $L_{1}=L_{T}$ even when $L_{T}<25$ '


## Design Factors

## Clear Zone Line



## AASHTO RDG Table 5-9 Recommended Flare Rates

Table 5-9. Suggested Flare Rates for Barrier Design

| Design Speed |  | Flare Rate for <br> Barrier Inside <br> Shy Line | Flare Rate for Barrier at <br> or Beyond Shy Line |  |
| :---: | :---: | :---: | :---: | :---: |
| $\mathbf{k m} / \mathbf{h}$ | [mph] | A | B |  |
| 110 | $[70]$ | $30: 1$ | $20: 1$ | $15: 1$ |
| 100 | $[60]$ | $26: 1$ | $18: 1$ | $14: 1$ |
| 90 | $[55]$ | $24: 1$ | $16: 1$ | $12: 1$ |
| 80 | $[50]$ | $21: 1$ | $14: 1$ | $11: 1$ |
| 70 | $[45]$ | $18: 1$ | $12: 1$ | $10: 1$ |
| 60 | $[40]$ | $16: 1$ | $10: 1$ | $8: 1$ |
| 50 | $[30]$ | $13: 1$ | $8: 1$ | $7: 1$ |

Notes:
A = Suggested maximum flare rate for rigid barrier system.
$B=$ Suggested maximum flare rate for semi-rigid barrier system.
In most cases, use flare rate at or beyond shy line column even when guardrail is within the shy line.

## Design Factors

## NOTES: TYPE 1 TERMINAL ILLUSTRATED

$\frac{b}{a}($ FLARE RATE $)=0$ WHEN THE GUARDRAIL RUN IS TANGENT


Note: $d$ and $Z$ are not described in the AASHTO RDG

## Design Factors

## Clear Zone Line



## Design Factors

## Clear Zone Line



Note: Y is a term from the AASHTO RDG typically not used by MDOT.

## Design Factors

## Clear Zone Line



$$
\mathrm{Z}=\mathrm{L}_{2}+\mid\left(\text { Sta. }_{\mathrm{B}}-\text { Sta. }_{\mathrm{A}}\right) \mid \times(\mathrm{b} / \mathrm{a})
$$

## Calculating Z



## Calculating Stations $A$ and $B$



Assume L $\approx$ L' for most guardrail applications (unless dealing with extremely long flared sections)

## Graphic Solution



Vehicular trajectory must intersect or be located in advance of beginning length of need (BLON) point

## Horizontal Curve Solution

 leaves the roadway (at location $\mathrm{P}_{\mathrm{T}}$ )

## Length of Need - Approach End Flared vs. Parallel



Figure 2.6.5-Simplified representation of length of need

Flaring the guardrail reduces the length of need (X)

## Length of Need - Departing End Flared vs. Parallel



Flaring the guardrail reduces the length of need (X)

## Grading Requirements



> = 1:10 or flatter

- Grading requirements for flared installations may be impractical or cost-prohibitive
- Decision to install flared or parallel guardrail run is site-specific


## Calculating Length of Guardrail

Freestanding Guardrail Shielding Fixed Object \& One-Way Traffic



$$
G^{*}=X-M+H
$$

## M (Deduction Value)

 MDOT Guardrail Worksheet
## DEDUCTION TABLE

## GUARDRAIL APPROACH TERMINAL TYPE

| $1 B$ | 1 T | $2 B$ | 2 T | 2 M | $3 B$ | 3 T |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $25^{\prime}$ | $31.25^{\prime}$ | $37.5^{\prime}$ | $43.75^{\prime}$ | $34.3^{\prime}$ | $12.5^{\prime}$ | $31.25^{\prime}$ |

Example:
For Type 2M terminals, use 34.3' for the deduction value

## Soft-Stop (Type 2M Terminal)



Of the three MDOT-approved Type 2M terminals, Soft-Stop has the smallest deduction value

- Use deduction value of 34.3 ' when specifying a Type 2M terminal


# Calculating Length of Guardrail 

## Freestanding Guardrail Shielding Fixed Object \& One-Way Traffic

- $\mathrm{H}=$ fixed object width
- $M=$ portion of approach terminal located within length of need
- Deduction values from guardrail worksheet
- $G=$ guardrail quantity

$$
G^{*}=X-M+H
$$

* Important Notes
- Always round up guardrail quantity based on whole number of guardrail panels
> With a freestanding run consisting of Type 2M approach terminals, Type MGS-8 guardrail, and/or Type MGS departing terminals, guardrail quantity will be divisible by $12.5^{\prime}$
> When interconnecting NCHRP 350 and MASH-compliant guardrail features, guardrail quantity might not be divisible by 12.5
\& Examples: Type MGS-8 guardrail to Type B or Type T guardrail, or Type MGS-8 guardrail to NCHRP 350-compliant anchorages
* Must take MGS ( $9^{\prime}-4.5^{\prime \prime}$ ) beam elements and thrie-beam transition panels into consideration when determining guardrail quantities


## MDOT Standard Plan R-60-Series



ELEVATION SHOWING TRANSITION DETAIL FOR CONNECTING GUARDRAIL, TYPE MGS-8 OR MGS-8D TO
GUARDRAIL, TYPE B, GUARDRAIL, TYPE BD, OR GUARDRAIL APPROACH TERMINAL TYPE 1B, 2B, OR 3B

Note: Transition is part of Guardrail, Type MGS-8 or MGS-8D

## MDOT Standard Plan R-60-Series



ELEVATION SHOWING TRANSITION DETAIL FOR CONNECTING
GUARDRAIL, TYPE MGS-8 OR MGS-8D TO GUARDRAIL, TYPE T, GUARDRAIL, TYPE TD, GUARDRAIL ANCHORAGE, MEDIAN,
GUARDRAIL ANCHORAGE, BRIDGE DETAIL A1, T1, T4 OR T6
Note: Transition is part of Guardrail, Type MGS-8 or MGS-8D

## MDOT Standard Plan R-60-Series



Note: Transition is part of Guardrail Approach Terminal, Type 2M

## MDOT Standard Plan R-60-Series



Note: Transition is part of Guardrail Approach Terminal, Type 2M

## Calculating Length of Guardrail

Guardrail Anchored to Bridge Railing


## Calculating Length of Guardrail

## Guardrail Anchored to Bridge Railing

- $\mathrm{T}=$ transition length measured from edge of bridge railing/barrier (if applicable)
- Do not deduct overall transition length
- Deduction lengths for M-series and T-series anchorages provided in earlier slides
- $M=$ portion of approach terminal located within length of need
- Deduction values from guardrail worksheet
- $\mathrm{G}=$ guardrail quantity

$$
G^{*}=X-M-T
$$

* Important Notes
> Always round up guardrail quantity to the nearest whole number of guardrail panels
$>$ Must take MGS (9'-4.5") beam elements and thrie-beam transition panels into consideration when determining guardrail quantities
* Guardrail quantity may not be divisible by $12.5^{\prime}$ in certain cases


## Reflectors

- MDOT Standard Plan R-60 Series describes recommended reflector spacing
- Do not install reflectors on approach terminals

$$
N_{R}=\left(\frac{\text { Guardrail Length }^{*}}{\text { Reflector Spacing }}\right)+1
$$

$N_{R}$ is always rounded up to nearest integer

* Total Guardrail Length, including anchorages, but excluding approach terminals


## Reflectors

- One-Way Roads:
- Reflector quantity $=\mathrm{N}_{\mathrm{R}}$
- Two-Way Roads:
- Reflector quantity $=2 \mathrm{~N}_{\mathrm{R}}$


ONE-WAY TRAFFIC

$\Longleftarrow$ DIRECTION
DIRECTION


TWO-WAY TRAFFIC
PLACEMENT OF GUARDRAIL REFLECTORS

## Common Design Problem

## Driveway



# Described in Section 7.01.30. H of RDM 

Driveway




Driveway


Otherwise, consider continuing guardrail past intersecting driveway until LON is satisfied


## Other Factors

- Sight Distance
- Run Length
- Right of Way
- Multiple Drives


However, designers must take other factors into consideration...design is site-specific!!



## Practice Example \#1

$>$ ADT: 4,500 vpd

> Design Speed: 60 mph
$>$ Slope: 1:5, Fill
> Non-Freeway
> Flare guardrail where possible
> Two-lane, two-way road with 12' lanes

EOP

## Practice Example \#1



CLEAR ZONE DISTANCES
(IN FEET FROM DGE OF DRIVING LANE)

| DESIGN SPEED | $\begin{aligned} & \text { DESIGN } \\ & \text { ADT } \end{aligned}$ | FILL SLPES |  |  | CUT SLOPES |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $1: 6$ OR FLATTER | $\begin{aligned} & 1: 5 \\ & \text { TO } \\ & 1: 4 \end{aligned}$ | 1:3 | 1:3 | $\begin{aligned} & 1: 4 \\ & \text { TO } \\ & \text { 1:5 } \end{aligned}$ | 1:6 OR <br> FLATTER |
| $\begin{gathered} 40 \mathrm{mph} \\ \text { or } \\ \text { Less } \end{gathered}$ | under 750 | 7-10 | 7-10 | ** | 7-10 | 7-10 | 7-10 |
|  | 750-1500 | 10-12 | 12-14 | ** | 10-12 | 12-14 | 12-14 |
|  | 1500-6000 | 12-14 | 14-16 | ** | 12-14 | 14-16 | 14-16 |
|  | over 6000 | 14-16 | 16-18 | ** | 14-16 | 16-18 | 16-18 |
| $\begin{aligned} & \text { 45-50 } \\ & \mathrm{mph} \end{aligned}$ | under 750 | 10-12 | 12-14 | ** | 8-10 | 8-10 | 10-12 |
|  | 750-1500 | 14-16 | 16-20 | ** | 10-12 | 12-14 | 14-16 |
|  | 1500-6000 | 16-18 | 20-26 | ** | 12-14 | 14-16 | 16-18 |
|  | over 6000 | 20-22 | 24-28 | ** | 14-16 | 18-20 | 20-22 |
| $\begin{gathered} 55 \\ \mathrm{mph} \end{gathered}$ | under 750 | 12-14 | 14-18 | ** | 8-10 | 10-12 | 10-12 |
|  | 750-1500 | 16-18 | 20-24 | ** | 10-12 | 14-16 | 16-18 |
|  | 1500-6000 | 20-22 | 24-30 | ** | 14-16 | 16-18 | 20-22 |
|  | over 6000 | 22-24 | 26-32* | ** | 16-18 | 20-22 | 22-24 |
| $\begin{gathered} 60 \\ \mathrm{moh} \end{gathered}$ | under 750 | 16-18 | 20-24 | ** | 10-12 | 12-14 | 14-16 |
|  | 750-1500 | 20-24 | 26-32* | ** | 12-14 | 16-18 | 20-22 |
|  | 1500-6000 | 26-30 | 32-40* | ** | 14-18 | 18-22 | 24-26 |
|  | over 6000 | 30-32* | 36-44* | ** | 20-22 | 24-26 | 26-28 |
| $\begin{aligned} & \geq 65 \\ & \mathrm{mph} \end{aligned}$ | under 750 | 18-20 | 20-26 | ** | 10-12 | 14-16 | 14-16 |
|  | 750-1500 | 24-26 | 28-36* | ** | 12-16 | 18-20 | 20-22 |
|  | 1500-6000 | 28-32* | 34-42* | ** | 16-20 | 22-24 | 26-28 |
|  | over 6000 | 30-34* | 38-46* | ** | 22-24 | 26-30 | 28-30 |

Where a site specific investigation indicates a high probability of continuing crashes, or such occurrences are indicated by crash history, the designer may provide clear zone distances greater than 30 feet as indicated. Clear zones may be limited to 30 feet for practicality and to provide a consistent roadway template if previous experience with similar projects or designs indicates satisfactory performance.
${ }^{* *}$ Since recovery is less likely on the unshielded, traversable $1: 3$ slopes, fixed objects should not be present in the vicinity of the toe of these slopes.

## Questions

- Which guardrail type should be used?
$\checkmark$ Type MGS-8
- Which terminal type should be used on the approach end of the guardrail run?
$\checkmark$ Guardrail Approach Terminal, Type 2M
$\checkmark$ Terminal within clear zone of approaching traffic
- Which terminal type should be used on the departing end of the guardrail run?
$\checkmark$ Guardrail Approach Terminal, Type 2M
$\checkmark$ Terminal within clear zone of opposing traffic


GUARDRAJL RUN \# $\qquad$
FJXED OBJECT


NOTES: TYPE 1 TERUCNAL JLUSTRATED


$$
X=\frac{L_{H}+\left(\frac{b}{a}\right)\left(L_{1}\right)-\left(L_{z}+d\right)}{\frac{b}{a}+\frac{L_{H}}{L_{R}}}
$$

$$
Z=L_{g^{+}}\left(\left|S_{B}-S_{A}\right|\right)\left(\frac{b}{a}\right)
$$

LEMGTH OF NEED guardrall taper rate (7.01.29a)
E.O.P. TO FACE OF BARRIER (DESJGMED)

CLEAR ZONE ( 7.01.11 )
$\qquad$
$\qquad$ ........ ..... $\qquad$
$X=$ $\qquad$
$L_{R}=$ $=$ $\qquad$
$=$
$\square$
$c$ $\square$${ }_{s}=$
$=$
$\square$ EFFECTJYE TURNED OUT DISTANCE OF ANCHORAGE ...d =
lateral extent of roadside feature (neasuredl. $L_{H}=$
Lateral offset at end of flare................. $Z=$ $\qquad$
NOTE: DJSTANCE OF OBJECT FRON baCE OF baRRIER wUSt be greater tham the maxchum deflection ( 7.01 .20 )
$L_{H} \leq L_{C}$
refer to standard plan r-59-SErles and destge manual
SECTLON 7.01 .30 FOR GUARDRALL AT EMBAMKMENTS

$\qquad$

## CALCULATIONS OR NOTES

## Pay [TENS



| DEDUCTLON TABLE |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| GUARDRAJL APPROACH TERMJNAL TYPE |  |  |  |  |  |  |
| 18 | 1 T | 28 | 2 T | 2 N | 38 | 3 T |
| $25^{\prime}$ | $31.25^{\prime}$ | $37.5^{\prime}$ | $43.75^{\prime}$ | $34.3^{\prime}$ | $12.5^{\prime}$ | $31.25^{\prime}$ |

PAY LENGTHS MUST BE DJVJSJBLE BY 12.5'.
ROUND TO NEXT HJGHEST RA[L LENGTH, EXCEPT WHEN TYPE MGS-8 OR TYPE NGS-BD GUARDRALL IS ATTACHED TO A GUARDRALL FEATURE REOULRLNG A HE[GHT TRANS[T]ON (e.g., GUARDRA[L APPROACH A HE[GHT TRANSITION (e.g., GUARDRALL APPR GUARDRA[L BRLDCE ANCHORAGE; otc.)

* FOR THIS PAY JTEM, THE GUARDRAJL APPROACH TERUINAL, TYPE PORTION OF LENGTH OF NEED $(X)$ MUST BE DEDUCTED

|  | Traffic Volume (ADT) veh/day |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Over 10,000 | Over <br> $5,000-10,000$ | $\mathbf{1 0 0 0 - 5 0 0 0}$ | Under 1000 |
| Design Speed <br> (mph) | Runout Length <br> $L_{R}(\mathrm{ft})$ | Runout Length <br> $\mathrm{L}_{R}(\mathrm{ft})$ | Runout Length <br> $\mathrm{L}_{R}(\mathrm{ft})$ | Runout Length <br> $L_{R}(\mathrm{ft})$ |
| 80 | 470 | 430 | 380 | 330 |
| 70 | 360 | 330 | 290 | 250 |
| 60 | 300 | 250 | 210 | 200 |
| 50 | 230 | 190 | 160 | 150 |
| 40 | 160 | 130 | 110 | 100 |
| 30 | 110 | 90 | 80 | 70 |


| Design Speed (mph) | Shy Line Offset (Ls) (ft) |
| :---: | :---: |
| 80 | 12 |
| 75 | 10 |
| 70 | 9 |
| 60 | 8 |
| 55 | 7 |
| 50 | 6.5 |
| 45 | 6 |
| 40 | 5 |
| 30 | 4 |

## Practice Example \#1



Shy distance for $60 \mathrm{mph}=8 \mathrm{ft}$
Clear Zone = 40 feet


## MDOT

## Guardrail Deflection Table

| Guardrail | Post Spacing | Minimum Design Offset * |
| :---: | :---: | :---: |
| Type T | 1'-63/4" | 1'-2" |
| Type T | $3^{\prime}-11 / 2^{\prime \prime}$ | Sth 1'-8" |
| Type T | 6'-3" | 2'-0" |
| Type B | 1'-63/4" | 1'-6" |
| Type B | $3^{\prime}-11 / 2^{\prime \prime}$ | 2'-0" |
| Type B | 6'-3" | 3'-0" |
| Type MGS-8 | 1'-63/4" | 2'-5" |
| Type MGS-8 | $3^{\prime}-11 / 2^{\prime \prime}$ | 2'-11" |
| Type MGS-8 | $6^{\prime}-3$ " | (-3'-6"_) ${ }^{\text {a }}$ |
| Type MGS-8 Adjacent to Curb | 6'-3" | 4'-1" |
| Type MGS-8 Near Shoulder Hinge Point ** | 6'-3" | 4'-1" |

RDM - Section 7.01.20


## AASHTO RDG Table 5-9 Recommended Flare Rates

Table 5-9. Suggested Flare Rates for Barrier Design

| Design Speed |  | Flare Rate for <br> Barrier Inside <br> Shy Line | Flare Rate for Barrier at <br> or Beyond Shy Line <br> $\mathbf{k m} / \mathbf{h}$ |  |
| :---: | :---: | :---: | :---: | :---: |
| $\mathbf{[ m p h}]$ | $[70]$ | $30: 1$ | $\mathbf{A}$ | B |
| 110 | $[60]$ | $26: 1$ | $18: 1$ | $15: 1$ |
| 100 | $[55]$ | $24: 1$ | $16: 1$ | $14: 1$ |
| 90 | $[50]$ | $21: 1$ | $14: 1$ | $12: 1$ |
| 80 | $[45]$ | $18: 1$ | $12: 1$ | $11: 1$ |
| 70 | $[40]$ | $16: 1$ | $10: 1$ | $10: 1$ |
| 60 | $[30]$ | $13: 1$ | $8: 1$ | $8: 1$ |
| 50 |  |  |  | $7: 1$ |

Notes:
A = Suggested maximum flare rate for rigid barrier system.
$B=$ Suggested maximum flare rate for semi-rigid barrier system.
In most cases, use flare rate at or beyond shy line column even when guardrail is within the shy line.

## Practice Example \#1



## Practice Example \#1



## Practice Example \#1


$X=\frac{L_{H}+(b / a)\left(L_{1}\right)-\left(L_{2}+d\right)}{(b / a)+\left(L_{H} / L_{R}\right)}$

## Practice Example \#1



## Practice Example \#1



## Practice Example \#1



## Opposing Traffic

Clear Zone Line


12' lanes
$\mathrm{L}_{\mathrm{c}}=40^{\prime}$

## Practice Example \#1


$X=\frac{L_{H}+(b / a)\left(L_{1}\right)-\left(L_{2}+d\right)}{(b /)+\left(L_{H} / L_{R}\right)}$

## Practice Example \#1



$$
X=\frac{L_{H}+(b / a)\left(L_{1}\right)-\left(L_{2}+d\right)}{(b / a)+\left(L_{H} / L_{R}\right)}=\frac{27+(1 / 14)(25)-(20+0)}{(1 / 14)+(27 / 250)}=?
$$

## Practice Example \#1



## Practice Example \#1



# Deduction Value Type 2M Approach Terminal MDOT Guardrail Worksheet 

## DEDUCTION TABLE

GUARDRAIL APPROACH TERMINAL TYPE

| $1 B$ | 1 T | $2 B$ | 2 T | $(\overline{2 M})$ | 3 B | 3 T |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $25^{\prime}$ | $31.25^{\prime}$ | $37.5^{\prime}$ | $43.75^{\prime}$ | $\left(\overline{3} \overline{3} \mathbf{B}^{\prime}\right)$ | $12.5^{\prime}$ | $31.25^{\prime}$ |

## Practice Example \#1

BLON

## Calculating Guardrail Quantity

Number of Guardrail Panels

- Type MGS-8 guardrail connected to Type 2M approach terminals
- Guardrail quantity is divisible by 12.5 (i.e., whole number of 12.5' panels)

$$
\frac{\mathrm{G}_{\min }}{12.5}=\frac{48.2}{12.5}=3.86 \longrightarrow 4 \text { panels }
$$

Type MGS-8 Guardrail Length $=(12.5)(4)=50 \mathrm{ft}$

## Reflectors

- Do not install reflectors on approach terminals

$$
N_{R}=\left(\frac{50}{50}\right)+1=2 \longrightarrow 2
$$

Since this is a two-way road, number of reflectors is $2 N_{R}$ :
Number of Reflectors =2(2) = 4

## Practice Example \#2



## Design Data \& Assumptions

- Rural Two-Lane Road
- Design Speed = 55 mph
- ADT $=5,000 \mathrm{vpd}$
- River is $6^{\prime}$ deep
- $1: 5$ Slope in advance of bridge ends
- Flare guardrail where possible


## NE Quadrant

## Determining Guardrail Components

Guardrail Anchored to Bridge Railing


## Detail T-1 (Sheet 1 of R-67-SD)



## Determining Guardrail Components

Guardrail Anchored to Bridge Railing

route. Practice Example \#2 control SEction 99999 Job \#EXAMPLE DESIGNED BY _ABC __ DATE .00/01/18 CHECKED BY XYZ __ DATE 00/01/18

APPROX. STATION OR M.P346+78 DESCRIPTION Practice Example \#2 GUARDRAIL RUN \# INE Quad

IF STATION]NG [S NOT AVAILABLE, LOCATE TO NEAREST FIXED OBJECT

NOTES: TYPE 1 TERMINAL [LLUSTRATED

$$
\begin{aligned}
& d=1.88^{\text {FOR TYPE }} 1 \text { TERMINALS } \\
& d=0 \text { FOR TYPE } 2 \text { AND } 3 \text { TERMIN }
\end{aligned}
$$

$$
X=\frac{L_{H}+\left(\frac{b}{a}\right)\left(L_{1}\right)-\left(L_{2}+d\right)}{\frac{b}{a}+\frac{L_{H}}{L_{R_{n}}}}
$$

$$
Z=L_{2}+\left(\left|S_{B}-S_{A}\right|\right)\left(\frac{b}{a}\right)
$$

|  |  |
| :--- | :--- |
| DESIGN ADT | $5,000 \mathrm{vpd}$ |
| DESICN SPEED | 55 mph |
| APPROACH SLOPE | $1: 5$ |

E.O.P. TO ROADSIDE FEATURE (MEASUREDI $\ldots \ldots . . . . L_{3}=.4$

EFFECTIVE TURNED OUT DJSTANCE OF anchorace $\ldots \mathrm{d}=0$
$L_{1}=23.125^{\prime}$ ' u[s. )
$L_{s}=\ldots 7^{\prime} \quad$ SHY LINE ( 7.01 .18 )
station at a $-347+01.1$
station at в $-347+66.8$
Lateral extent of roadstde feature (veasuredi. $L_{H}=3^{\prime}$
lateral offset at end of flare. $\qquad$ $. z=9.47^{\text {** }}$

NOTE: DISTANCE OF OBJECT FROW BACK OF BARRIER MUST BE greater than the max[wuy deflection ( $7,01,20$ ) ** Refer to Calculations and Notes $L_{H} \leq L_{c}$

$$
\begin{aligned}
& d=1.8^{\prime} \text { FOR TYPE } 1 \text { TERMINALS } \\
& d=0 \text { FOR TYPE } 2 \text { AND } 3 \text { TERMINALS }
\end{aligned}
$$

$$
X=\frac{L_{H}+\left(\frac{b}{a}\right)\left(L_{1}\right)-\left(L_{2}+d\right)}{\frac{b}{a}+\frac{L_{H}}{L_{R}}}
$$

$$
Z=L_{2}+\left(\left|S_{B}-S_{A}\right|\right)\left(\frac{b}{a}\right)
$$

$$
\text { E.O.P. TO FACE OF BARRIER (DESIGNEDI } \ldots \ldots . . . . . L_{2}=\frac{a}{4^{\prime}}
$$

$$
\text { CLEAR ZONE }(7.01 .11), \ldots . . . . . . . . . . . . . . . . . . . . . L_{c}={ }_{c} 3^{\prime}
$$

$$
L_{1}=.23 .125^{\prime} \quad \text { 'и[N. ) }
$$

$$
\text { E.O.P. TO ROADSIDE FEATURE (MEASURED) } \ldots \ldots, \ldots, L_{3}=.4^{\prime}
$$

$$
\text { EFFECTJVE TURNED OUT DISTANCE OF ANCHORAGE } \ldots d=0
$$

$$
L_{s}=\ldots 7^{\prime} \quad \text { SHY LINE }(7.01 .18 \text { ) }
$$

$$
\text { Lateral extent of roadside feature (weasured). } L_{H}=-30^{\prime}
$$

$$
\text { station at a }-347+01.1
$$

$$
\text { STATION AT 日 } \quad-347+66.8
$$

$$
\text { Lateral offset at end of flare ................... } Z=9.47^{\text {** }}
$$

## Runout Length Table

|  | Traffic Volume (ADT) veh/day |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Over 10,000 | $\begin{gathered} \text { Over } \\ 5,000-10,000 \end{gathered}$ | 1000-5000 | Under 1000 |
| Design Speed (mph) | Runout Length $L_{R}(\mathrm{ft})$ | Runout Length $L_{R}(\mathrm{ft})$ | Runout Length $\mathrm{L}_{\mathrm{R}}(\mathrm{ft})$ | Runout Length $\mathrm{L}_{\mathrm{R}}(\mathrm{ft})$ |
| 80 | 470 | 430 | 380 | 330 |
| 70 | 360 | 330 | 290 | 250 |
| 60 | 300 | 250 | I 210 | 200 |
| 50 | 230 | 190 | 1 160 | 150 |
| 40 | 160 | 130 | 110 | 100 |
| 30 | 110 | 90 | 80 | 70 |

RDM - Section 7.01.19
${ }^{* *}$ Must interpolate in this case to obtain $L_{R}$

$$
\begin{aligned}
& d=1.8^{\prime} \text { FOR TYPE } 1 \text { TERMINALS } \\
& d=0 \text { FOR TYPE } 2 \text { AND } 3 \text { TERMINALS }
\end{aligned}
$$

$$
X=\frac{L_{H}+\left(\frac{b}{a}\right)\left(L_{1}\right)-\left(L_{2}+d\right)}{\frac{b}{a}+\frac{L_{H}}{L_{R}}}
$$

$$
Z=L_{2}+\left(\left|S_{B}-S_{A}\right|\right)\left(\frac{b}{a}\right)
$$

$$
\text { LENGTH OF NEED } \ldots . . . . . . . . . . . . . . . . . . . . . . . . . . X=\frac{113.76^{\prime}}{185^{\prime}} \text { DESIGN ADT }
$$

$$
\text { GUARDRAIL TAPER RATE (R-59-SERLES) } \ldots \ldots \ldots \cdot \frac{b}{a}=\frac{\overline{1 / 12}}{1^{\prime}} \quad \text { APPROACH SLOPE }
$$

$$
\begin{aligned}
& \text { E.O.P. TO FACE OF BARREER (DESIGNED) } \ldots . . . . . . . . L_{2}=\frac{a}{4} \\
& \text { CLEAR ZONE }(7.01 .11) \ldots . . . . . . . . . . . . . . . . . . . . . L_{c}=-30^{\prime}
\end{aligned}
$$

$$
L_{1}=.23 .125^{\prime} \quad \text { ' и[N. ) }
$$

$$
\text { E.O.P. TO ROADSIDE FEATURE (MEASURED) } \ldots \ldots, \ldots, L_{3}=.4^{\prime}
$$

$$
\text { EFFECTJVE turned out distance of anchorace } \ldots d=0
$$

$$
L_{s}=\ldots 7 ' \text { SHY LINE ( } 7.01 .18 \text { ) }
$$

$$
\text { Lateral extent of roadside feature (weasured). } L_{H}=-30^{\prime}
$$

$$
\text { station at a }-347+01.1
$$

$$
\text { STATION AT a }-347+66.8
$$

$$
\text { lateral offset at end of flare. .................. } Z=9.47^{\text {n* }}
$$

## AASHTO RDG Table 5-9 Recommended Flare Rates

Table 5-9. Suggested Flare Rates for Barrier Design

| Design Speed |  | Flare Rate for <br> Barrier Inside <br> Shy Line | Flare Rate for Barrier at <br> or Beyond Shy Line <br> $\mathbf{k m} / \mathbf{h}$ |  |
| :---: | :---: | :---: | :---: | :---: |
| $\mathbf{[ m p h}]$ | $[70]$ | $30: 1$ | $\mathbf{A}$ | B |
| 110 | $[60]$ | $26: 1$ | $18: 1$ | $15: 1$ |
| 90 | $[55]$ | $24: 1$ | $16: 1$ | $14: 1$ |
| 80 | $[50]$ | $21: 1$ | $14: 1$ | $12: 1$ |
| 70 | $[45]$ | $18: 1$ | $12: 1$ | $11: 1$ |
| 60 | $[40]$ | $16: 1$ | $10: 1$ | $10: 1$ |
| 50 | $[30]$ | $13: 1$ | $8: 1$ | $8: 1$ |

Notes:
A = Suggested maximum flare rate for rigid barrier system.
$B=$ Suggested maximum flare rate for semi-rigid barrier system.
In most cases, use flare rate at or beyond shy line column even when guardrail is within the shy line.

$$
\begin{aligned}
& \boldsymbol{d}=1.8^{\prime} \text { FOR TYPE } 1 \text { TERMINALS } \\
& d=0 \text { FOR TYPE } 2 \text { AND } 3 \text { TERMINALS }
\end{aligned}
$$

$$
X=\frac{L_{H}+\left(\frac{b}{a}\right)\left(L_{1}\right)-\left(L_{2}+d\right)}{\frac{b}{a}+\frac{L_{H}}{L_{R}}}
$$

$$
Z=L_{2}+\left(\left|S_{B}-S_{A}\right|\right)\left(\frac{b}{a}\right)
$$

$$
\text { CLEAR ZONE }(7.01 .11), \ldots . . . . . . . . . . . . . . . . . . . . . . . . L_{c}=3^{\prime}
$$

$$
L_{1}=.23 .125^{\prime} \quad \text { ' u[N. ) }
$$

$$
\text { E.O.P. TO ROADSIDE FEATURE (MEASURED) } \ldots \ldots, \ldots, L_{3}=.4^{\prime}
$$

$$
\text { EFFECTJVE turned out distance of anchorace } \ldots d=0
$$

$$
L_{s}=\ldots 7 ' \text { SHY LINE ( } 7.01 .18 \text { ) }
$$

$$
\text { Lateral extent of roadside feature (veasured). } L_{H}=-30^{\prime}
$$

$$
\text { station at a }-347+01.1
$$

$$
\text { Lateral offset at end of flare } . . . . . . . . . . . . . . . .
$$

$$
\text { STATION AT а }-347+66.8
$$

## Used distance to face of bridge railing

$$
\begin{aligned}
& d=1.8^{\prime} \text { FOR TYPE } 1 \text { TERMINALS } \\
& d=0 \text { FOR TYPE } 2 \text { AND } 3 \text { TERMINALS }
\end{aligned}
$$

$$
X=\frac{L_{H}+\left(\frac{b}{a}\right)\left(L_{1}\right)-\left(L_{2}+d\right)}{\frac{b}{a}+\frac{L_{H}}{L_{R}}}
$$

$$
Z=L_{2}+\left(\left|S_{B}-S_{A}\right|\right)\left(\frac{b}{a}\right)
$$

$$
\text { LENGTH OF NEED } . \ldots . . . . . . . . . . . . . . . . . . . . . . . . . . . . .
$$

$$
\text { GUARDRAIL TAPER RATE (R-59-SERLES) } \ldots \ldots \ldots \ldots \cdot \frac{b}{a}=\frac{1 / 12}{4^{\prime}} \quad \text { APPROACH SLOPE }
$$

$$
\text { E.O.P. TO FACE OF BARRIER (DESJGNEDI ............. } L_{2}^{a}=\frac{4^{\prime}}{30^{\prime}}
$$

$$
\text { CLEAR ZONE }(7.01 .11), \ldots . . . . . . . . . . . . . . . . . . . . . . L_{c}={ }^{\prime} 0^{\prime}
$$

$$
L_{1}=.23 .125^{\prime} \quad \text { 'и[N. ) }
$$

$$
\text { E.O.P. TO ROADSIDE FEATURE (MEASURED) } \ldots \ldots, \ldots, L_{3}=.4^{\prime}
$$

$$
\text { EFFECTJVE turned out distance of anchorace } \ldots d=0
$$

$$
L_{s}=\ldots 7^{\prime} \quad \text { SHY LINE }(7.01 .18 \text { ) }
$$

$$
\text { station at a }-347+01.1
$$

$$
\text { Lateral extent of roadside feature (weasured). } L_{H}=-30^{\prime}
$$

$$
\text { STATION AT a }-347+66.8
$$

$$
\text { Lateral offset at end of flare. ................. } Z=9.47^{\text {n* }}
$$

CLEAR ZONE DISTANCES
(IN FEET FROM DGE OF DRIVING LANE)

| DESIGN SPEED | $\begin{aligned} & \text { DESIGN } \\ & \text { ADT } \end{aligned}$ | FILL SLPES |  |  | CUT SLOPES |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $1: 6$ OR FLATTER | $\begin{aligned} & 1: 5 \\ & \text { TO } \\ & 1: 4 \end{aligned}$ | 1:3 | 1:3 | $\begin{aligned} & 1: 4 \\ & \text { TO } \\ & \text { 1:5 } \end{aligned}$ | 1:6 OR <br> FLATTER |
| $\begin{gathered} 40 \mathrm{mph} \\ \text { or } \\ \text { Less } \end{gathered}$ | under 750 | 7-10 | 7-10 | ** | 7-10 | 7-10 | 7-10 |
|  | 750-1500 | 10-12 | 12-14 | ** | 10-12 | 12-14 | 12-14 |
|  | 1500-6000 | 12-14 | 14-16 | ** | 12-14 | 14-16 | 14-16 |
|  | over 6000 | 14-16 | 16-18 | ** | 14-16 | 16-18 | 16-18 |
| $\begin{aligned} & \text { 45-50 } \\ & \mathrm{mph} \end{aligned}$ | under 750 | 10-12 | 12-14 | ** | 8-10 | 8-10 | 10-12 |
|  | 750-1500 | 14-16 | 16-20 | ** | 10-12 | 12-14 | 14-16 |
|  | 1500-6000 | 16-18 | 20-26 | ** | 12-14 | 14-16 | 16-18 |
|  | over 6000 | 20-22 | 24-28 | ** | 14-16 | 18-20 | 20-22 |
| $\stackrel{55}{\mathrm{mnh}}$ | under 750 | 12-14 | 14-18 | ** | 8-10 | 10-12 | 10-12 |
|  | 750-1500 | 16-18 | 20-24 | ** | 10-12 | 14-16 | 16-18 |
|  | 1500-6000 | 20-22 | 24-30 | ** | 14-16 | 16-18 | 20-22 |
|  | over 6000 | 22-24 | 26-32* | ** | 16-18 | 20-22 | 22-24 |
| $\begin{gathered} 60 \\ \mathrm{mph} \end{gathered}$ | under 750 | 16-18 | 20-24 | ** | 10-12 | 12-14 | 14-16 |
|  | 750-1500 | 20-24 | 26-32* | ** | 12-14 | 16-18 | 20-22 |
|  | 1500-6000 | 26-30 | 32-40* | ** | 14-18 | 18-22 | 24-26 |
|  | over 6000 | 30-32* | 36-44* | ** | 20-22 | 24-26 | 26-28 |
| $\begin{aligned} & \geq 65 \\ & \mathrm{mph} \end{aligned}$ | under 750 | 18-20 | 20-26 | ** | 10-12 | 14-16 | 14-16 |
|  | 750-1500 | 24-26 | 28-36* | ** | 12-16 | 18-20 | 20-22 |
|  | 1500-6000 | 28-32* | 34-42* | ** | 16-20 | 22-24 | 26-28 |
|  | over 6000 | 30-34* | 38-46* | ** | 22-24 | 26-30 | 28-30 |

Where a site specific investigation indicates a high probability of continuing crashes, or such occurrences are indicated by crash history, the designer may provide clear zone distances greater than 30 feet as indicated. Clear zones may be limited to 30 feet for practicality and to provide a consistent roadway template if previous experience with similar projects or designs indicates satisfactory performance.
${ }^{* *}$ Since recovery is less likely on the unshielded, traversable $1: 3$ slopes, fixed objects should not be present in the vicinity of the toe of these slopes.

$$
\begin{aligned}
& \boldsymbol{d}=1.8^{\prime} \text { FOR TYPE } 1 \text { TERMINALS } \\
& d=0 \text { FOR TYPE } 2 \text { AND } 3 \text { TERMINALS }
\end{aligned}
$$

$$
X=\frac{L_{H}+\left(\frac{b}{\mathrm{a}}\right)\left(L_{1}\right)-\left(L_{2}+d\right)}{\frac{\mathrm{b}}{\mathrm{a}}+\frac{L_{H}}{L_{R}}}
$$

$$
Z=L_{2}+\left(\left|S_{B}-S_{A}\right|\right)\left(\frac{b}{a}\right)
$$

$$
\text { E.0.P. TO FACE OF BARRIER (DESJGNEDI } \ldots . . . . . . . . . L_{2}^{a}=\frac{4^{\prime}}{30^{\prime}}
$$

$$
\text { CLEAR ZONE }(7.01 .11), \ldots . . . . . . . . . . . . . . . . . . . . . . L_{c}=3^{\prime}
$$

$$
L_{1}=.23 .125^{\prime} \quad \text { ' и[N. ) }
$$

$$
\text { E.O.P. TO ROADSIDE FEATURE (YEASURED) } \ldots \ldots, \ldots, L_{3}=.4^{\prime}
$$

$$
\text { EFFECTIVE TURNED OUT DISTANCE OF ANCHORAGE } \ldots d=0
$$

$$
L_{s}=\ldots 7 ' \text { SHY LINE ( } 7.01 .18 \text { ) }
$$

$$
\text { Lateral extent of roadside feature (weasured). } L_{H}=-30^{\prime}
$$

$$
\text { station at a }-347+01.1
$$

$$
\text { Lateral offset at end of flare } . . . . . . . . . . . . . . . .
$$

$$
\text { STATION AT а }-347+66.8
$$

## Used distance to face of bridge railing

$$
\begin{aligned}
& \boldsymbol{d}=1.8^{\prime} \text { FOR TYPE } 1 \text { TERMINALS } \\
& d=0 \text { FOR TYPE } 2 \text { AND } 3 \text { TERMINALS }
\end{aligned}
$$

$$
X=\frac{L_{H}+\left(\frac{b}{a}\right)\left(L_{1}\right)-\left(L_{2}+d\right)}{\frac{b}{a}+\frac{L_{H}}{L_{R}}}
$$

$$
Z=L_{2}+\left(\left|S_{B}-S_{A}\right|\right)\left(\frac{b}{a}\right)
$$

| LENGTH OF NEED ................................................. $=$ $\qquad$ <br>  $185^{\prime}$ $\qquad$ <br> guardrail taper rate (r-59-SERIES) $\qquad$ $\frac{b}{a}=$ $\frac{1 / 12}{4^{\prime}}$ <br> E.OP. TO FACE OF BARRIER (DESIGNEDI <br> $\ldots, L_{2}=$ $\qquad$ | DESJGN ADT DESJCN SPEED approach slope | 5,000 vpd |
| :---: | :---: | :---: |
|  |  | 55 mph |
|  |  | 1:5 |
|  |  |  |

E.O.P. TO FACE OF BARRCER (DESJGNED) ............. $L_{2}^{a}=\frac{4^{\prime}}{30^{\prime}}$

CLEAR ZONE ( 7.01 .11 ) $\ldots . . . . . . . . . . . . . . . . . . . . . . . . . L_{c}=3^{\prime}$
$L_{1}=23.125^{\prime} \quad$ ' U[N. )
E.O.P. TO ROADSIDE FEATURE (MEASUREDI $\ldots \ldots . . . . . . L_{3}=.4$ '
$L_{s}=\ldots 7$ ' SHY LLNE ( 7.01 .18 )
EFFECTJVe turned out distance of anchorage $\ldots d={ }^{2} 0$
lateral extent of roadside feature (weasured). $L_{H}=3^{\prime}$ Lateral offset at end of flare.................. $Z=9.47^{\text {** }}$
station at a $-347+01.1$
station at a $-347+66.8$

## Using a Type 2M approach terminal, so d=0

$$
\begin{aligned}
& d=1.8^{\prime} \text { FOR TYPE } 1 \text { TERMINALS } \\
& d=0 \text { FOR TYPE } 2 \text { AND } 3 \text { TERMINALS }
\end{aligned}
$$

$$
X=\frac{L_{H}+\left(\frac{b}{a}\right)\left(L_{1}\right)-\left(L_{2}+d\right)}{\frac{b}{a}+\frac{L_{H}}{L_{R}}}
$$

$$
Z=L_{2}+\left(\left|S_{B}-S_{A}\right|\right)\left(\frac{b}{a}\right)
$$

| * ${ }^{\text {c }}$ 113.76' | 5,000 vpd |
| :---: | :---: |
|  | DESICN SPEED - 55 mph |
| guardeail taper pate (r-59-SEPIES) $\underline{b}^{n}=1 / 12$ | Roach slope $1: 5$ |
| E.O.P. TO FACE OF BARRIER (DESJGNED) ............ $L_{2}=$ 4 $\qquad$ |  |
| CLEAR ZONE ( 7.01 .11 ) . ...................... $L_{c}=$ _ $30^{\prime}$ |  |
| E.O.P. TO ROADSIDE FEATURE (MEasuredi . . . . . . . . . $L_{3}=.4{ }^{\text {a }}$ | $L_{s}=\ldots \ldots 7{ }^{\text {c }}$ SHY LINE ( 7.01 .18 |
| effective turned out distance of anchorage ... d | station at a $-347+01.1$ |
| Lateral extent of roadside feature ineasuredi. $L_{H}={ }^{\text {a }}$ 30' | Station at a $-347+66.8$ |
| lateral offset at end of flare ............... $Z$ Z $=9.47$ ' |  |

## $L_{H}=L_{C}$ in this case, since the river is the hazard and extends beyond the clear zone

$$
\begin{aligned}
& \boldsymbol{d}=1.8^{\prime} \text { FOR TYPE } 1 \text { TERMINALS } \\
& \boldsymbol{d}=0 \text { FOR TYPE } 2 \text { AND } 3 \text { TERMINALS }
\end{aligned}
$$

$$
X=\frac{L_{H}+\left(\frac{b}{a}\right)\left(L_{1}\right)-\left(L_{2}+d\right)}{\frac{b}{a}+\frac{L_{H}}{L_{R}}}
$$

$$
Z=L_{2}+\left(\left|S_{B}-S_{A}\right|\right)\left(\frac{b}{a}\right)
$$

| LENGTH OF NEED ................................................ $=$ <br> RUNOUT LENGTH ( 7.01 .19 ) ........................... $L_{R}=$ <br> guardrail taper rate (r-59-SERES) . ............ $\frac{b}{a}=\frac{\overline{1 / 12}}{4^{\prime}}$ |  | 5,000 vpd |
| :---: | :---: | :---: |
|  | DESJGN ADT | 55 mph |
|  |  | 1:5 |
|  |  |  |

E.O.P. TO FACE OF BARRIER (DESICNED) ............. $L_{2}^{a}=\frac{4^{\prime}}{30^{\prime}}$ CLEAR ZONE ( 7.01 .11 ) $\ldots . . . . . . . . . . . . . . . . . . . . . . . . . L_{c}=3^{\prime}$

$$
L_{1}=.23 .125^{\prime} \quad \text { ' u[N. ) }
$$

E.O.P. TO ROADSIDE FEATURE (MEASUREDI $\ldots \ldots, \ldots, L_{3}=.4^{\prime}$
effective turned out distance of anchorage $\ldots d=0$ lateral extent of roadside feature (weasured). $L_{H}=3^{\prime}$ Lateral offset at end of flare.................. $Z=9.47^{\text {** }}$
$L_{s}=\ldots 7$ ' SHY LINE ( 7.01 .18 )
station at a $-347+01.1$
station at a $-347+66.8$
$L_{1}<25^{\prime}$ in this case because $L_{1}=L_{T}$ (exception to $L_{1}=25$ ' min. rule)

## Detail T-1 (Sheet 1 of R-67-Series)


$\boldsymbol{d}=1.8^{\prime}$ FOR TYPE 1 TERMINALS
$\boldsymbol{d}=0$ FOR TYPE 2 AND 3 TERMINALS

$$
X=\frac{L_{H}+\left(\frac{b}{a}\right)\left(L_{1}\right)-\left(L_{2}+d\right)}{\frac{b}{a}+\frac{L_{H}}{L_{R}}}
$$

$$
Z=L_{2}+\left(\left|S_{B}-S_{A}\right|\right)\left(\frac{b}{a}\right)
$$

$$
\text { E.O.P. TO FACE OF barrier (DESJGNEDI } \ldots . . . . . . . . . \stackrel{L}{2}_{2}^{a}=\frac{4^{\prime}}{20^{\prime}}
$$

$$
L_{1}=.23 .125^{\prime} \quad \text { ' и[N. ) }
$$

$$
\text { E.0.P. TO ROADSIDE FEATURE (MEASURED . . . . . . . . . . . } L_{3}=.4^{\prime}
$$

$$
\text { EFFECTIVE TURNED OUT DISTANCE OF anchorace } \ldots d=0
$$

$$
\text { Lateral extent of roadside feature (weasuredl. } L_{H}=3^{\prime}
$$

STATJON AT A $-347+01.1$
station at a $-347+66.8$

| Design Speed (mph) | Shy Line Offset (Ls) (ft) |
| :---: | :---: |
| 80 | 12 |
| 75 | 10 |
| 70 | 9 |
| 60 | 8 |
| 55 | 7 |
| 50 | 6.5 |
| 45 | 6 |
| 40 | 5 |
| 30 | 4 |

$$
\begin{aligned}
& \boldsymbol{d}=1.8^{\prime} \text { FOR TYPE } 1 \text { TERMINALS } \\
& d=0 \text { FOR TYPE } 2 \text { AND } 3 \text { TERMINALS }
\end{aligned}
$$

$$
X=\frac{L_{H}+\left(\frac{b}{a}\right)\left(L_{1}\right)-\left(L_{2}+d\right)}{\frac{b}{a}+\frac{L_{H}}{L_{R}}}
$$

$$
Z=L_{2}+\left(\left|S_{B}-S_{A}\right|\right)\left(\frac{b}{a}\right)
$$

$$
\text { E.0.P. TO FACE OF BARRIER (DESJGNED1 } . . . . . . . . . . \stackrel{L}{L}_{2}^{a}=\frac{4^{\prime}}{30^{\prime}}
$$

$$
\text { CLEAR ZONE }(7.01 .11) \ldots \ldots . \ldots . . . . . . . . . . . . L_{c}=L^{\prime}
$$

$$
L_{1}=.23 .125^{\prime} \quad \text { ' u[N. ) }
$$

$$
\text { E.O.P. TO ROADSIDE FEATURE (MEASURED) } \ldots \ldots, \ldots, L_{3}=.4^{\prime}
$$

$$
\text { EFFECTJVE TURNED OUT DISTANCE OF anchorace } \ldots d^{-}=0
$$

$$
L_{s}=\ldots 7 ' \text { SHY LINE ( } 7.01 .18 \text { ) }
$$

$$
\text { Lateral extent of roadside feature (veasuredl. } L_{H}=-30^{\prime}
$$

$$
\text { station at a }-347+01.1
$$

$$
\text { Lateral offset at end of flare ................... } Z=9.47^{* *}
$$

$$
\text { STATION AT а }-347+66.8
$$

$L_{1}<25^{\prime}$ in this case because $L_{1}=L_{T}$ (exception to $L_{1}=25$ min. rule)

## Length of Need (X)

$X=\frac{30+\left(\frac{1}{12}\right) \times(23.125)-4}{\left(\frac{1}{12}\right)+\left(\frac{30}{185}\right)}=113.76^{\prime}$

## Minimum Guardrail Length



$$
G_{\min }=113.76^{\prime}-34.3^{\prime}-23.125^{\prime}=56.34^{\prime}
$$

## However, the MGS ( $\left.9^{\prime}-4.5^{\prime \prime}\right)$ beam element and thrie-beam

 transition panel must be considered due to $\mathrm{T}-1$ anchorage

ELEVATION SHOWING TRANSITION DETAIL FOR CONNECTING
GUARDRAIL, TYPE MGS-8 OR MGS-8D TO
GUARDRAIL, TYPE T, GUARDRAIL, TYPE TD,
GUARDRAIL ANCHORAGE, MEDIAN,
GUARDRAIL ANCHORAGE, BRIDGE DETAIL A1, T1, T4 OR T6
$\therefore$ \# of 12.5' panels $=\left(\frac{56.34-9.375-6.25}{12.5}\right)=3.26 \rightarrow 4$ panels Type MGS-8 guardrail length $=(12.5)(4)+9.375+6.25$

$$
=\underline{65.625 \text { feet }}
$$

## Reflectors

$\#$ of reflectors $=\left(\frac{65.625+23.125}{50}\right)+1=2.78 \rightarrow$ round up to 3 *** But two-way roads require reflectors facing both sides ***
$\therefore$ \# of reflectors $=3 \times 2=\underline{6}$ reflectors

## Stations A and B



## Calculating Stations $A$ and $B$

Does Flaring Affect the Calculations?


Assume L $\approx$ L' for most guardrail applications
(unless dealing with extremely long installations)

## Stations

## Station $A=(346+78)+23.125^{\prime} \approx \underline{347+01.1}$

Station $B=(346+78)+23.125+65.625^{\prime} \approx \underline{347+66.8}$

## Calculating Z

$$
\begin{aligned}
\mathrm{Z} & =\mathrm{L}_{2}+\left(\text { Distance }_{\mathrm{B}-\mathrm{A}}\right) \times\left(\frac{b}{a}\right) \\
& =4+(65.625) \times\left(\frac{1}{12}\right)=\underline{9.47^{\prime}}
\end{aligned}
$$

## Pay [TENS

65.625 Ft * Guordrail, Type MGS-8
_1 - Ea Guardrail Anchorage, Bridge, Det T-1
___ Ft Bridge Railing. Thrie Beom Retrofit
_ _ Eo Guordrail Approoch Terminal, Type 2M
___ Ea Guardrail Departing Terminal, Type _
_6 . Ea Guardrail Reflector
___Cyd Embonkment, LK

$\boldsymbol{d}=1.8^{\prime}$ FOR TYPE 1 TERMINALS
$\boldsymbol{d}=0$ FOR TYPE 2 AND 3 TERMINALS

$$
X=\frac{L_{H}+\left(\frac{b}{a}\right)\left(L_{1}\right)-\left(L_{2}+d\right)}{\frac{b}{a}+\frac{L_{H}}{L_{R}}}
$$

$$
\left.Z=L_{2^{+}}+\left|S_{B}-S_{A}\right|\right)\left(\frac{b}{a}\right)
$$

| LENGTH OF NEED ................................ $X=64.88{ }^{\prime}$ | DESJGN ADT | 5,000 vpd |
| :---: | :---: | :---: |
| RUNOUT LENGTH ( 7.01 .19 ) . ...................... $L_{R}=.185^{\prime}$ | DESJCN SPEED | 55 mph |

GUARDRALL TAPER RATE (R-59-SERIES) $\ldots \ldots \ldots \ldots, \frac{b}{a}=\_1 / 12$. APPROACH SLOPE _ $1: 5$
E.O.P. TO FACE OF BARRIER (DESIGNEDI ............. $L_{z}=1^{16}$ '_
CLEAR ZONE ( 7.01 .11 ) $\ldots . . . . . . . . . . . . . . . . . . . . . . . . . L_{c}=30^{\prime}$
$L_{1}=23.125^{\prime} 5^{\prime}$ u[N. )
E.0.p. TO ROADSIDE FEATURE (MEASURED) $\ldots \ldots . . . . . L_{3}=16^{\prime}$
$L_{s}=$ _ $^{\prime}$. SHY LLNE ( 7.01 .18 )
effective turned out distance of anchorage $\ldots d=$. 0
Lateral extent of roadside feature tweasuredi. $L_{H}=3^{\prime}$
station at a $345+76.9$
station at a $345+48.8$ Lateral offset at end of flare ................ $z=6.34^{\prime}$ (measured from EOP)** 18.34' (measured from CL)**

NOTE: DISTANCE OF OBJECT FROK BACK OF BARRLER MUST be GREATER THAN THE NAX[MUN DEFLECT]ON ( 7.01 .20 )
$L_{H} \leq L_{c}$
REFER TO STANDARD PLAN R-59-SERJES AND DESIGN MANUAL
SECTION 7.01.30 FOR GUARDRALL AT EMBANKMENTS
** Refer to Calculations and Notes

## Length of Need (X)

$$
X=\frac{30+\left(\frac{1}{12}\right) \times(23.125)-16}{\left(\frac{1}{12}\right)+\left(\frac{30}{185}\right)}=64.88^{\prime}
$$

## Guardrail Length

Using a Guardrail Approach Terminal, Type 2M with Guardrail, Type MGS-8 in this case
$\therefore$ Min. Guardrail Length $=64.88^{\prime}-23.125^{\prime}-34.3^{\prime}=7.46^{\prime}$

However, in this case, the minimum length of Type MGS-8 between the $\mathrm{T}-1$ anchorage and Type 2 M approach terminal is 28'-1.5" due to the required height transition section; see MDOT Standard Plan R-60-Series.
$\therefore$ Type MGS-8 guardrail length $=\underline{28.125 \text { feet }}$


## Reflectors

$\#$ of reflectors $=\left(\frac{28.125+23.125}{50}\right)+1=2.02 \rightarrow$ round up to 3 *** But two-way roads require reflectors facing both sides ***
$\therefore$ \# of reflectors $=3 \times 2=\underline{6}$ reflectors

## PAY [TENS

$28.125 \mathrm{Ft} *$ Guordrail, Type MGS-8
_1.Ee Guardrail Anchorage, Bridge, Det T-1
___ Ft Bridge Railing. Thrie Beom Retrofit
_1 . Eo Guordrail Approach Terminal, Type 2M
__ Ea Guardrail Departing Terminal, Type __
_6 _ Eo Guordrail Reflector
__Cyd Embonkment, LL

Stations
Station $A=(346+00)-23.125^{\prime} \approx \underline{345+76.9}$
Station $B=(346+00)-23.125-28.125^{\prime} \approx \underline{345+48.8}$

## Calculating Z

Z

$$
\begin{aligned}
& =\mathrm{L}_{2}+\left(\text { Distance }_{\mathrm{B}-\mathrm{A}}\right) \times\left(\frac{b}{a}\right) \\
& =16+(28.125) \times\left(\frac{1}{12}\right)=\underline{18.34^{\prime}(\text { measured from CL) }}
\end{aligned}
$$

$$
\begin{gathered}
\text { or } \\
=4+(28.125) \times\left(\frac{1}{12}\right)=\underline{6.34^{\prime}(\text { measured from EOP) })}
\end{gathered}
$$

## Guardrail Design Shielding Embankments



## Guardrail at Embankments MDOT Method

## Parallel Guardrail Installations

- Section 7.01.30F of RDM
$\underset{\text { DF TRAFFIC }}{\text { DIRECTION }}$


## SHOULDER



## Guardrail at Embankments MDOT Method

Parallel Guardrail Installations

- Section 7.01.30F of RDM

| GUARDRAIL AT EMBANKMENTS <br> (PARALLEL INSTALLATIONS) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| HEIGHT OF FILL <br> AT <br> $1: 3$ (ft) | LENGTH OF NEED IN <br> ADVANCE OF <br> $1: 3(\mathrm{ft})$ |  |  |  |
| OVER | TO | 70 mph | 60 mph | 50 mph |
| 5 | 10 | 147 | 121 | 100 |
| 10 | 12 | 197 | 171 | 122 |
| 12 | 14 | 235 | 205 | 153 |
| 14 | 16 | 269 | 238 | 179 |
| 16 | 18 | 296 | 262 | 198 |
| 18 | 20 | 316 | 280 | 212 |
| 20 | 22 | 331 | 294 | 223 |
| 22 | 24 | 343 | 305 | 231 |
| 24 | 25 | 349 | 309 | 235 |

# Guardrail at Embankments <br> MDOT Method 

Flared Guardrail Installations

- Section 7.01.30E of RDM
- MDOT Standard Plan R-59 Series

** SEE CHART FOR THE " X " AND THE "K" DISTANCE. (SHEET 6 OF 6)
BEAM GUARDRAIL AT EMBANKMENTS - TWO-WAY ROADWAYS


1:10 SLOPE BETWEEN SHOULDER LINE AND $2^{\prime}-0^{\prime \prime}$ BEHIND FACE DF POST.
"/7/ 1:6 BERM

## Standard Plan R-59-E X \& K Values

| GUARDRAIL AT EMBANKMENTS (FLARED INSTALLATIONS, b/a) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| HEIGHT OF FILL AT 1:3 SLOPE (FEET) |  | 70 MPH <br> FLARE 1 : 15 |  | $\begin{gathered} 60 \text { MPH } \\ \text { FLARE } 1: 14 \end{gathered}$ |  | $\begin{gathered} 50 \text { MPH } \\ \text { FLARE } 1: 11 \end{gathered}$ |  |
| OVER | TO | X | K | X | K | X | K |
| 5 | 10 | 100 | 37.5 | 100 | 12.5 | 100 | 0 |
| 10 | 12 | 100 | 37.5 | 100 | 12.5 | 100 | 0 |
| 12 | 14 | 100 | 37.5 | 100 | 12.5 | 100 | 0 |
| 14 | 16 | 113 | 24.5 | 110 | 2.5 | 100 | 0 |
| 16 | 18 | 155 | -17.5 | 149 | -36.5 | 101 | -1 |
| 18 | 20 | 193 | -55.5 | 182 | -69.5 | 127 | -27 |
| 20 | 22 | 223 | -85.5 | 207 | -94.5 | 148 | -48 |
| 22 | 24 | 246 | -108.5 | 227 | -113.5 | 164 | -64 |
| 24 | 25 | 256 | -118.5 | 235 | -122.5 | 171 | -71 |



FOR POSITIVE "K" DISTANCES, BEGIN FLARE POINT BEYOND THE $1: 3$ SLOPE.


FOR NEGATIVE "K" DISTANCES, BEGIN FLARE POINT IN ADVANCE OF THE 1:3 SLOPE.


BEAM GUARDRAIL AT EMBANKMENTS - TWO-WAY ROADWAYS
(BARN ROOF SLOPE)

** SEE CHART FOR THE " $X$ " AND THE "K" DISTANCE. (SHEET 6 OF 6)
BEAM GUARDRAIL AT EMBANKMENTS - DUAL ROADWAYS


BEAM GUARDRAIL AT EMBANKMENTS - DUAL ROADWAYS

## Guardrail at Embankments <br> Calculation Method (AASHTO RDG)


$L_{c}$ is clear zone based on slope at Point $V$ (in this example, the slope would be a 1:6 Fill Slope)

## Guardrail at Embankments

Calculation Method

## Methodology

- Step 1: Determine $L_{R}$
- Step 2: Determine $L_{c}$
- In this case, $\mathrm{L}_{\mathrm{H}}=\mathrm{L}_{\mathrm{c}}$


## Guardrail at Embankments

Calculation Method

## Methodology

- Step 3: Determine Layout and Terminal
- Flared or Parallel Guardrail If flared:
- Determine flare rate (b/a)
- Determine location where flare begins
- Terminal Type:
- Type 1 (Flared) or Type 2 (Parallel) Terminal


## Guardrail at Embankments

Calculation Method

## Methodology

- Step 4: Determine Guardrail Location $\left(\mathrm{L}_{2}\right)$


## Guardrail at Embankments

Calculation Method

## Methodology

- Step 5: Use appropriate formula to calculate length of need $(X)$ in advance of 1:3 point


## Guardrail at Embankments

Calculation Method

## Methodology

- Step 5: Use appropriate formula to calculate length of need $(X)$ in advance of 1:3 point

$$
X=\frac{L_{H}+(b / a)\left(L_{1}\right)-\left(L_{2}+d\right)}{(b / a)+\left(L_{H} / L_{R}\right)}
$$



## Design Data \& Assumptions



- Rural Two-Lane Road
- Design Speed = 60 mph
- ADT = 8,700 vpd
- Parallel Installation (SB side; west side of road)
- Approach End: Use Chapter 7 - RDM to design guardrail
- Departing End: Use Calculation Method to design guardrail
- Type MGS-8 guardrail will be used
- Type 2M guardrail approach terminals will be used
- $L_{c}=32^{\prime}\left(1: 6\right.$ slope at Sta. $168+79 ; 250^{\prime}\left(L_{r}\right)$ south of Sta. 171+29)
- Assume $L_{2}=8.4^{\prime}$ (i.e., $10^{\prime}-1.6^{\prime}$ ); requires use of $9^{\prime}$ posts



## 9' Posts <br> Required

## Approach End (North End)

## Refer to Subsection 7.01.30.F of Michigan Road Design Manual

- Fill Height $=14^{\prime}$ at 1:3 Point (Sta. $178+84$ ); Speed $=60 \mathrm{mph}$
$\therefore$ Length of Need in Advance of 1:3 = 205'

| GUARDRAIL AT EMBANKMENTS (PARALLEL INSTALLATIONS) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| HEIGHT OF FILL AT 1:3 (ft) |  | LENGTH OF NEED IN ADVANCE OF 1:3 (ft) |  |  |
| OVER | TO | 70 mph | 60 mph | 50 mph |
| 5 | 10 | 147 | 121 | 100 |
| 10 | 12 | 197 | 171 | 122 |
| 12 | 14 | 235 | 205 | 153 |
| 14 | 16 | 269 | 238 | 179 |
| 16 | 18 | 296 | 262 | 198 |
| 18 | 20 | 316 | 280 | 212 |
| 20 | 22 | 331 | 294 | 223 |
| 22 | 24 | 343 | 305 | 231 |
| 24 | 25 | 349 | 309 | 235 |

## Departing End (South End)

- Shoulder hinge point on west side of road is within northbound (NB) traffic's clear zone
- Use guardrail worksheet to calculate length of need
- Guardrail ending on south end is within NB traffic's clear zone
- Must use a crashworthy guardrail terminal (i.e., Type 2M guardrail approach terminal).


|  | desjgn adt $\quad 8,700 \mathrm{vpd}$ |
| :---: | :---: |
| RUNOUT LENGTH ( 7.01 .19 ) . ...................... $L_{R}=.250^{\prime}$ | design speed _ 60 mph |
| guardrail taper rate (R-59-SERIES) . . . . . . . . . $\cdot \frac{b}{a}={ }_{-} 0$ | approach slope _1:6 |
| E, O.P. TO FACE OF BARRIER (DESJGNEDI $\ldots \ldots . . . . . . L_{2}=L_{2}=20.4{ }^{\prime}$ |  |
| CLEAR ZONE ( 7.01 .11 ) . . . . . . . . . . . . . . . . . . . . . $L_{c}=3{ }^{\prime}$ | $L_{1}=\mathrm{N} / \mathrm{A}$ |
| E.0.p. TO ROADSJDE FEATURE (Measured) .......... $L_{3}=16{ }^{\prime}$ | $L_{s}=\ldots 8^{\prime}$. SHY LINE ( 7.01.18 ) |
| effective turned out distance of anchorage ... d | station ata $\mathrm{N} / \mathrm{A}$ |
| lateral extent of roadside feature (weasured). $L_{H}={ }^{\text {a }}$ 3' | Station at a $170+72.7$ |
| lateral offset at end of flare................ $Z=8.4{ }^{\prime}$ |  |

## Departing End



On two-lane, two-way roads, $\mathrm{L}_{2}, \mathrm{~L}_{\mathrm{H}}$, and $\mathrm{L}_{\mathrm{C}}$ referenced from centerline on departing end

Length of Need (X) - South End (Using Guardrail Worksheet)
$X=\frac{32-20.4}{\left(\frac{32}{250}\right)}=90.63^{\prime}{ }^{\prime}$ (measured from 1:3 point; Sta. 171+29)

## Total Guardrail Length

Min. Length $=(178+84)-(171+29)+205+90.63-2(34.3)$

$$
=982.03^{\prime}
$$

\# of panels $=\frac{982.03}{12.5}=78.56 \rightarrow$ round up to 79 panels
$\therefore$ Type MGS-8 Guardrail Length $=(12.5)(79)=\underline{987.5 \text { feet }}$

## Reflectors

$\#$ of reflectors $=\left(\frac{987.5}{50}\right)+1=20.75 \rightarrow$ round up to 21 *** But two-way roads require reflectors facing both sides ***
$\therefore$ \# of reflectors $=21 \times 2=\underline{42}$ reflectors

## Stations

- The difference between the minimum guardrail length and the actual guardrail length $=987.5-982.03 \approx 5.47^{\prime}$
- The additional $5.47^{\prime}$ of guardrail will be placed on the north (approach) end.


## North (Approach) End

Station where approach terminal meets Type MGS-8 guardrail on the north (approach) end is:

Station $B_{n}=(178+84)+205+5.47-34.3=\underline{180+60.2}$
Station $A_{n} \rightarrow N / A$ in this case

## South (Departing) End

Station where approach terminal meets Type MGS-8 guardrail on the south (departing) end is:

Station $B_{s}=(171+29)-90.63+34.3 \approx \underline{170+72.7}$
Station $A_{s} \rightarrow N / A$ in this case

Check: Type MGS-8 Guardrail Length $=$ Sta. $\mathrm{B}_{\mathrm{n}}-$ Sta. $\mathrm{B}_{\mathrm{s}}$

$$
\begin{aligned}
& 987.5 \text { feet }=(180+60.2)-(170+72.7) \\
& 987.5 \text { feet }=987.5 \text { feet } \checkmark
\end{aligned}
$$

Calculating Z
$Z=\underline{8.4^{\prime}}$ (measured from EOP)


## Quantities

987.5 Ft Guardrail, Type MGS-8

2 Ea
42 Ea
Guardrail Approach Terminal, Type 2M Guardrail Reflector

## Questions?

## Contact Information Carlos Torres

Phone: (517) 335-2852
E-mail: torresc@michigan.gov

